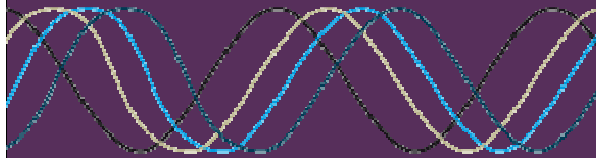
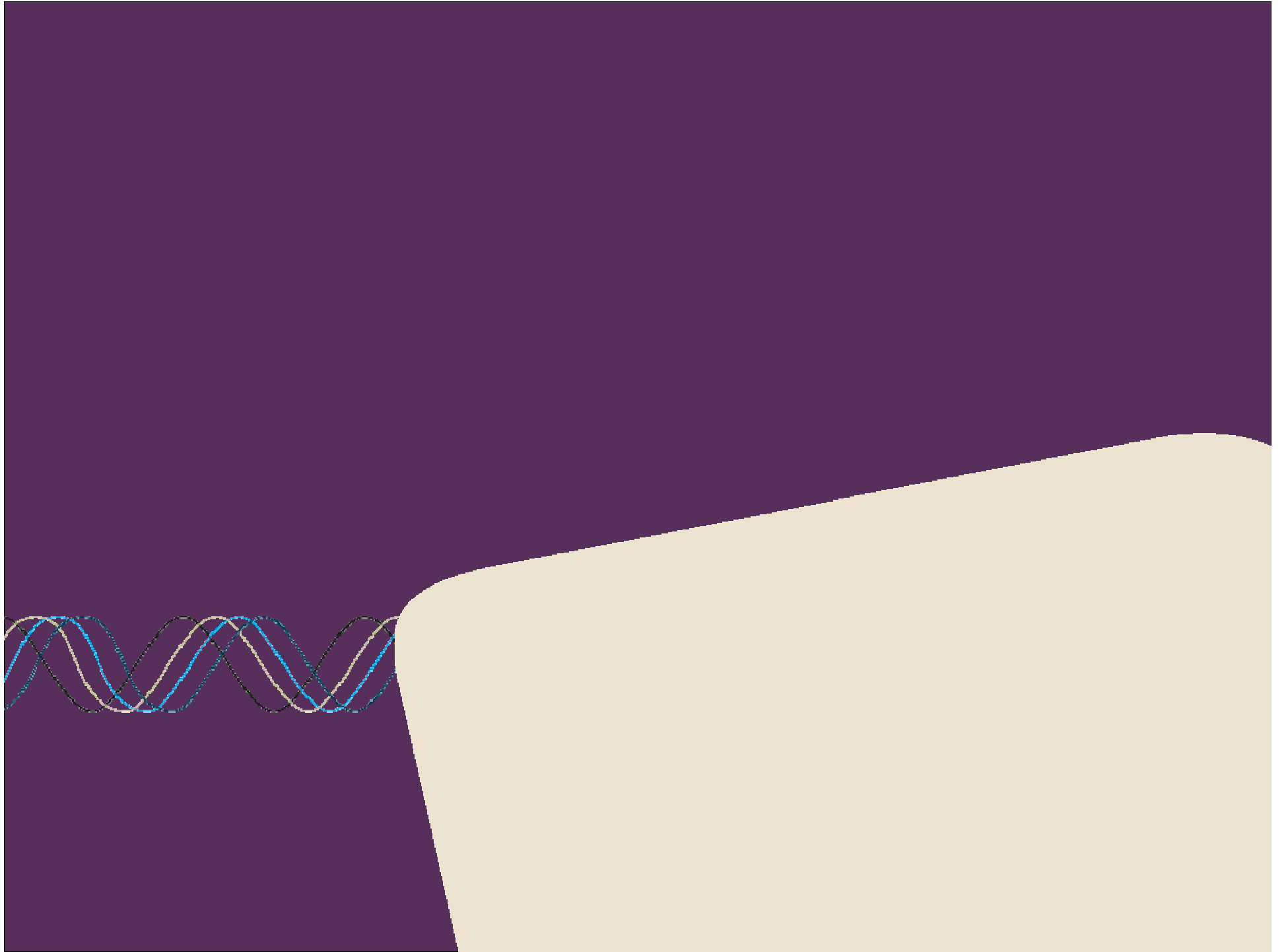


Fundamentals in signal analysis of passive acoustic data

Dr Cédric Gervaise & Dr Lucia Di Iorio



Chaire CHORUS
Remote sensing of Aquatic Environment
By
Passive Acoustics

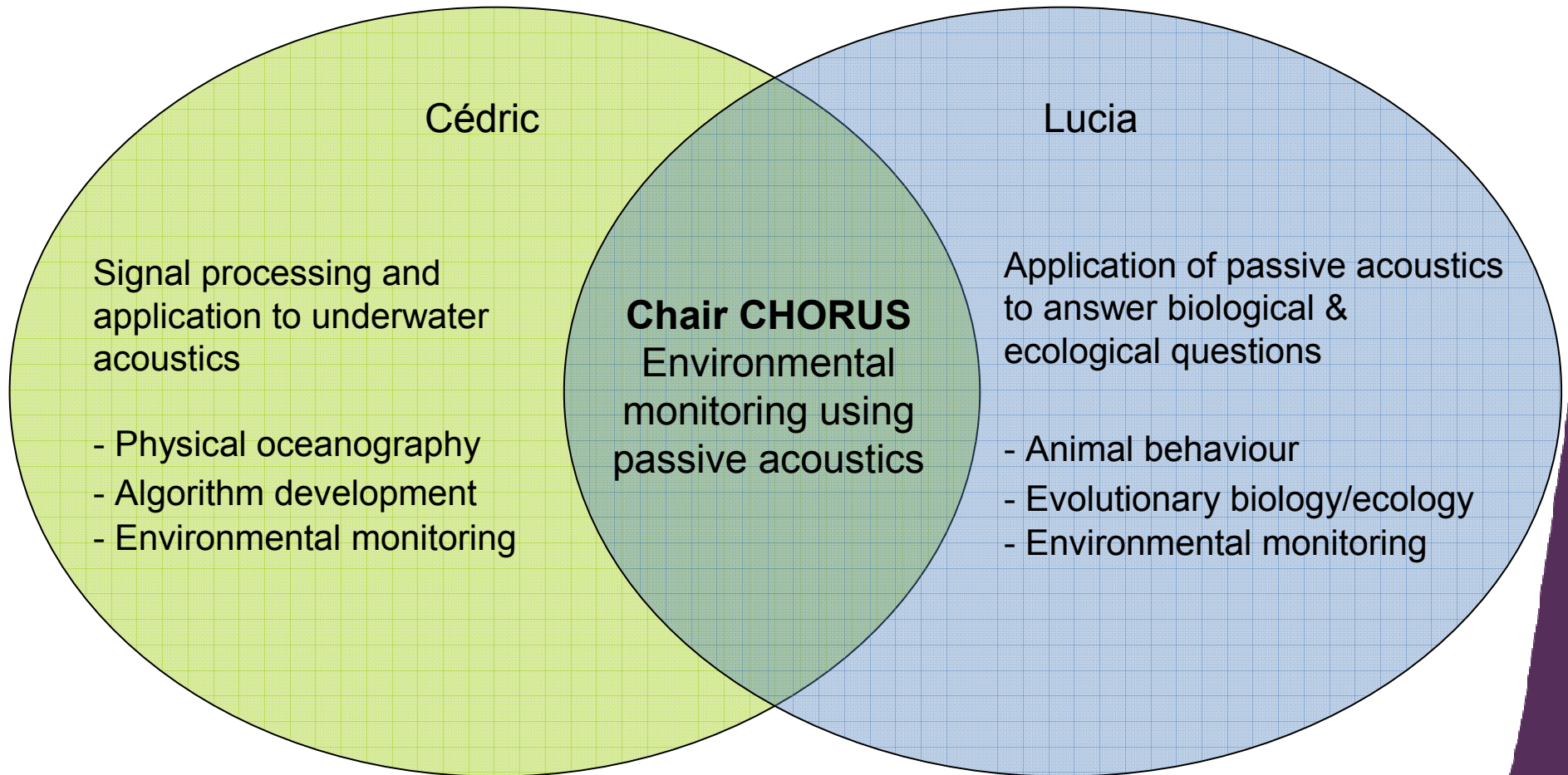


Outline

- **Introduction**
- Introduction to sound
- Measurement chain
- Spectral analysis of acoustic measurements
- Time-frequency representation
- Applied examples from our own research

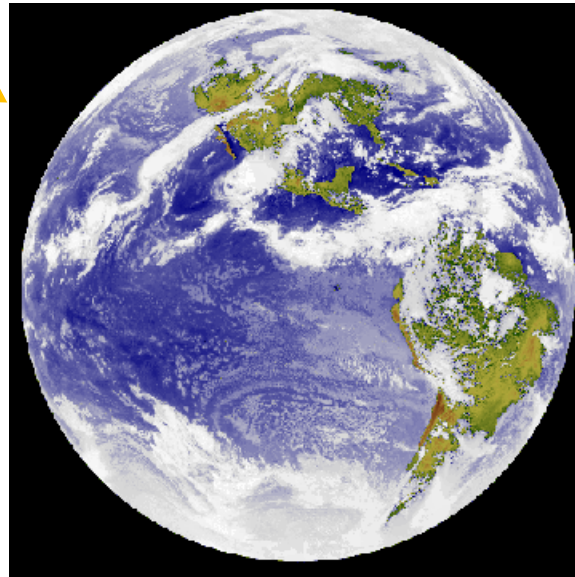


Who are we ?



Why sound in a time series conference?

hosts



medium

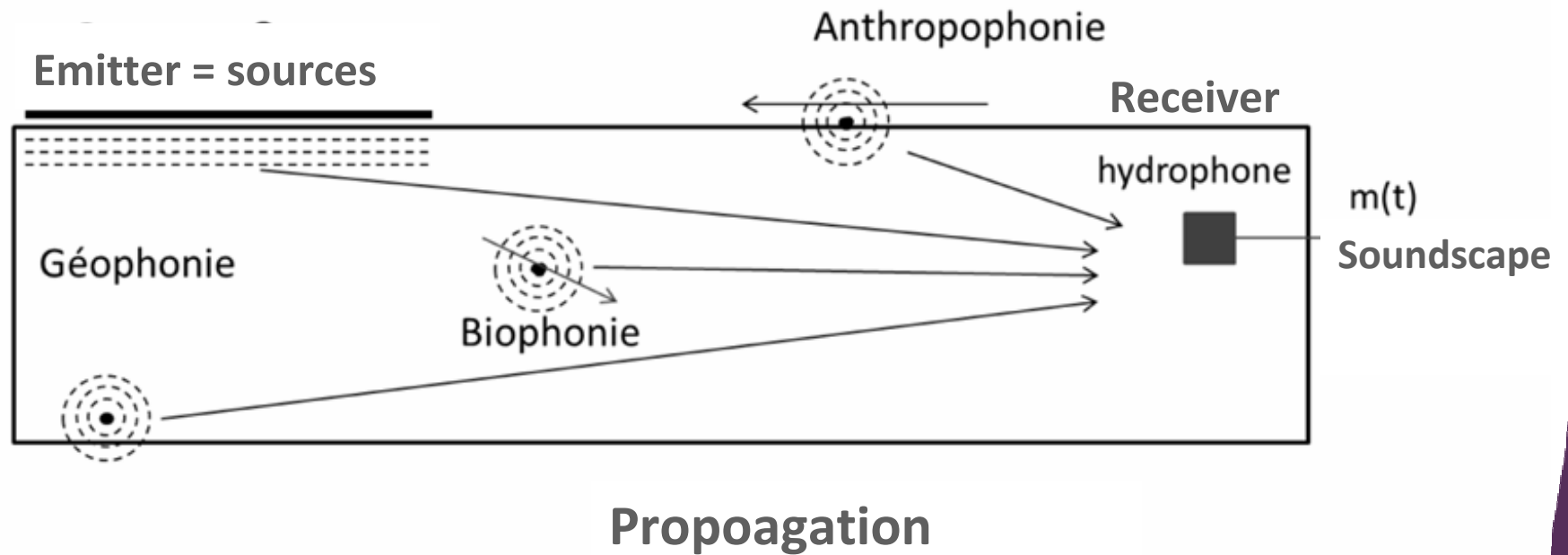
Services deriving from the hydrosphere : 20 900 billions \$ / year

**The ocean: a vast still largely unknown environment
Its observation : a priority of the 21st century**



Costanza, R.; d'Arge, R.; De Groot, R.; Farber, S.; Grasso, M.; Hannon, B.; Limburg, K.; Naeem, S.; O'Neill, R.; Paruelo, J. & others (1997), 'The value of the world's ecosystem services and natural capital', *Nature* **387(6630)**, 253--260.

Why sound in a time series conference?



AQUATIC ENVIRONMENT = ACOUSTIC SOUNDSCAPE

- Pijanowski, B.; Villanueva-Rivera, L.; Dumyahn, S.; Farina, A.; Krause, B.; Napoletano, B.; Gage, S. & Pieretti, N. (2011), 'Soundscape ecology: the science of sound in the landscape', *BioScience* **61(3)**, **203--216**.
- Radford, C.; Stanley, J.; Tindle, C.; Montgomery, J. & Jeffs, A. (2010), 'Localised coastal habitats have distinct underwater sound signatures', *Mar. Ecol. Prog. Ser.* **401**, **21-29**
- Kennedy, E.; Holderied, M.; Mair, J.; Guzman, H. & Simpson, S. (2010), 'Spatial patterns in reef-generated noise relate to habitats and communities: Evidence from a Panamanian case study', *Journal of Experimental Marine Biology and Ecology* **395(1-2)**, 85--92.
- Gervaise, C.; Di Iorio, L.; Grall, J.; Chauvaud, L. ; Jolivet, A. ; Clavier, J. (2012), 'La polyphonie côtière : des sons au fonctionnement des écosystèmes', *Chapitre HDR*

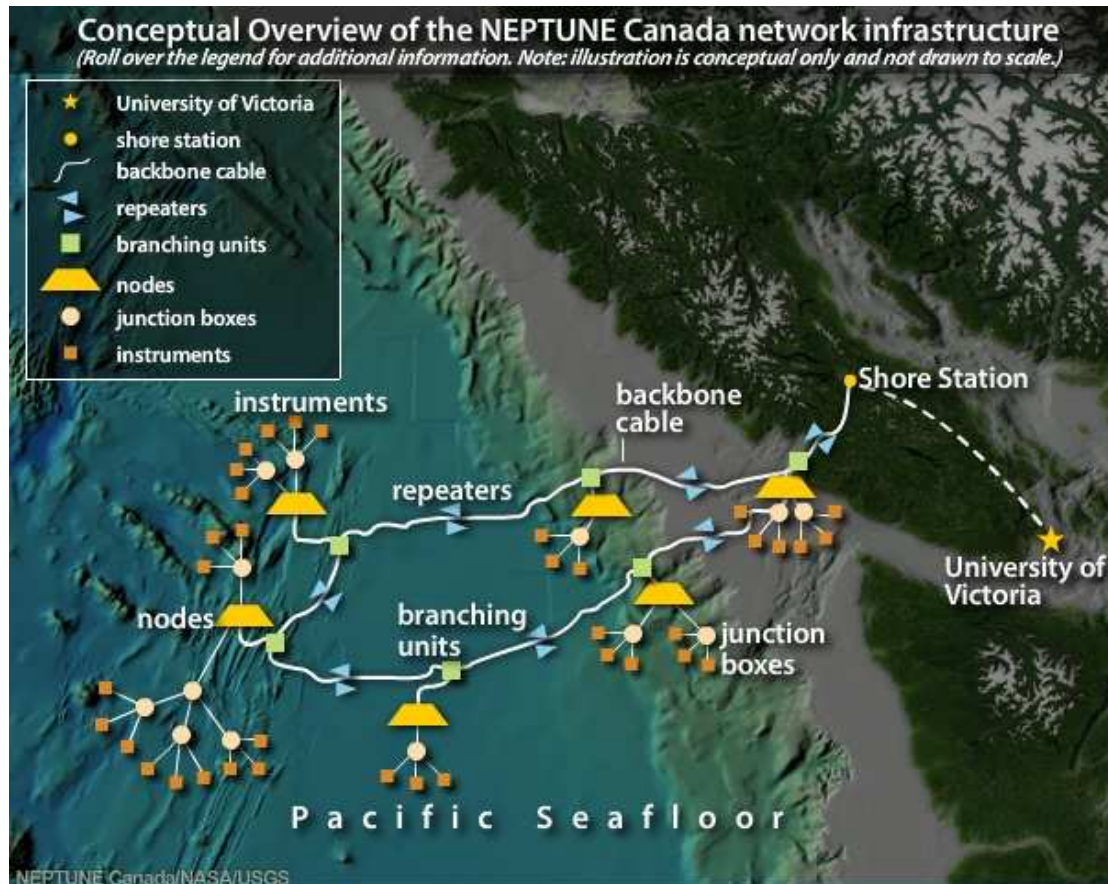


Why sound in a time series conference?

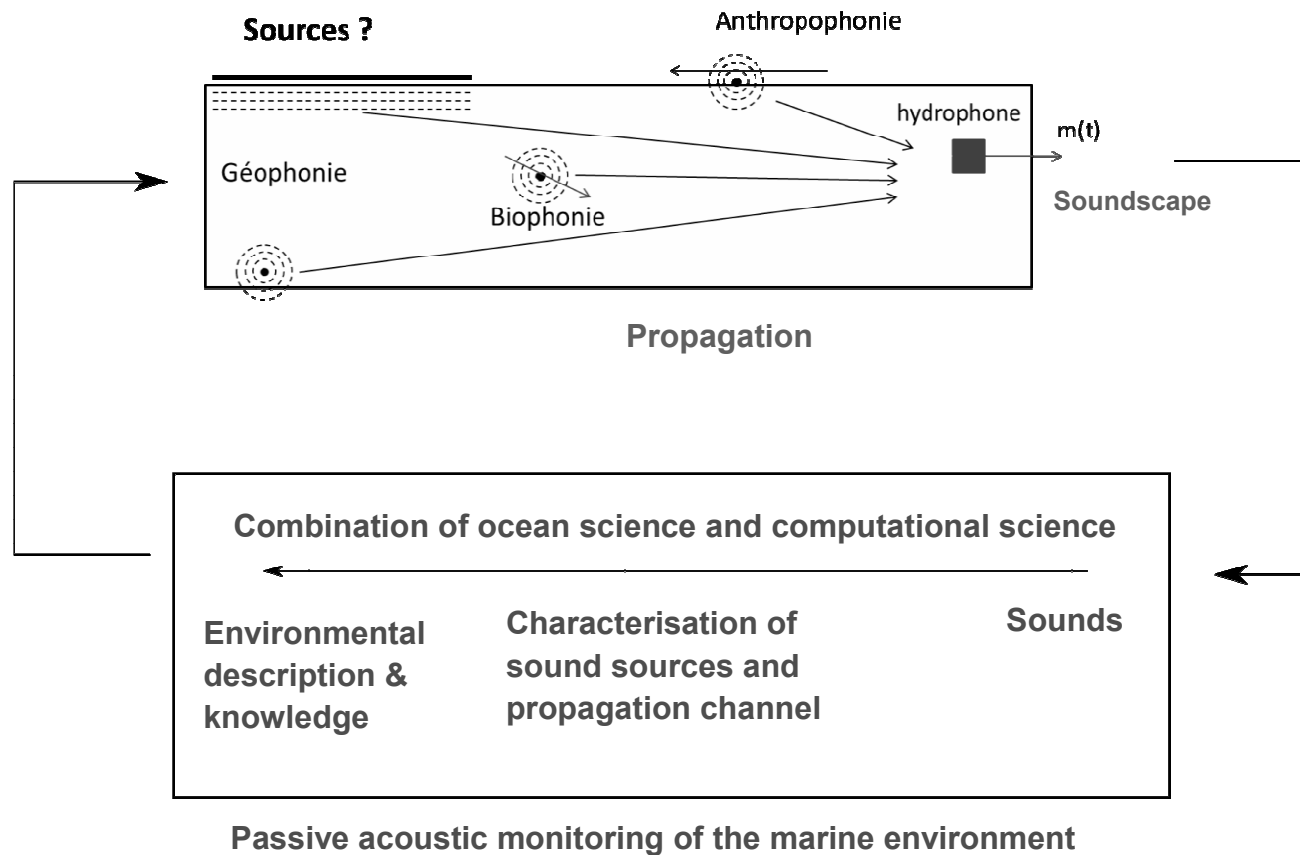
- Recent technological advances in sound acquisition
- Long-term monitoring,
- Continuous recordings,
- High resolution,
- Deployment in areas/substrates difficult to access,
- Relatively cost-effective,
- Real-time acquisition possible....



Why sound in a time series conference?



Why sound in a time series conference?



Passive acoustic monitoring = an indirect measurement that needs processing!

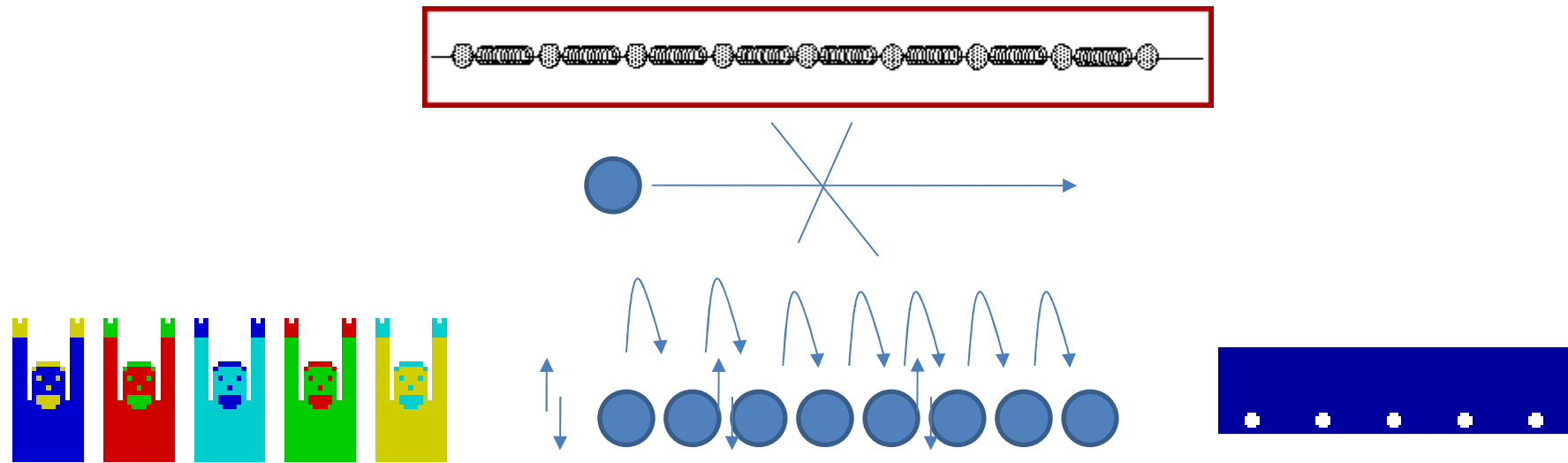
Outline

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- Applied examples from our own research

What is a wave ?

A mechanical WAVE



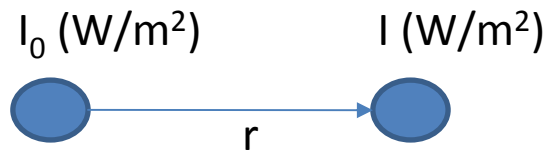
Initial information
Oscillation of a particle

Propagation of information
Transmission of oscillation

Different possible waves to explore the marine environment:

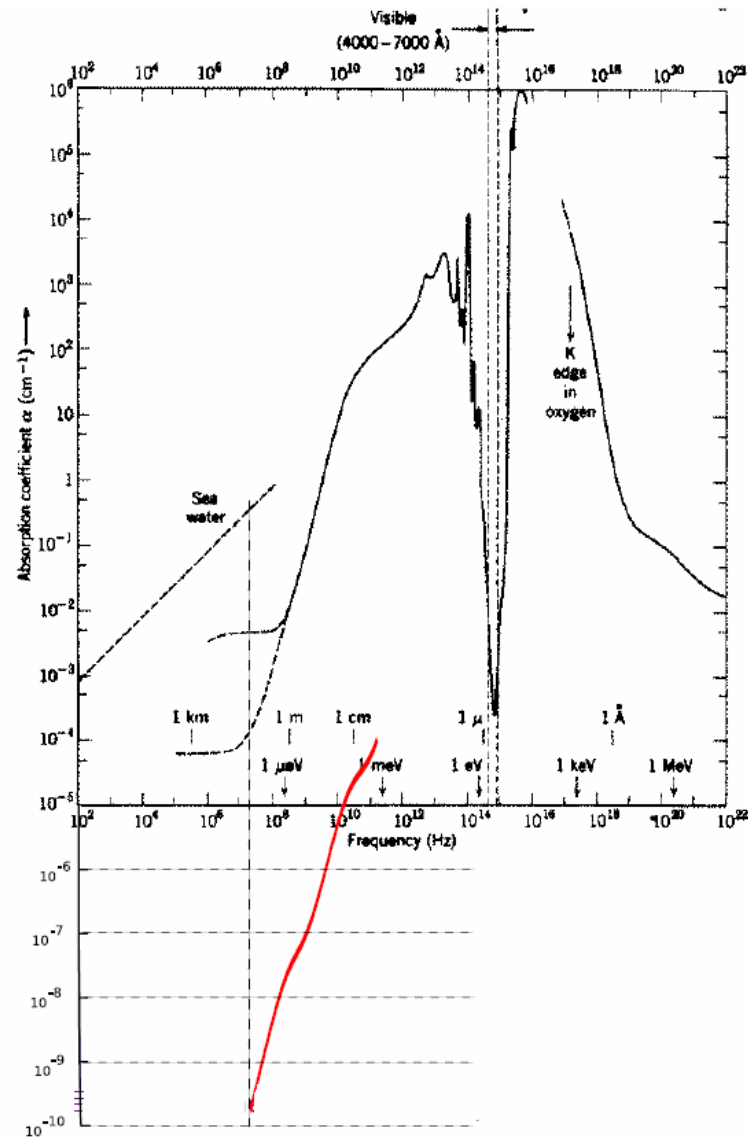
- electromagnetic
- optic
- acoustic

Why acoustic waves?

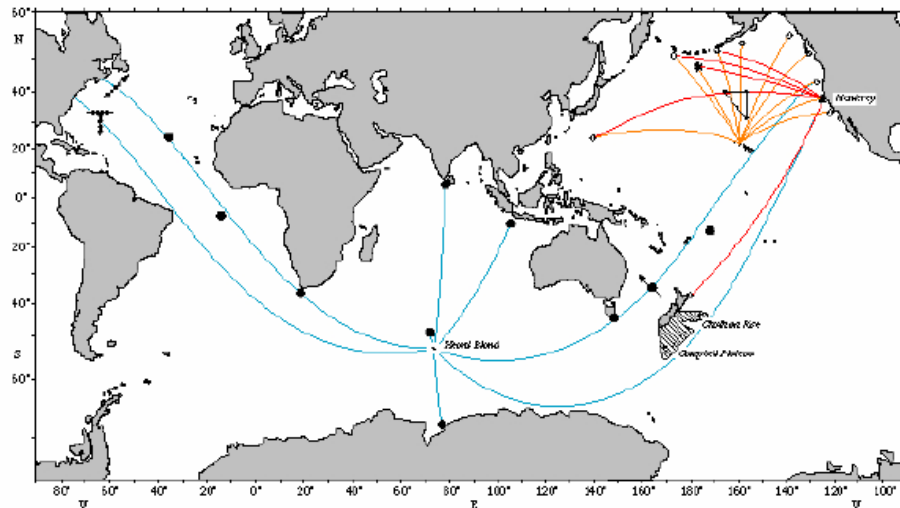


$$I(r) = I_0 e^{-\alpha r}$$

with α = coefficient of absorption (here in cm⁻¹)



Why acoustic waves?



— Heard Island Feasibility Test (HIPT) — ATOC (Pioneer Source)
— RTB87 — ATOC (Hawaii Source)

Frequency 50Hz, range 20000km!



Frequency 18Hz, range > 3000km

Frequency	10 Hz	100 Hz	1 kHz	10 kHz	100 kHz	1MHz
Absorption (dB/km)	$10^{-5}!!$	10^{-3}	0.06	1	33	300 !!
Range	>1000km		100 km	10 km	300m	25 m
Wavelength	150 m	15 m	1.5 m	15 cm	1.5 cm	15 mm



Munk, W.; Spindel, R.; Baggeroer, A. & Birdsall, T. (1994), 'The Heard Island Feasibility Test', *The Journal of the Acoustical Society of America* **96(4)**, 2330-2342.

Clark, C. W. & Gagnon, G. J. 2004. Low-frequency vocal behaviors of baleen whales in the North Atlantic: Insights from integrated Undersea Surveillance System detections, locations, and tracking from 1992 to 1996. *Journal of Underwater Acoustics (USN)*, **52**.



What is an acoustic wave ?

The equation of wave propagation is obtained from:

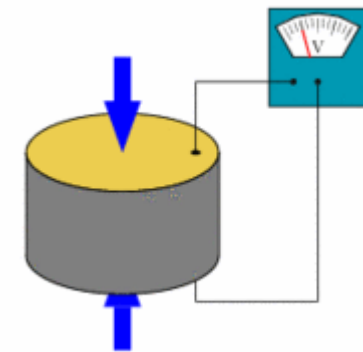
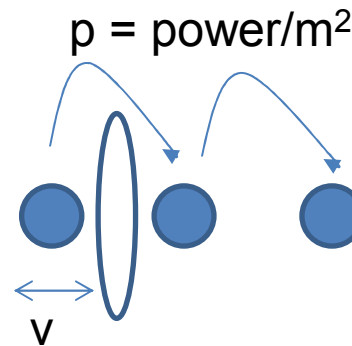
- the law of conservation of mass
- the law of conservation of momentum
- the law of fluid dynamics (linking P to ρ)

and from their 1st order linearization around the equilibrium pressure + $v=0\text{ms}^{-1}$

$$\Delta p - \frac{1}{c^2} \frac{\partial^2 p}{\partial t^2} = 0$$
$$\rho c^2 = p$$
$$\rho_0 \frac{\partial \vec{v}}{\partial t} + \vec{\nabla} p = 0$$

Wave equation

source

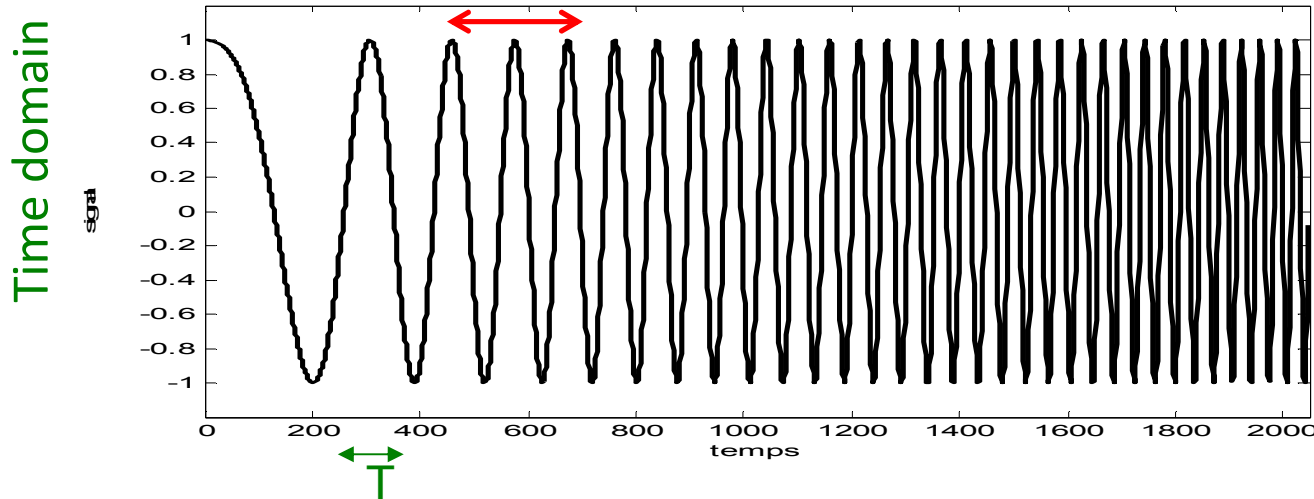


Piezo-electric receiver

Jensen, F. (1994), *Computational ocean acoustics*, Amer Inst of Physics.

What is a sound ?

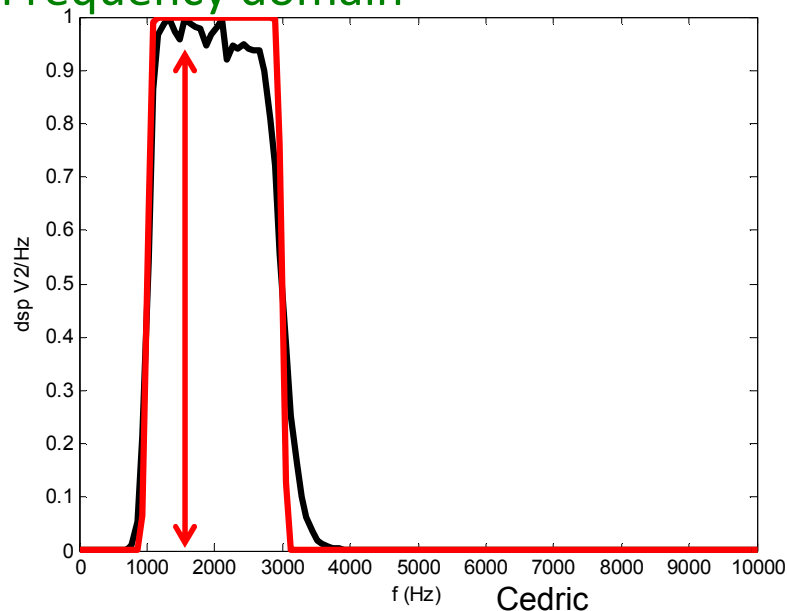
Level (received μPa , emitted $\mu\text{Pa}@1\text{m}$?) in decibel as a function of:



Sound intensity level:

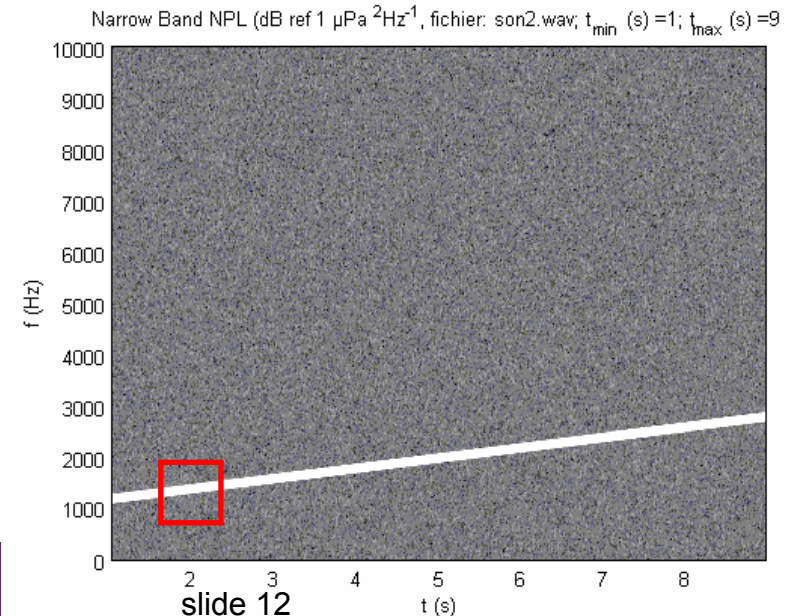
$$P_{|dB\text{re}P_0} = 10 \log_{10} \left(\frac{P}{P_0} \right)$$

Frequency domain



$$T = 1/f$$

Time-frequency



Sound speed

$$\Delta p - \frac{1}{c^2} \frac{\partial^2 p}{\partial t^2} = 0$$

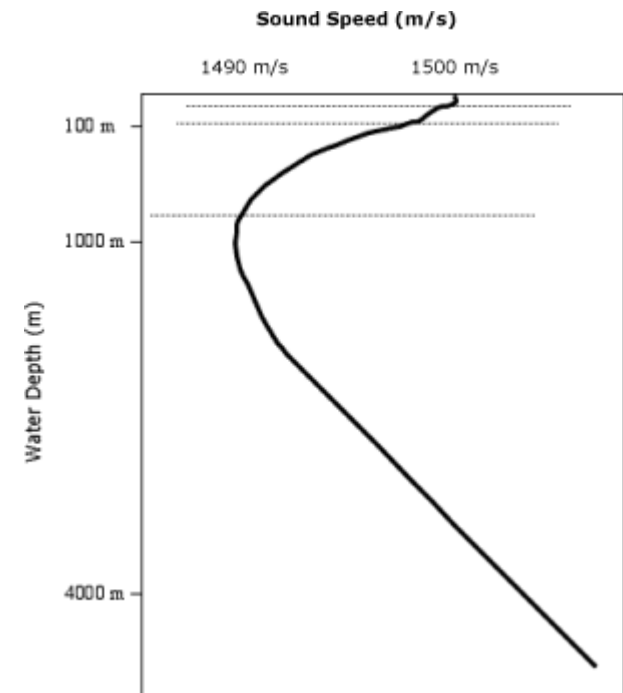
$$\rho c^2 = p$$

air, $c=330 \text{ ms}^{-1}$

water, $c=1500 \text{ ms}^{-1}$

rock, $c = 4000 \text{ ms}^{-1}$

Sea water sound velocity
 $c = G(T,p,S) = H(T,z,S)$



Take home message (for $T = 0^\circ\text{C}$ and $S = 35^\circ / \text{‰}$)

- c increases with T (4.6m/s for $\Delta T = 1^\circ\text{C}$)
- c increases with S (1.4m/s for $\Delta S = 1^\circ / \text{‰}$)
- c increases with p and z (1.7m/s for $\Delta S = 1000\text{m}$)



Sound speed

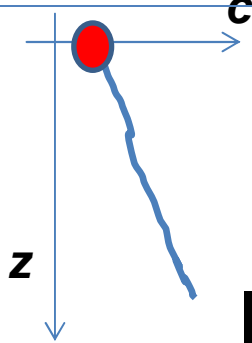
If sound velocity c changes with depth z , sound waves do not propagate on a straight line, they are refracted.

Sound waves always tend to converge towards the sound speed minimum.

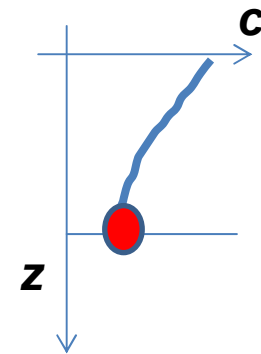


Sound speed

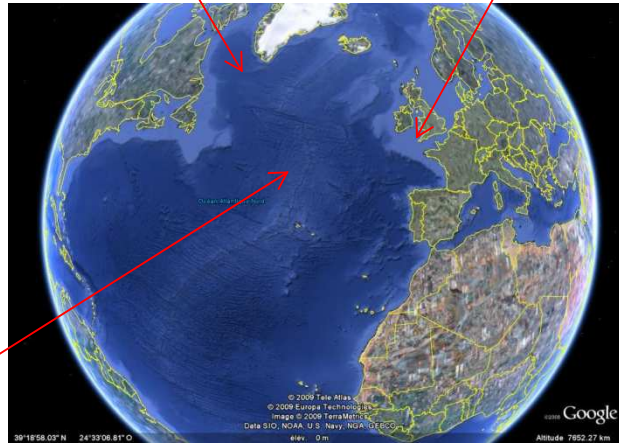
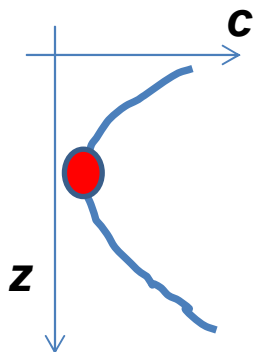
Polar profile



Shallow water / continental shelf profile

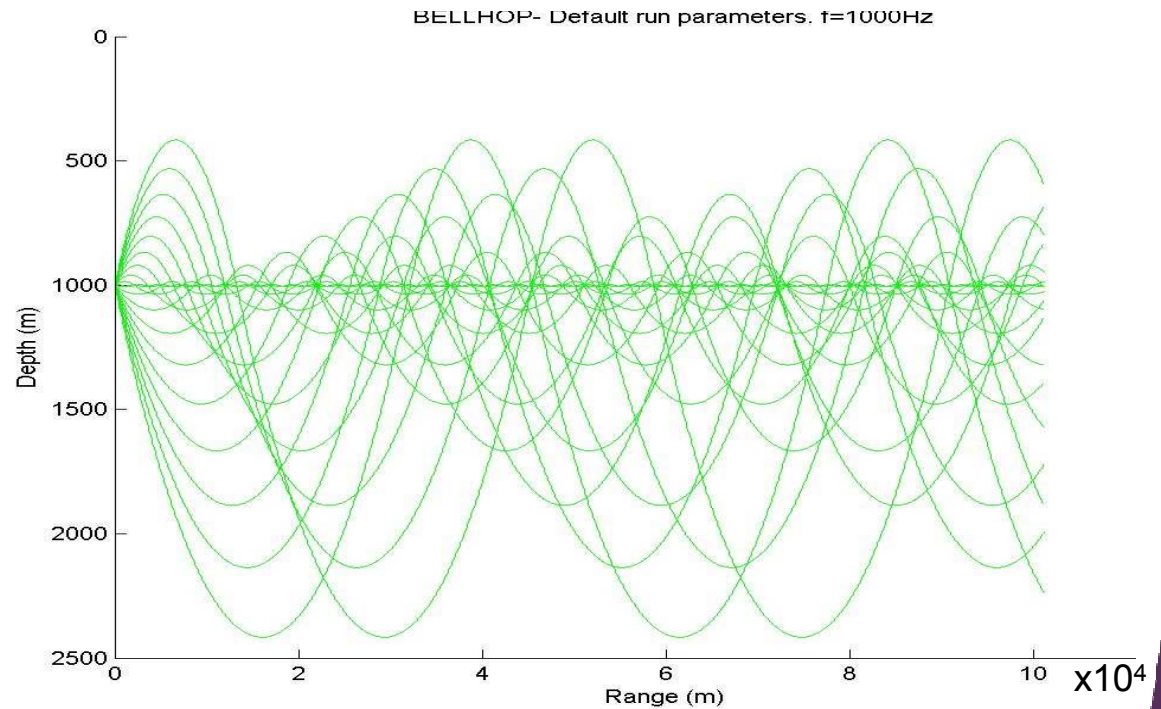
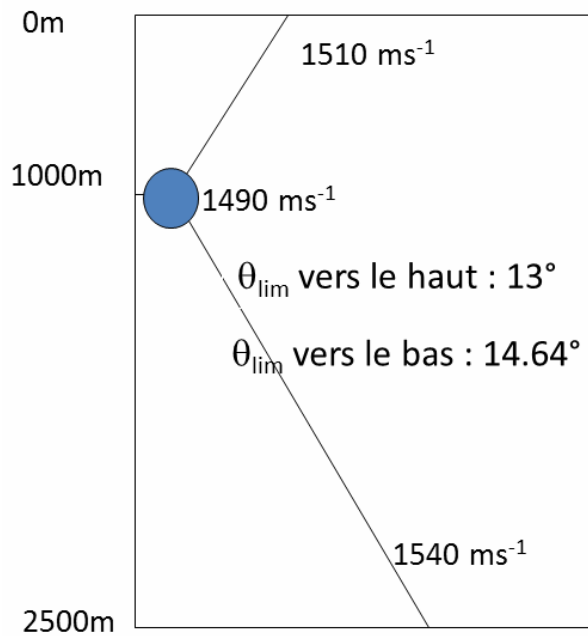


Deep water / temperate profile



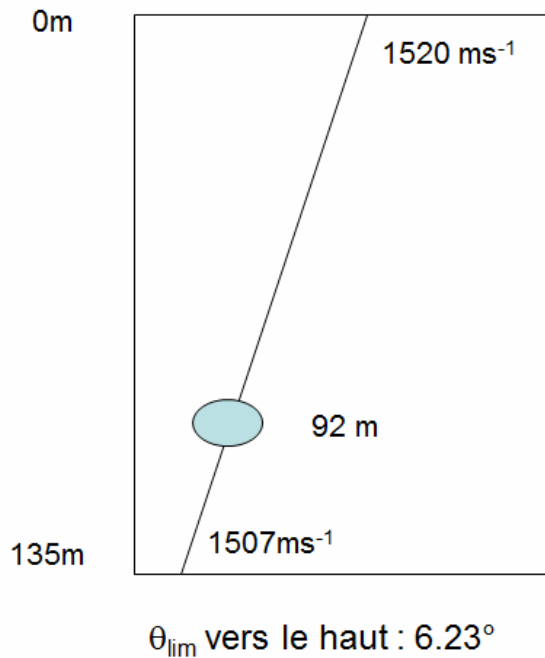
Temperate deep water sound propagation

Canal SOFAR « Sound Fixing & Ranging »

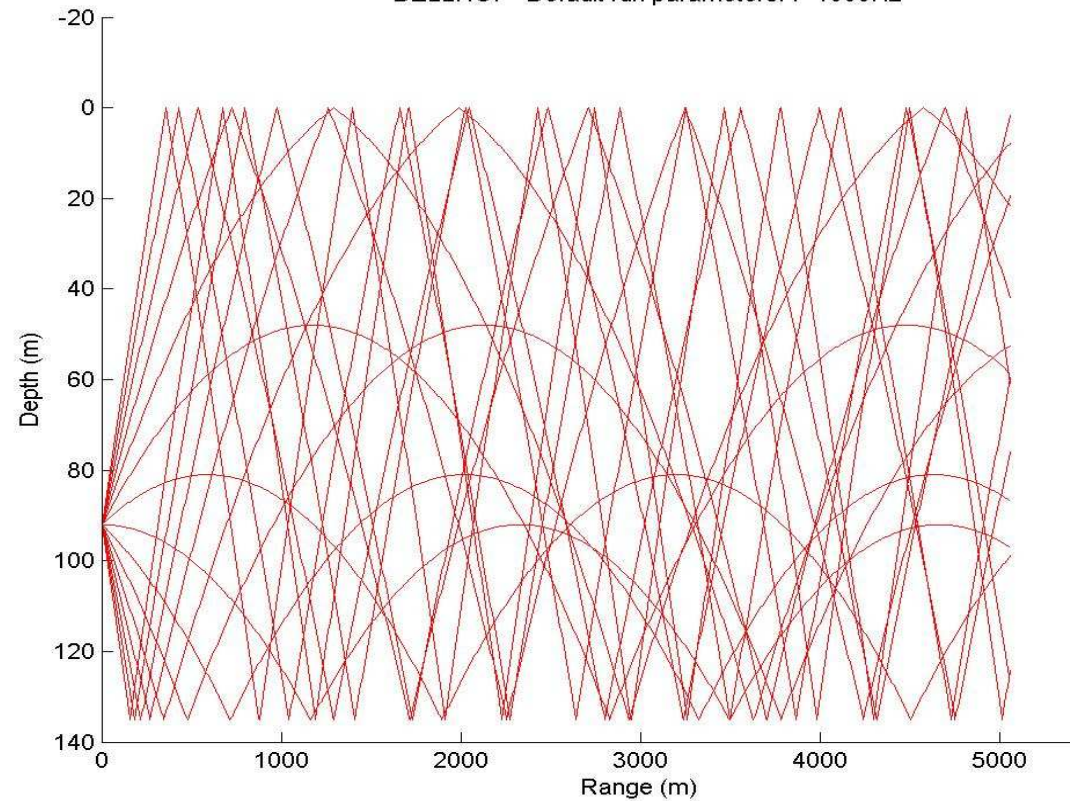


Temperate shallow water propagation

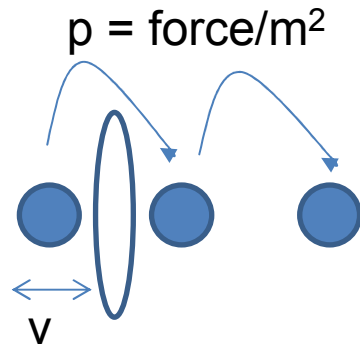
Shallow water – FARO - portugal



BELLHOP- Default run parameters. f=1000Hz



The intensity of sound



Power = strength x velocity

Intensity = amount of power transmitted through a unit area (m^2) =
pressure x speed
(W/m^2)

For planar waves :

$$I = \frac{p^2}{\rho c}$$

The intensity of sound

Example = sound wave with an amplitude of 1 Pa

In water: ($\rho=1000\text{kg/m}^2$; $c=1500\text{ms}^{-1}$) $\Rightarrow I_{\text{eau}} = 6.10^{-7}\text{W/m}^2$

In air: ($\rho=1.2\text{kg/m}^2$; $c=330\text{ms}^{-1}$) $\Rightarrow I_{\text{air}} = 2,5.10^{-3}\text{W/m}^2$

$I_{\text{air}} / I_{\text{eau}} = 4166$!!!!!!!!!!!!!

$$I = \frac{p^2}{\rho c}$$

Air : compressible gaz
Water : incompressible fluide



Decibels – unit of Sound (pressure) Level

J represents a quantity and J_{ref} a reference quantity

$$J \text{ dB (ref } \rightarrow J_{ref}) = 20 \log_{10} \left(\frac{J}{J_{ref}} \right) \text{ if } J \text{ is an amplitude}$$

$$J \text{ dB (ref } \rightarrow J_{ref}) = 10 \log_{10} \left(\frac{J}{J_{ref}} \right) \text{ if } J \text{ is an intensity}$$

Decibels are used to represent and compare amplitude quantities. The sound level in dB is a scale based on multiples of 10 (logarithmic scale):

10dB = $1 * 10^{-11}$ W/m² -> acoustic pressure increases 10 times

20dB = $1 * 10^{-10}$ W/m² -> acoustic pressure increases 100 times

40dB = $1 * 10^{-8}$ W/m² -> acoustic pressure increases 10000 times



Can Decibels be a source of confusion ?

Yes or No !

Two sounds with the following levels:

Son 1 : 100 dB ref 1 μ Pa

Son 2 : 100 dB ref 1 μ Pa²

Are the sound of equal amplitudes ?

Son 1 => ref 1 μ Pa, The quantity is an amplitude: $100 = 20 \log_{10} \left(\frac{p}{p_{ref}} \right)$ donc

$$\underline{p = p_{ref} \times 10^{100/20} = 10^5 p_{ref}}$$

Son 2 => ref 1 μ Pa²

remember $Q = \frac{p^2}{\rho c}$ The quantity is an intensity:

$$100 = 10 \log_{10} \left(\frac{I}{I_{ref}} \right)$$

$$I = I_{ref} \times 10^{100/10}$$

$$I \sim p^2$$

Donc

$$p^2 = p_{ref}^2 \times 10^{100/10}$$

$$\underline{p = p_{ref} \times 10^{100/20} = 10^5 p_{ref}}$$



Can Decibels be a source of confusion ?

Yes or No !

- The sound level in dB of a sum of acoustic signals is not equal to the sum of the sound levels of each signal !!!!!!!!!!!!!!!

- Two independent sounds => intensity of the sum = sum of the intensities in a **linear** scale:

- Son 1 : Q_1 dB , son 2: Q_2 dB, et soit $son_3 = son_1 + son_2$ (*son = sound*)

$$I_{son_3} = I_{son_1} + I_{son_2}$$
$$I_{son_3} = 10^{Q_1/10} + 10^{Q_2/10}$$
$$I_{son_3} dB = 10 \times \log_{10}(10^{Q_1/10} + 10^{Q_2/10})$$

- Si $Q_1 = Q_2 = 100$ dB then $I_{son_3} dB = Q_1 dB + 3 = 103$ dB
- Si $Q_1 = 100$ dB, $Q_2 = 90$ dB then $I_{son_3} dB = 100.41$ dB

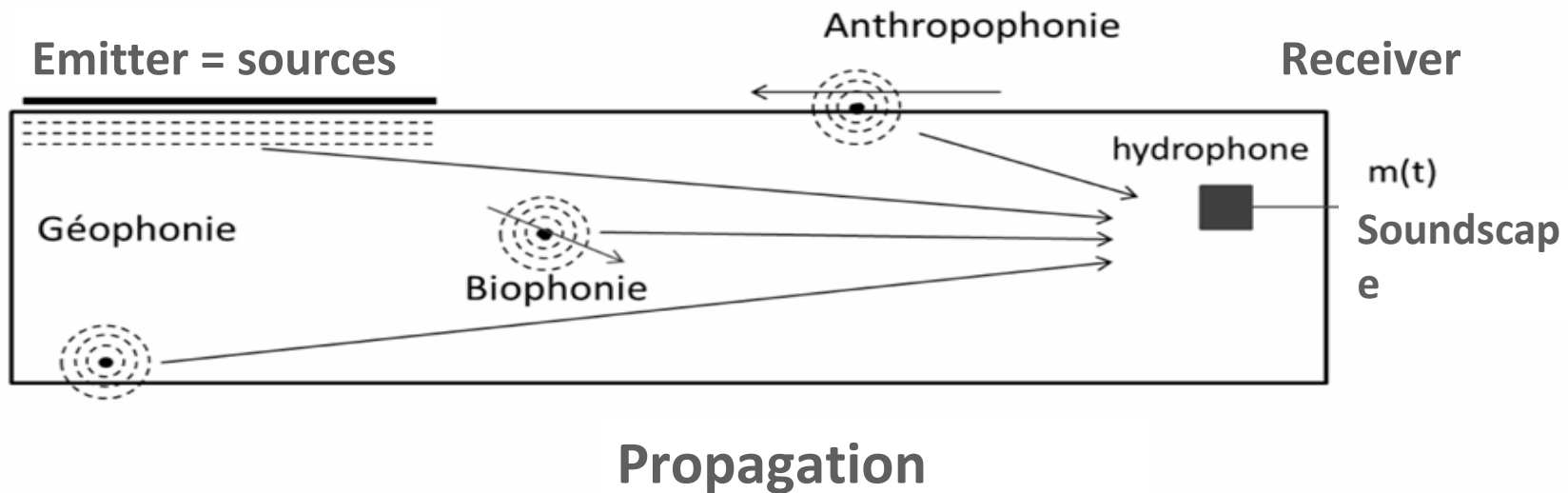
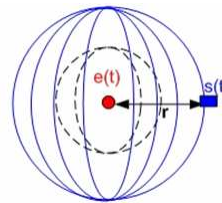


Source Level & Reveived Level

Source Level
SL dB re
 $1\mu\text{Pa}^2$ @ 1m.....

Level heard if @ 1m form an
isotropic source

Received Level
RL dB ref
 $1\mu\text{Pa}^2$



Acoustic intensity :

The energetic budget of a singing blue whale

Mean source level of blue whale song note: 160 dB re 1 μ Pa @ 1m (188 dB peak), signal duration = 18s with 960 signals/day, energetic value of krill = 96kcal/100g.

Biophony

From invertebrates...



Range

1m - > 200m



10m - > 1km



> 100m - > 1000km

... to marine mammals

Geophony

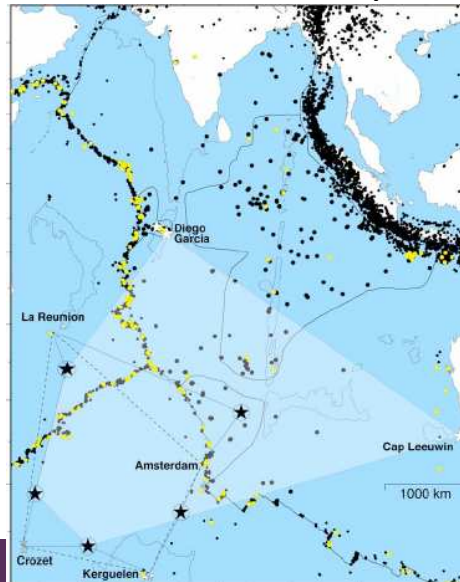
Wind & rain



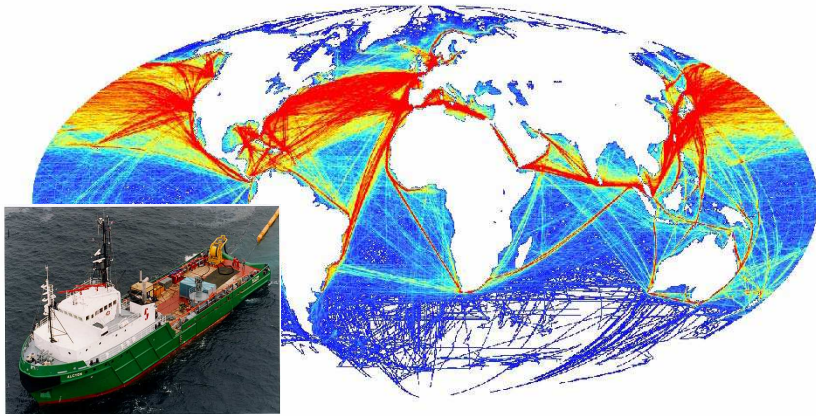
Sounds of breaking ice



Underwater earthquake



Anthropophony

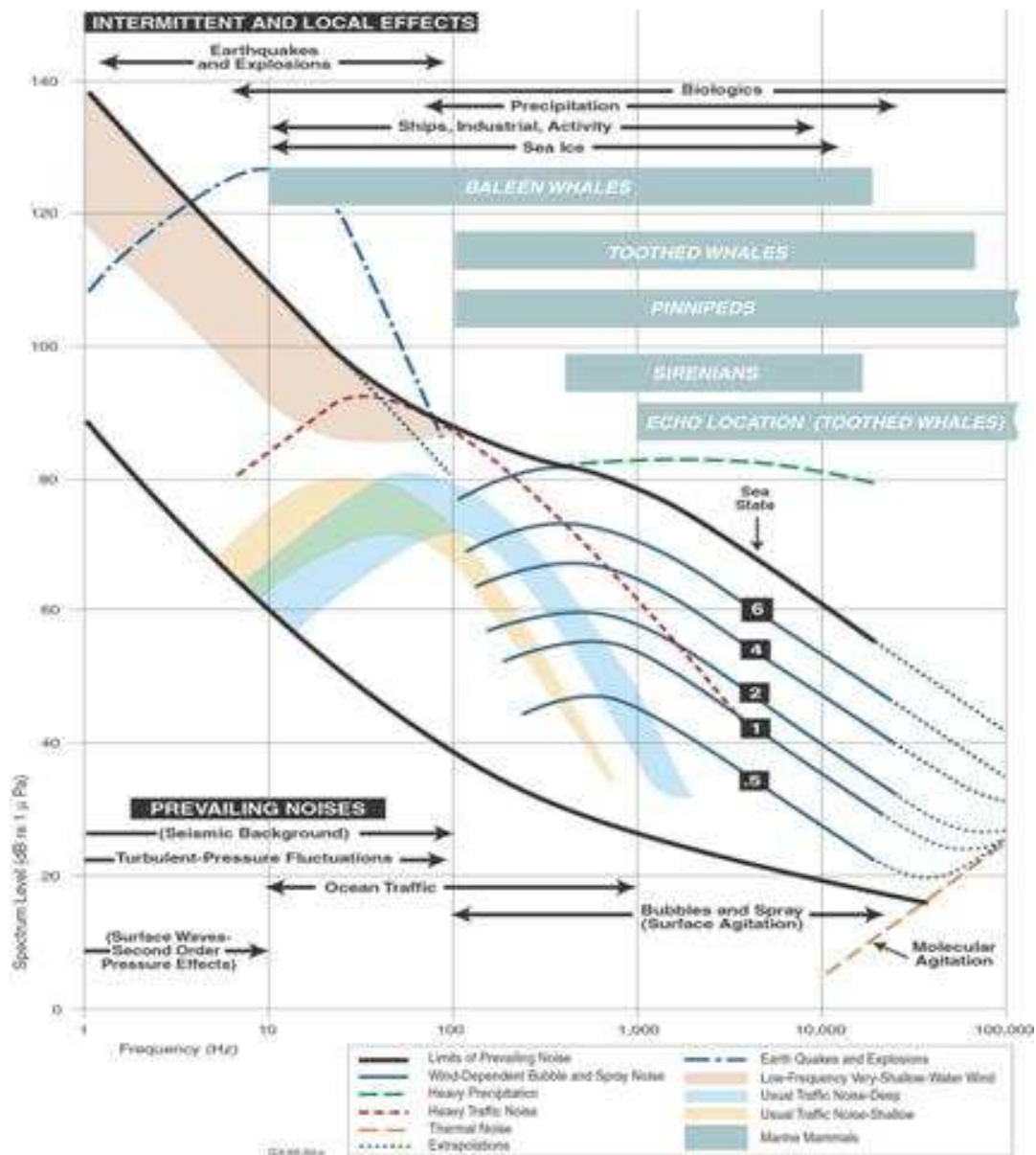


Sound Levels

Source (SL)	Mesure (RL)
<p>Wideband effective source level (SL),</p> $SL = 10 \log_{10}(rl); \text{ dBref } 1\mu\text{Pa}^2 @ 1\text{m}$ $sl = \frac{1}{T} \int_T m(t)^2 dt$	<p>Wideband effective received level (RL),</p> $RL = 10 \log_{10}(rl); \text{ dBref } 1\mu\text{Pa}^2$ $rl = \frac{1}{T} \int_T m(t)^2 dt$
<p>Narrowband source level Power spectral density</p> $\gamma_{SL}(f) = \text{dBref } 1\mu\text{Pa}^2 / \text{Hz} @ 1\text{m}$	<p>Narrowband received level Power spectral density</p> $\gamma_{RL}(f) = \text{dBref } 1\mu\text{Pa}^2 / \text{Hz}$
	<p>Sound exposure level (SEL)</p> $SEL = 10 \log_{10}(sel); \text{ dBref } 1\mu\text{Pa}^2\text{s}$ $sel = \int_T m(t)^2 dt$



An inventory
initiated by 2nd
world war and cold
war

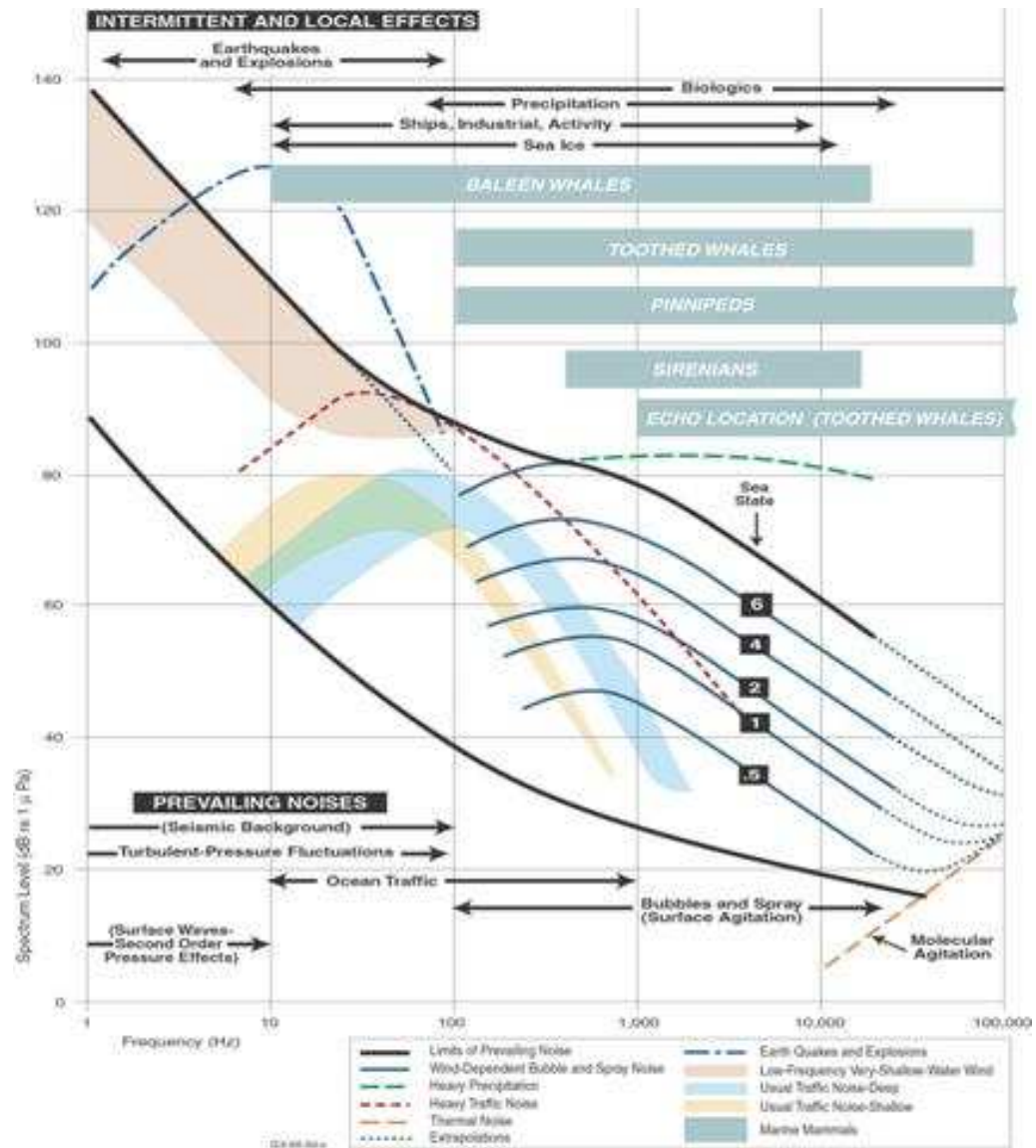


Source whoi.edu, Wenz 1962, Wenz 1972, Urick 1984

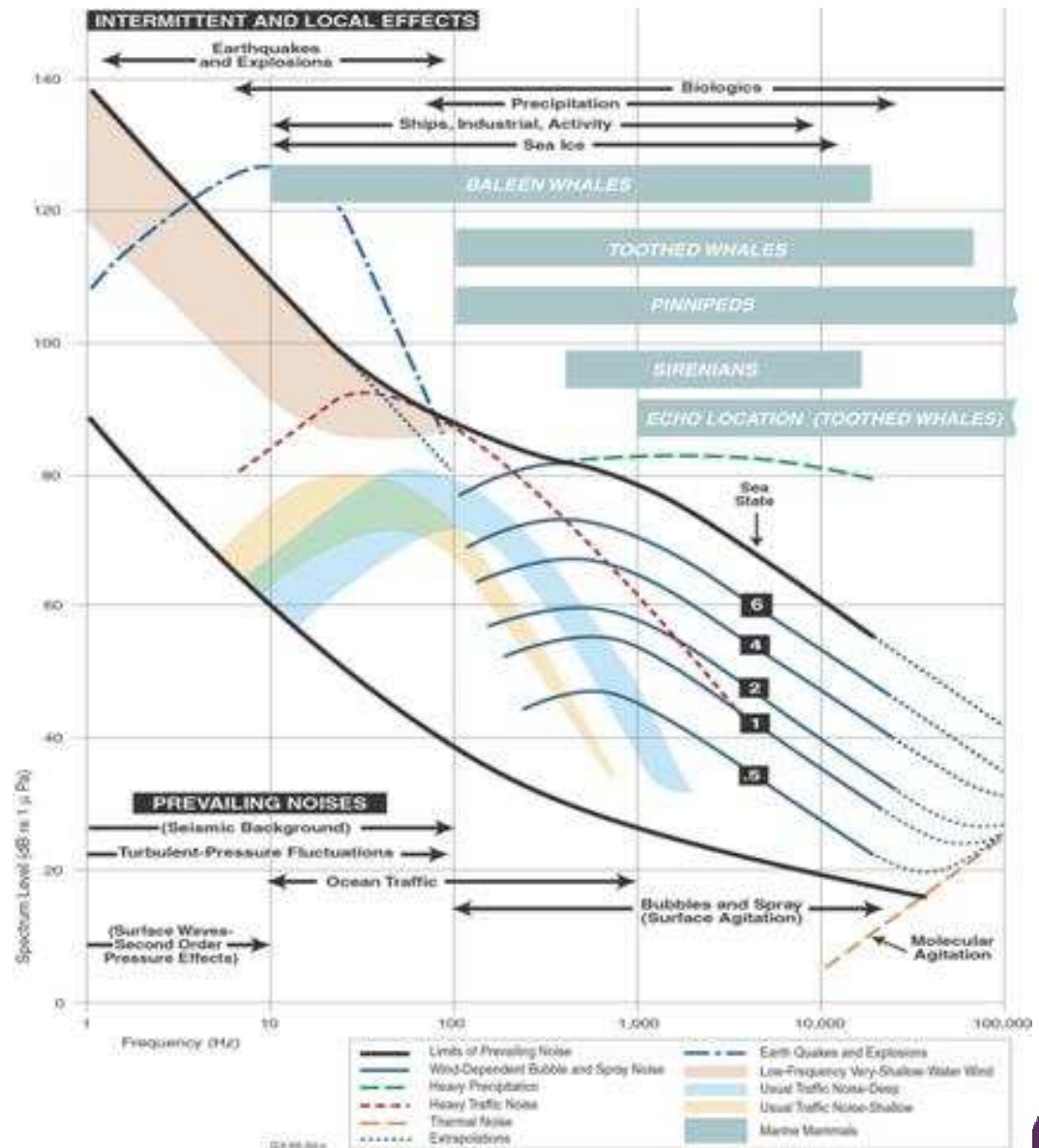


Natural sources
Abiotic
Biotic

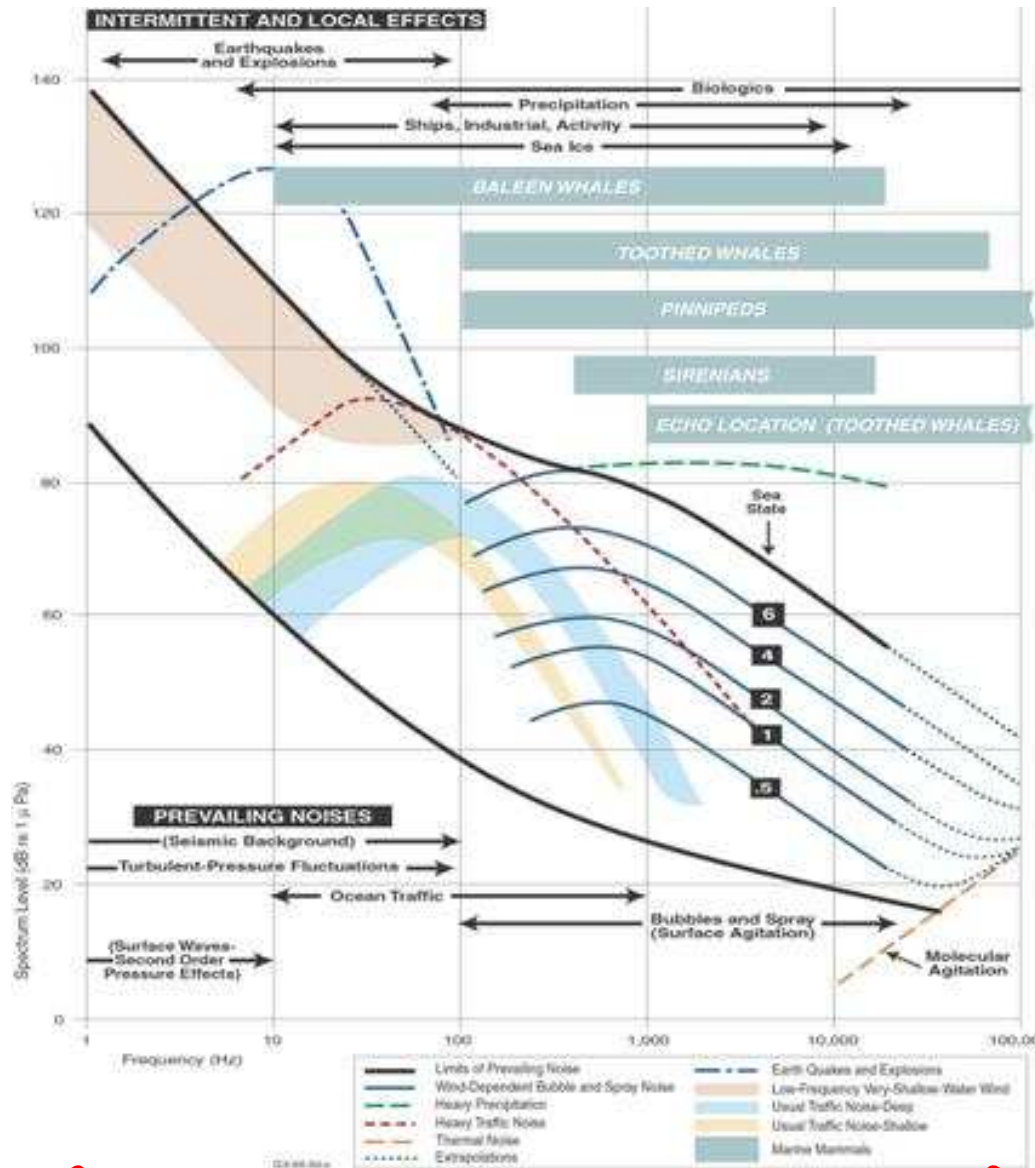
Anthropogenic
sources



Ambient noise
 Background noise
 from many different
 sources excluding
 individually
 identifiable sounds



Very large amplitude dynamic



Very large frequency dynamic



Hildebrand, J. (2009), 'Anthropogenic and natural sources of ambient noise in the ocean', Marine Ecology Progress Series 395, 5--20.

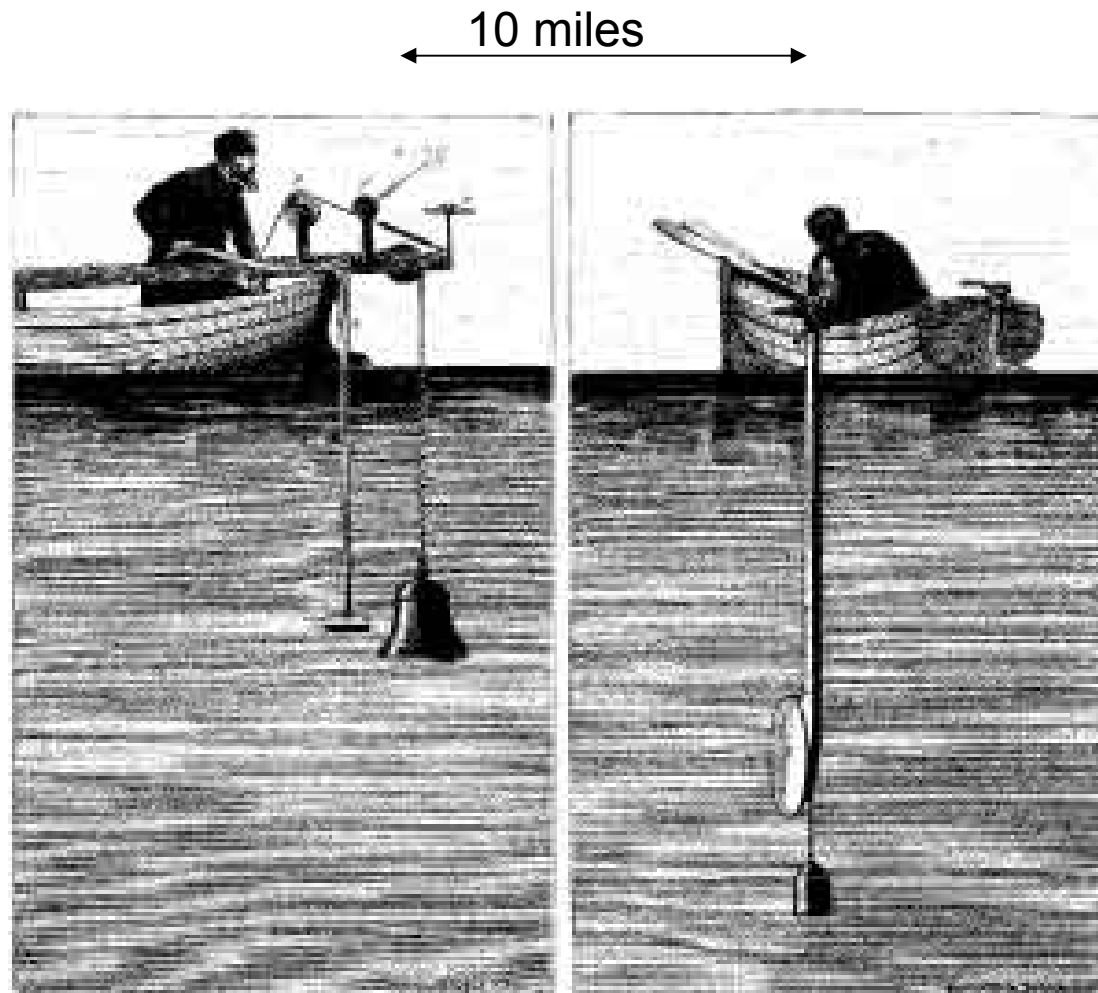
Wenz, G. (1972), 'Review of underwater acoustics research: Noise', The Journal of the Acoustical Society of America 51, 1010.

Wenz, G. M. (1962), 'Acoustic Ambient Noise in the Ocean: Spectra and Sources', The Journal of the Acoustical Society of America 34(12), 1936-1956.

Outline

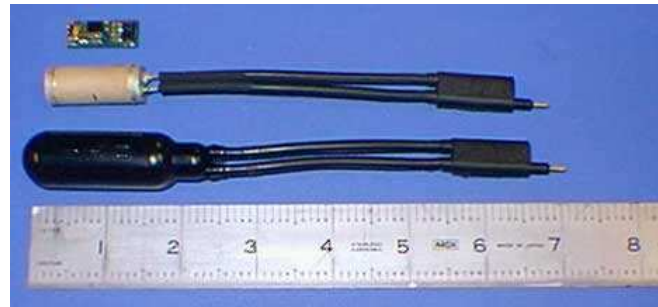
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Some measurement devices



1826, lake of Geneva: Calladon & Strum

Some measurement devices



Portable device



Hydrophone

Amplifier



IN

OUT



IN

Recorder



Some measurement devices

Autonomous recorders



Aural, Multi-Electronique, Qc.



RT SYS, France

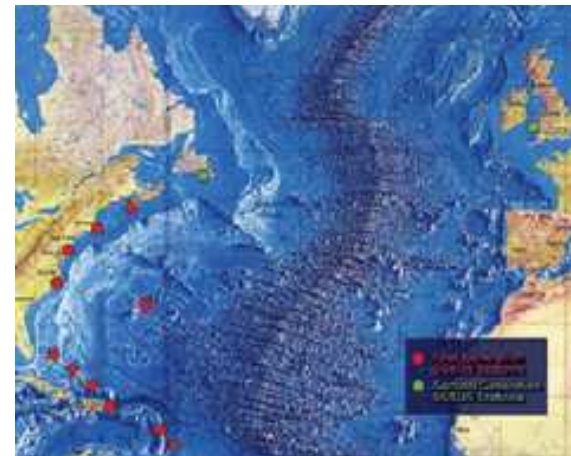
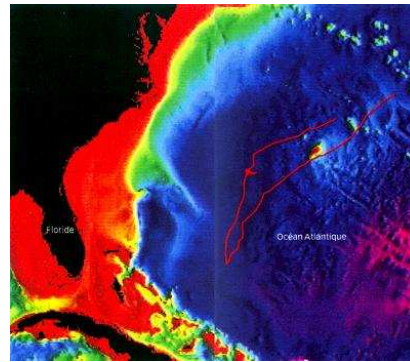
Some measurement devices

Cabled systems

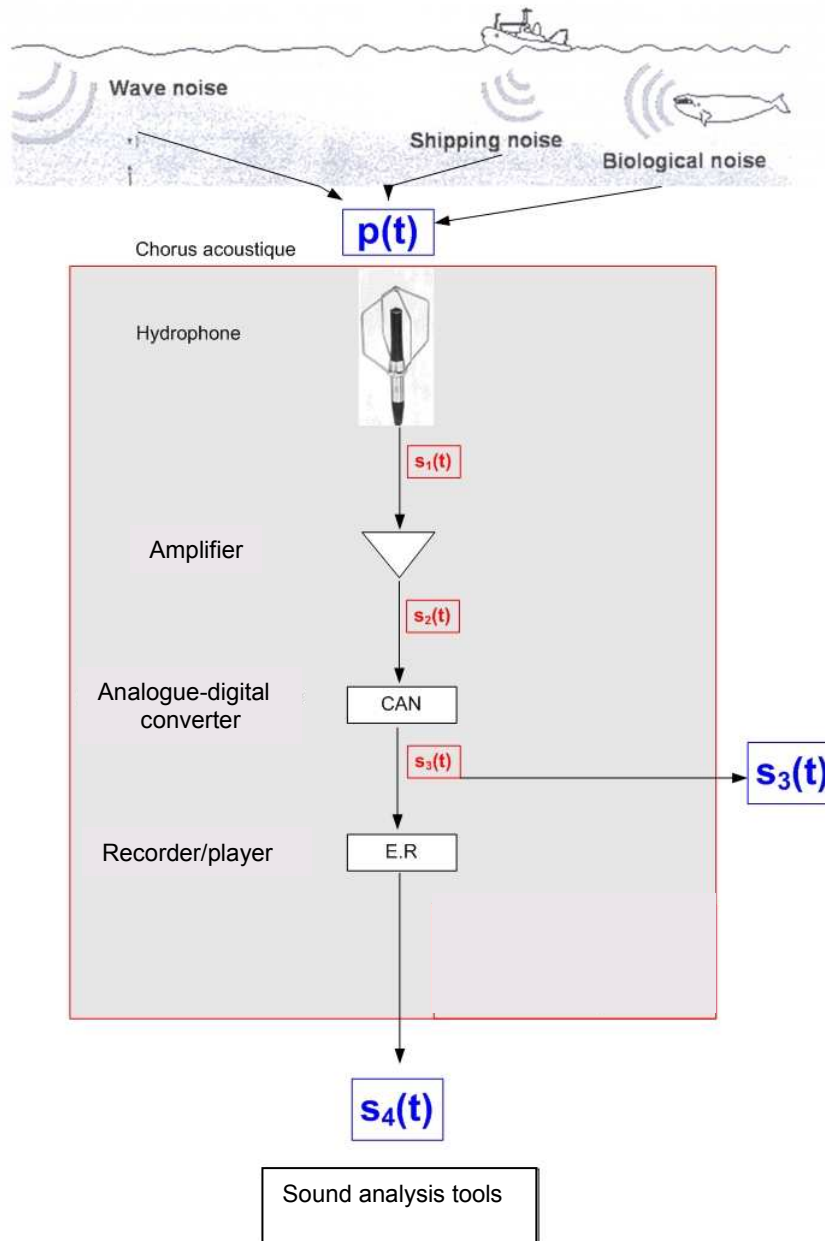
<http://www.medon.info/>



SOUND SURVEILLANCE SYSTEM



The elements of the acquisition chain



$$|s_1| = 10^{\frac{RS}{20}} |p|$$

$$|s_1|_{dB} = |p|_{dB} + RS$$

$$|s_2| = 10^{\frac{G}{20}} |s_1|$$

$$|s_2|_{dB} = |s_1|_{dB} + G$$

$$|s_3| = E\left(\frac{|s_2|}{D} 2^{nb-1}\right)$$

$$|s_3|_{dB} = |s_2|_{dB} + 20 \log_{10}\left(\frac{2^{nb-1}}{D}\right)$$

Receiver sensitivity

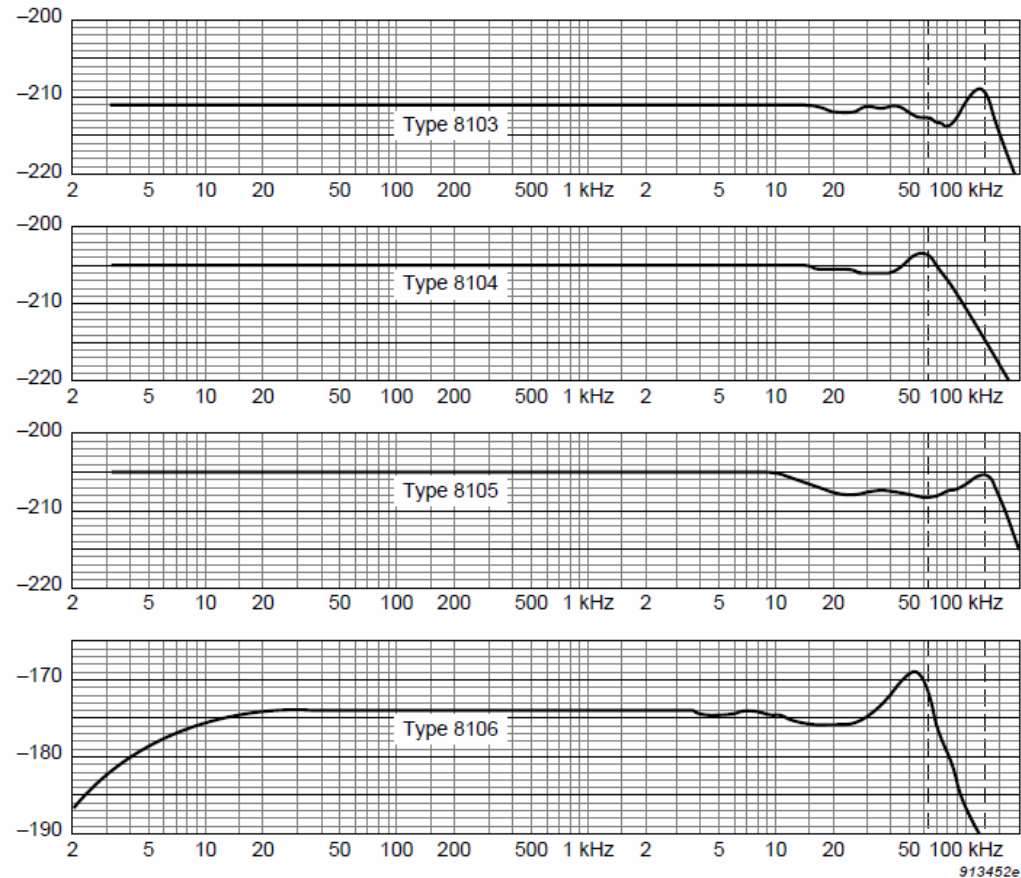


Fig.5 Typical receiving frequency characteristics of Hydrophones Types 8103, 8104, 8105 and 8106 (dB re 1V/ μ Pa)

RS dB ref 1V / 1μ Pa

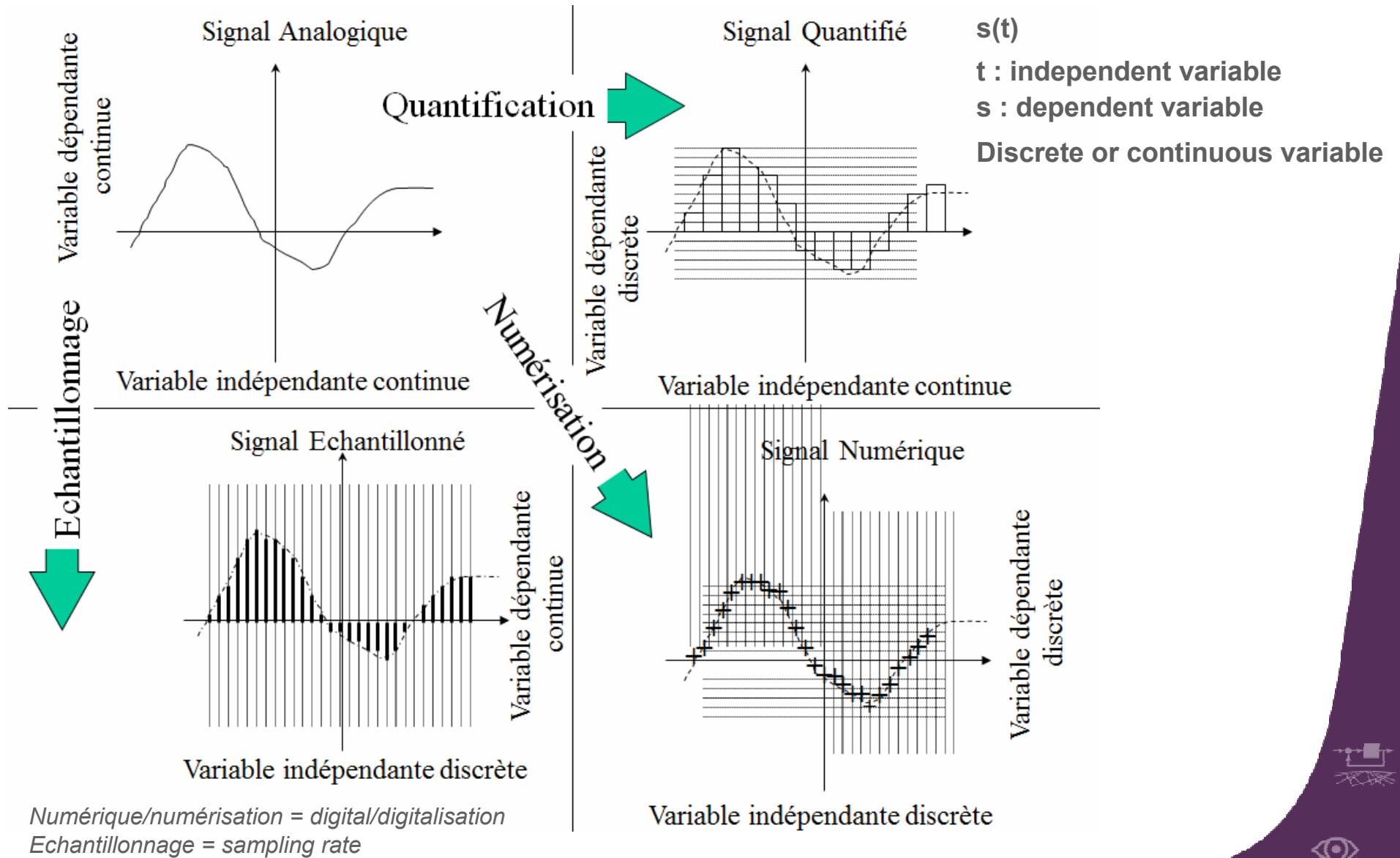


A key element : the analogue to digital conversion

It allows the use of digital technology to process the acquired data.



The analogue to digital conversion



Sampling rate

f_{\max} is the maximal frequency of a signal $s(t)$
only if

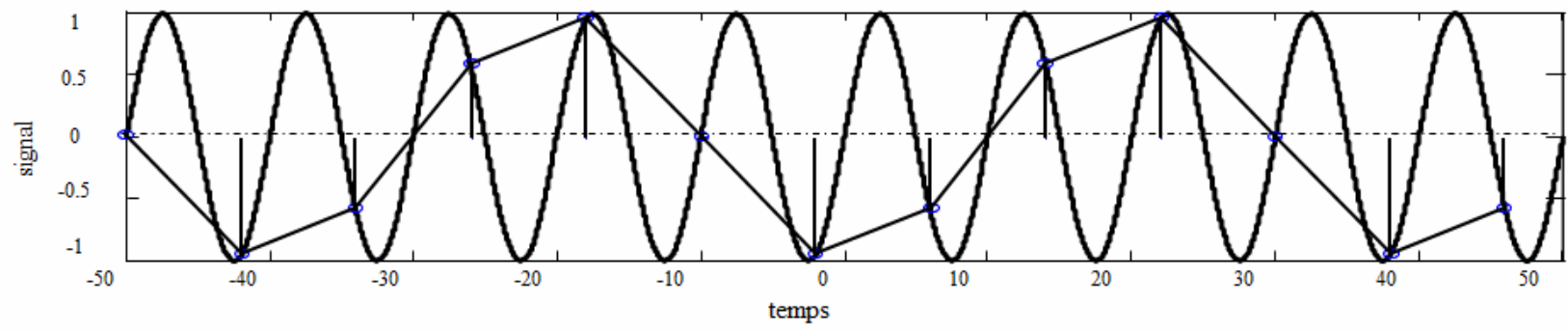
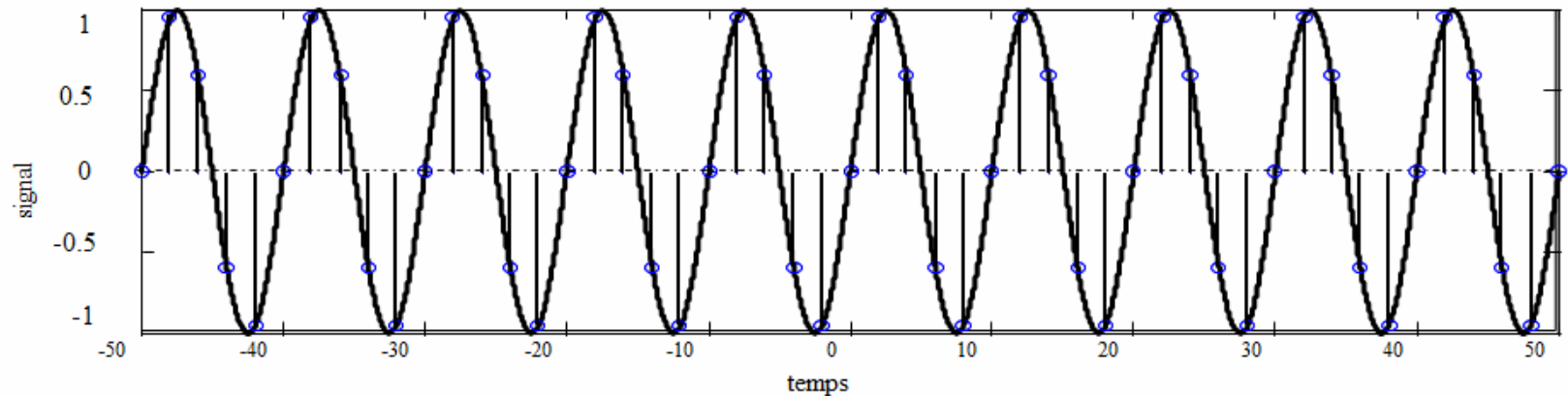
$$\forall f > f_{\max}, S(f) = 0$$

The sampling of a signal $s(t)$ **is reversible**
only if
 $s(t)$ is low-pass
and
 $f_e > 2f_{\max}$



Sampling rate

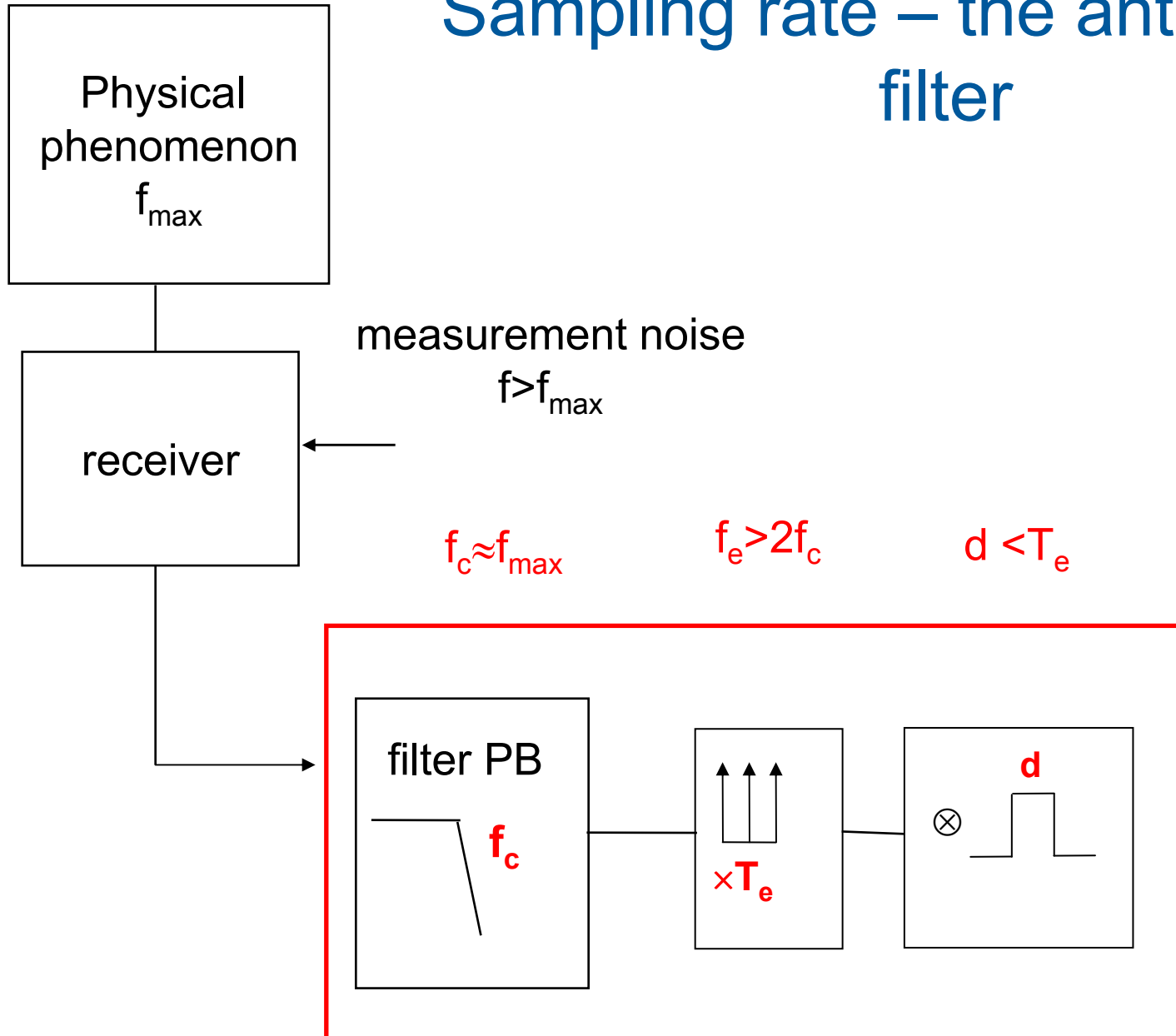
Shannon:cool



pas Shannon:pas cool



Sampling rate – the anti aliasing filter

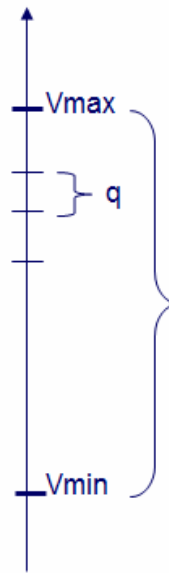


Quantification

The 3 key parameters:

- V_{min}
- V_{max}
- Number of quantification levels N

$$E_p = \{V/\exists k \in (0, 1, \dots, N-1), V = \frac{k}{N-1}(V_{max}-V_{min})+V_{min}\}$$



D : dynamic range

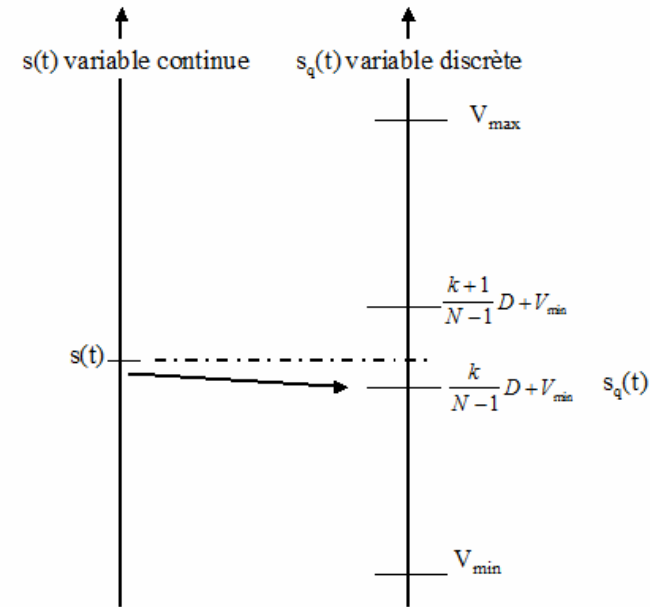
$$D = V_{max} - V_{min}$$

q : quantification step

$$q = \frac{V_{max} - V_{min}}{N - 1}$$

b : number of bits

$$N = 2^b$$



Quantification rule: :

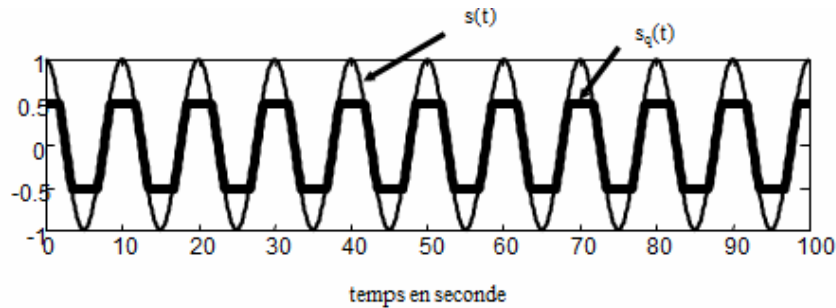
$$s_q(t) = \arg \min_{V \in E_p} |s(t) - V|$$



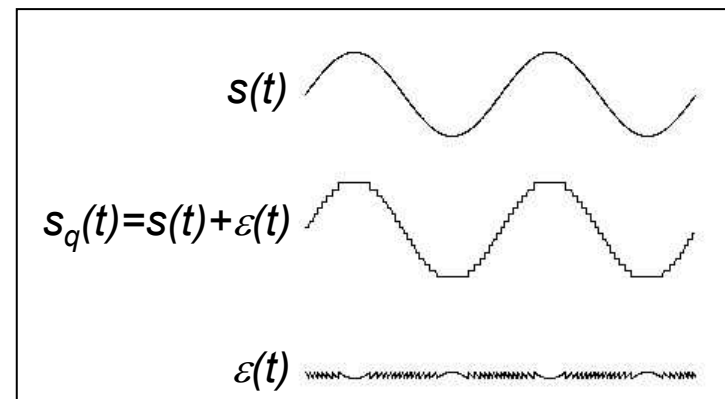
Quantification errors

$$s_q(t) = s(t) + \epsilon(t)$$

Saturation



Discretization

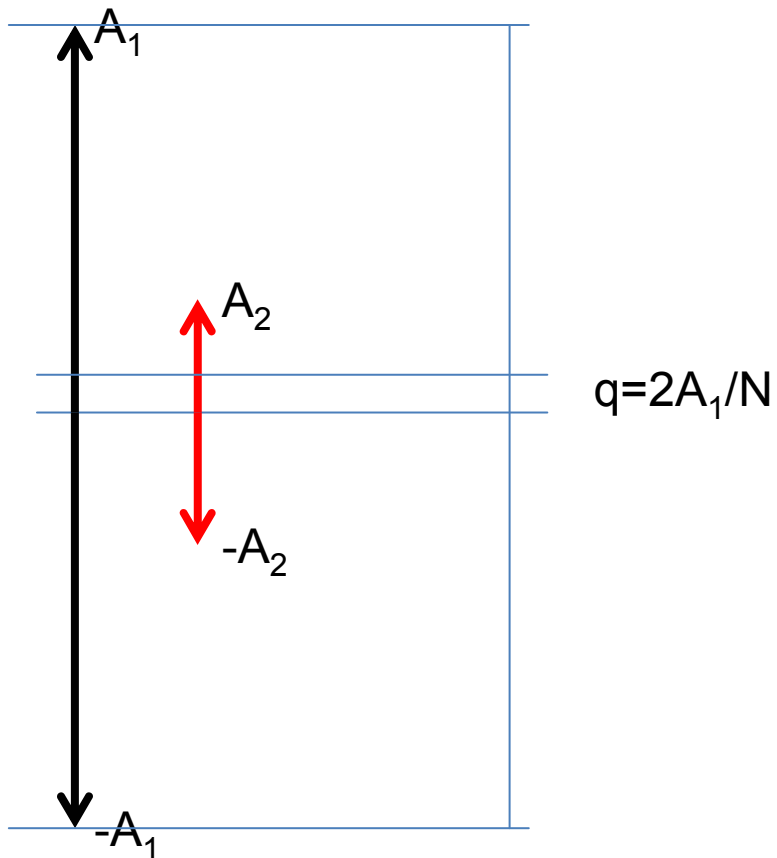


The quantification error ϵ : $\mathbf{s(t)} \in [\mathbf{Vmin}, \mathbf{Vmax}]$

- $\epsilon(t)$ limited $\in [-q/2, q/2]$
- Evenly distributed over $[-q/2, q/2]$
- $E(\epsilon(t)) = 0$ $E(\epsilon^2(t)) = \frac{q^2}{12}$
- $\epsilon(t)$ white noise \rightarrow constant spectral component **istante** high frequencies

How to set a quantification chain?

Case: need to measure two signals: an intense (amplitude A_1) and a low one (amplitude A_2)

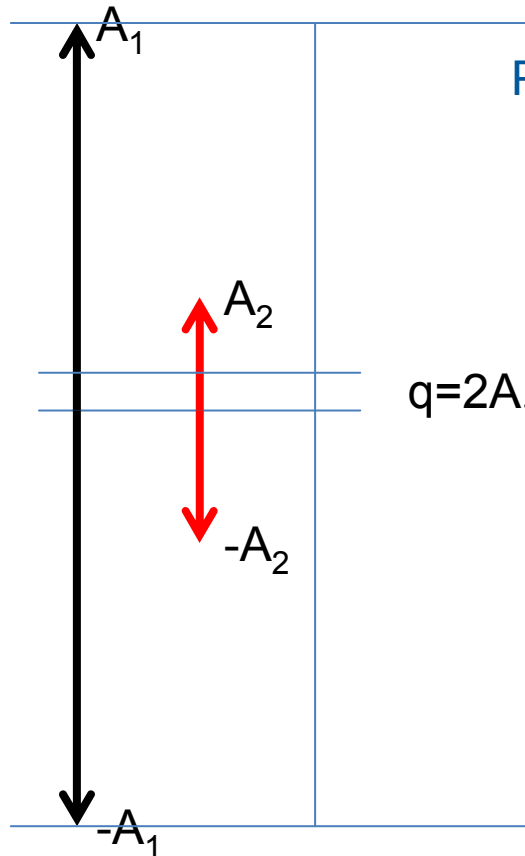


Choose V_{min} , V_{max} , N in order to :

- 1) Avoid saturation of the intense signal
- 2) Record the faint signal with a minimal signal to noise ratio (so that it is audible)

Choose V_{min} , V_{max} , N in order to :

- 1) Avoid saturation of the intense signal
- 2) Record the faint signal with a minimal signal to noise ratio (SNR)



Procedure to estimate quantification N

- $V_{max} = -V_{min} = A_1$
- $q = \frac{2A_1}{N}$
- $RSB_2 = \frac{(A_2)^2}{q^2/12}$
- $RSB_2 = 3N^2 \frac{(A_2)^2}{(A_1)^2}$
- $RSB_2 dB + 10 \log_{10} \left(\frac{(A_2)^2}{(A_1)^2} \right) - 10 \log_{10}(3) = 20 \log_{10}(N)$
- $RSB_2 dB + 10 \log_{10} \left(\frac{(A_2)^2}{(A_1)^2} \right) - 4 = 7 \log_2(N)$

$RSB = SNR$

$N = \text{quantification}$

Example

Calculate the parameters of a measurement chain that allows to record dolphin whistles at 1000 meters of the hydrophone and simultaneously ship noise at 100 meters. SNR of dolphin signals = 20dB.

Sampling rate: Low-frequency ship noise, dolphin whistles (frequency range: few kHz to 30 kHz) $\Rightarrow f_s > 60\text{kHz}$; we choose $f_s = 96\text{kHz}$

Quantification:

-Intense signal: shipping noise $\Rightarrow (180\text{dB re } 1\mu\text{Pa}^2/\text{Hz}@1\text{m around } f_0=50\text{Hz, spherical transmission loss } -20\log_{10}(f) \Rightarrow 156\text{dB re } 1\mu\text{Pa}^2$

- Faint signal: dolphin whistle $\Rightarrow (110 \text{ dB re } 1\mu\text{Pa}@1\text{m, spherical transmission loss}) \Rightarrow 50\text{dB}$.

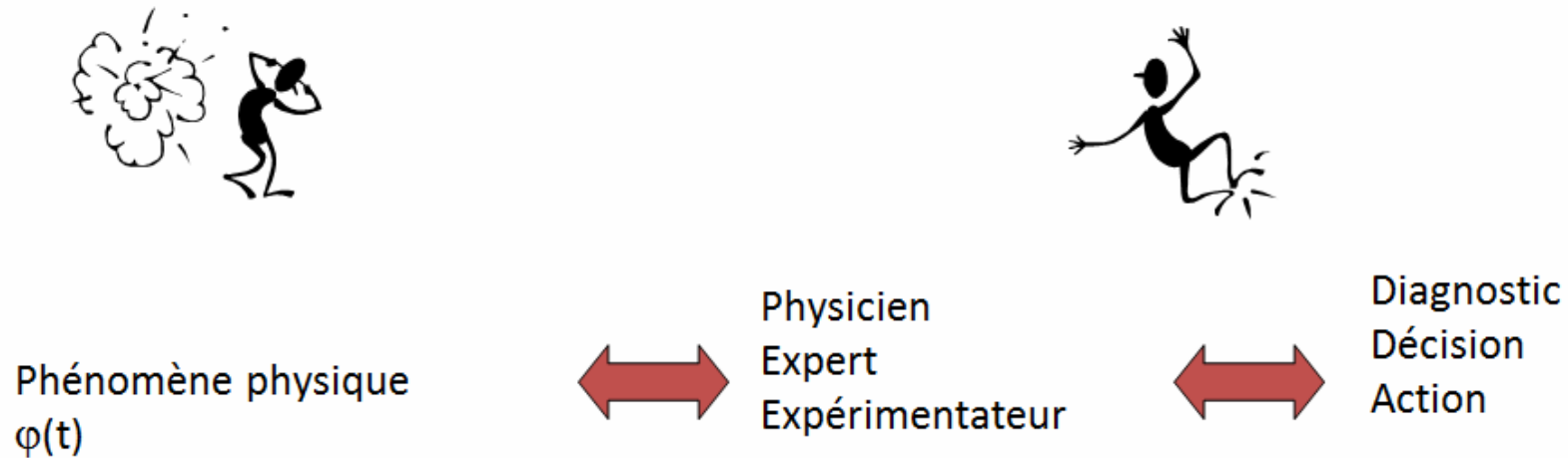
$$20 + 106 - 4 = 7\log_2(N) \Rightarrow \log_2(N) = 17 \Rightarrow 24 \text{ bit needed}$$



Outline

- Introduction
- Introduction to sound
- Measurement chain
- **Spectral analysis of acoustic measurements**
- Time-frequency representation
- Applied examples from our own research

Why ?



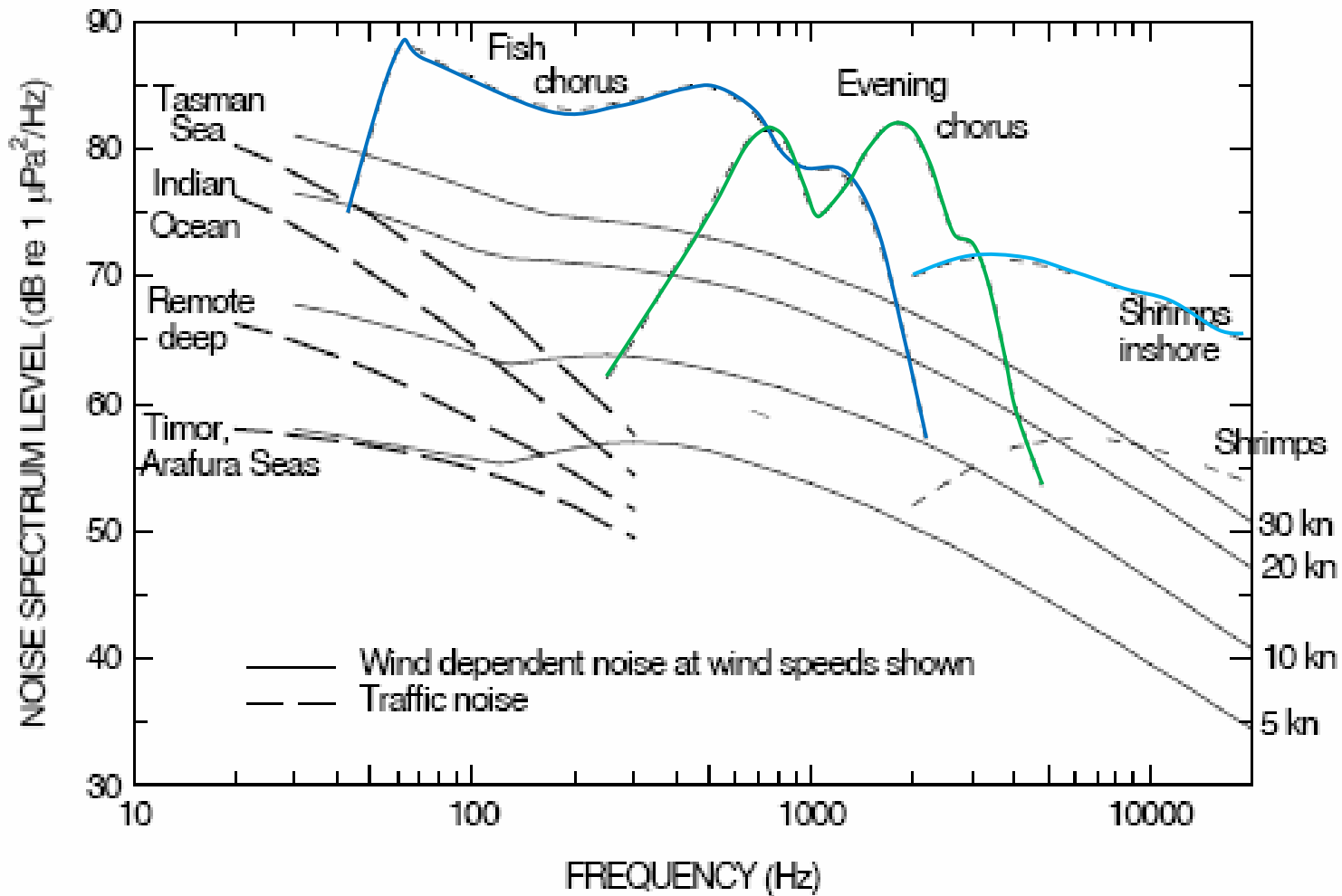
To represent the measurements to a scientist in the best way to understand its information content and to process them adequately.

Spectral analysis

- Frequency : number of repetitions of a phenomenon per second
- The frequency representation (rhythm of the repetitions naturally occurring in the measurement) allows sometimes to better understand the content of acoustic signals



Spectral analysis



Cato 2008, *Proc Inst Acoust*



Spectral analysis

Example: Description of the content of a mailing box (L. Di Iorio)

Introduction to Fourier analysis

Temporal representation

Mon	Tue	Wed	Thu	Fry	Sat	Sun	Mon	Tue	Wed
J	J	J	J	J+TV	J	J	J	J	J

Frequency representation

amplitude

1 daily newspaper J (1/day) at 8 am

+

1 newspaper with a weekly TV magazine (1/7 days) at 8am every friday

frequency

phase



How ? Easy

- $\cos(2\pi f_0 t)$, $\sin(2\pi f_0 t)$, $\exp(j2\pi f_0 t)$ contain only the frequency f_0 !

- $s(t)$ contains the frequency f_0 if it looks like $\cos(2\pi f_0 t)$, $\sin(2\pi f_0 t)$, $\exp(j2\pi f_0 t)$!

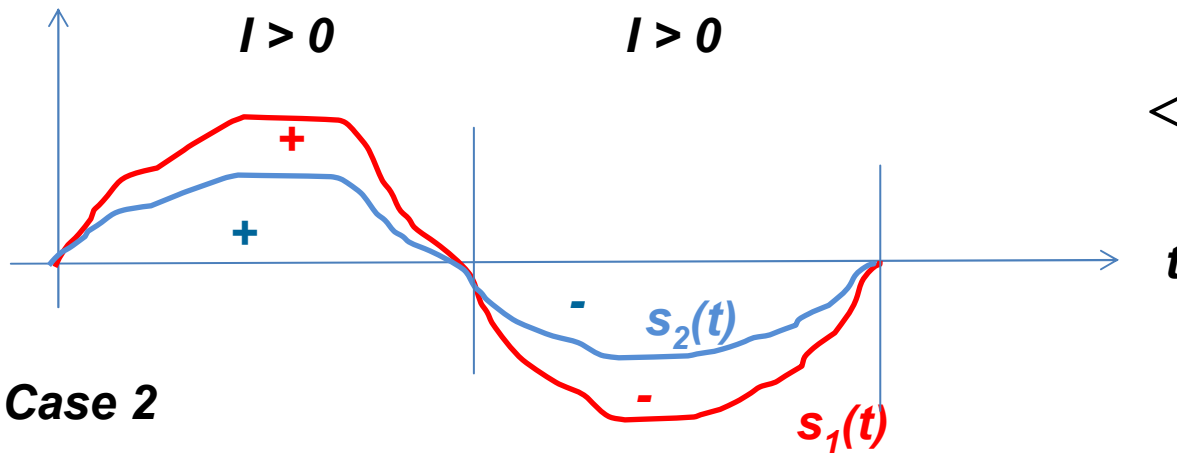
- $s_1(t)$ looks like $s_2(t)$ if their scalar products is high. (Linear Algebra)

$$\langle s_1(t), s_2(t) \rangle = \int s_1(t) s_2^*(t) dt$$



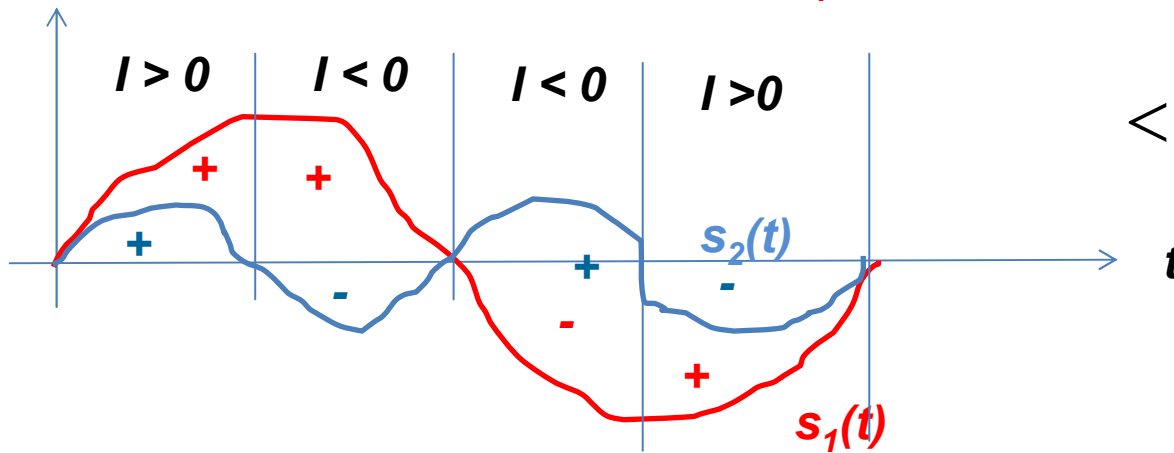
$$\langle s_1(t), s_2(t) \rangle = \int s_1(t) s_2^*(t) dt$$

Case 1



$$\langle s_1(t), s_2(t) \rangle > 0$$

Case 2



$$\langle s_1(t), s_2(t) \rangle \approx 0$$



How ?

Analogue signal: Fourier transform (FT)

$$s(t), t \in]-\infty, \infty[\quad S(f) = \int_{-\infty}^{+\infty} s(t) \exp(-2\pi f t) dt$$

Digital signal: Fourier transform via Fast FT (FFT)

$$\text{DFTS}(m) = \sum_{n=0}^{N-1} s(n) \exp(-2\pi j \frac{n \times m}{N})$$

$$s(n) \quad n \in \{1, \dots, N\}$$

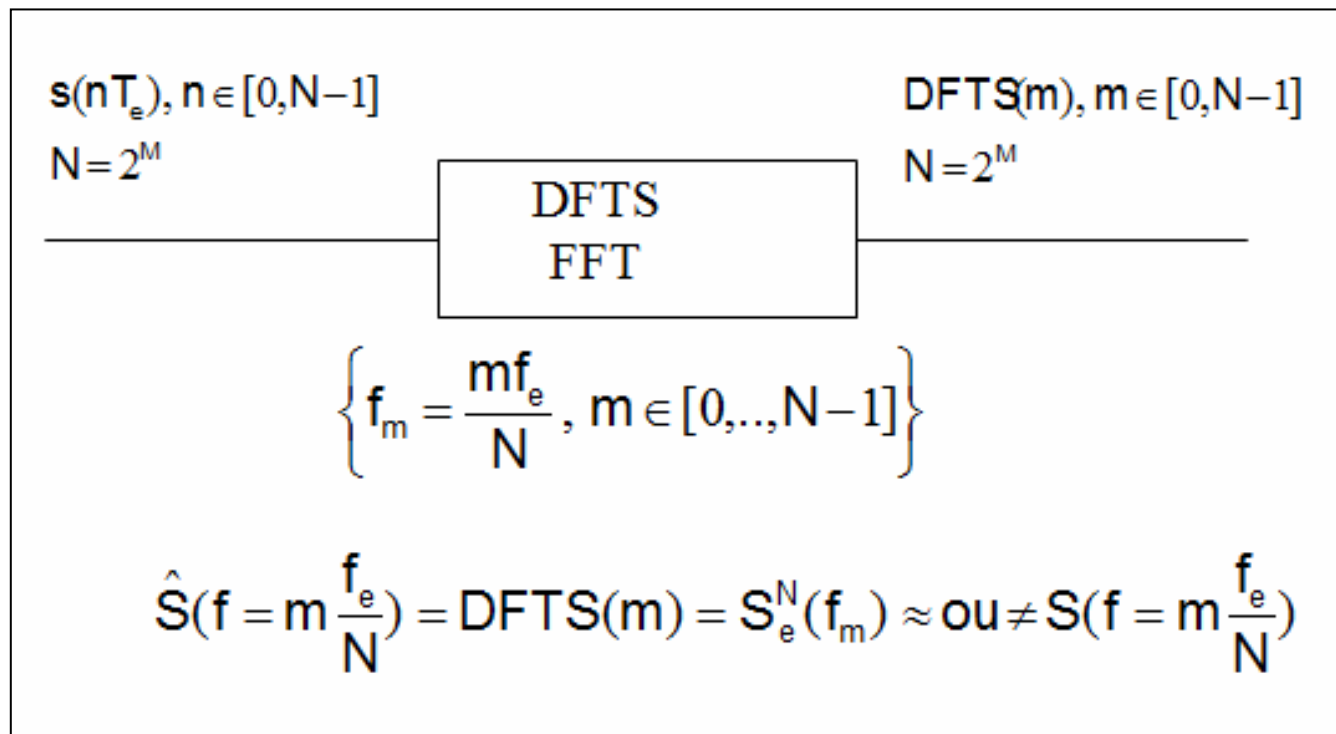
$$= \sum_{n=0}^{N-1} s(n) \times W_N^{n \times m}$$

$$\text{avec } W_N = \exp(-\frac{2\pi j}{N})$$



How ?

For digital signals: the discrete Fourier transform (DFT) can be implemented real-time! through the FFT algorithm (of N^2 operations at $N \log_2(N)$)

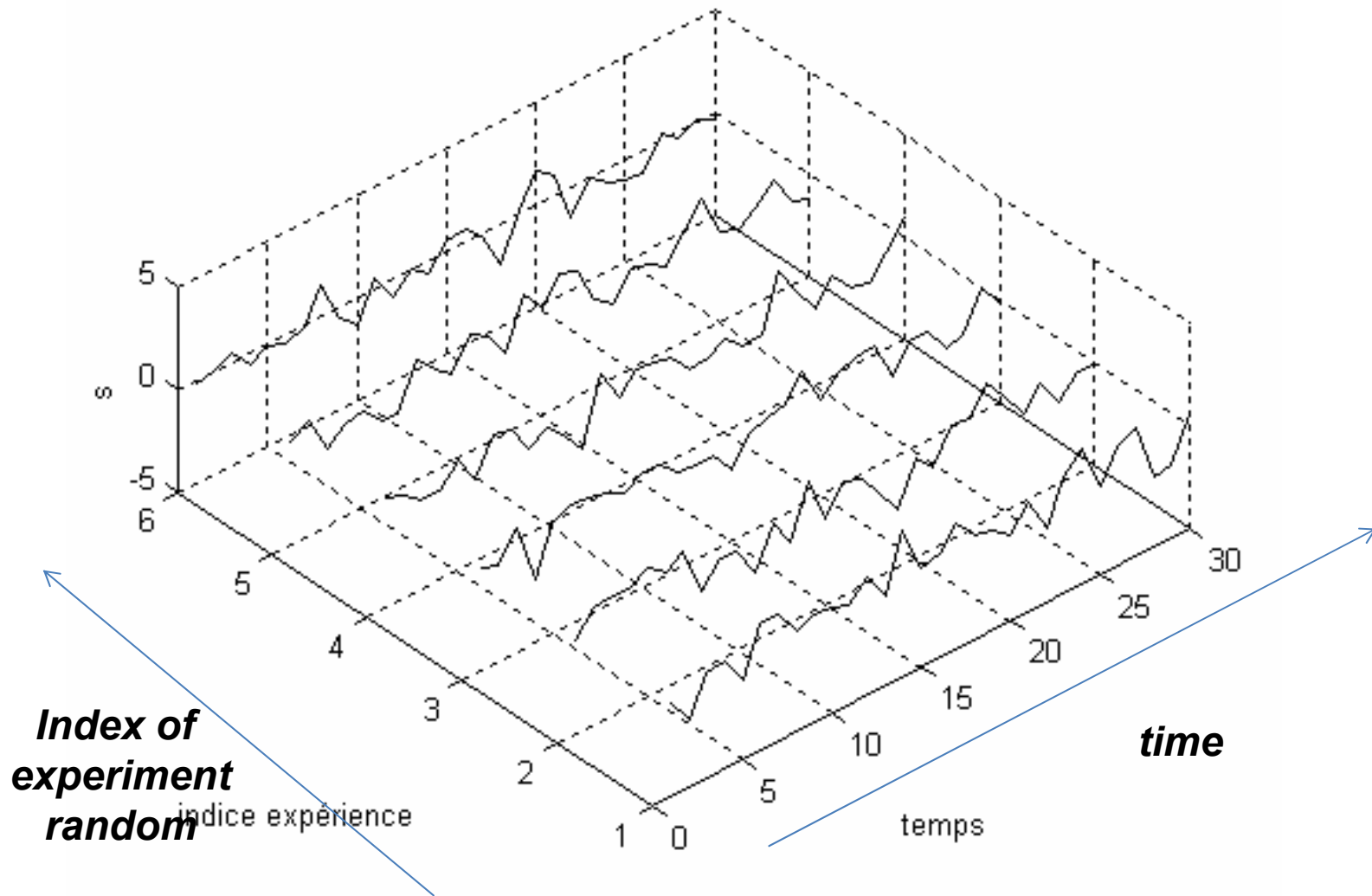


The case of random signals

- A random signal depends on time and hazard ε .
- Two recordings carried out within exactly the same conditions produce different measurements.
- $m(t, \varepsilon)$



$$s(t, \xi) !!!!!!!$$



The case of random signals

- For random signals, the Fourier transform cannot be applied directly!

Analogue signals : Fourier Transform

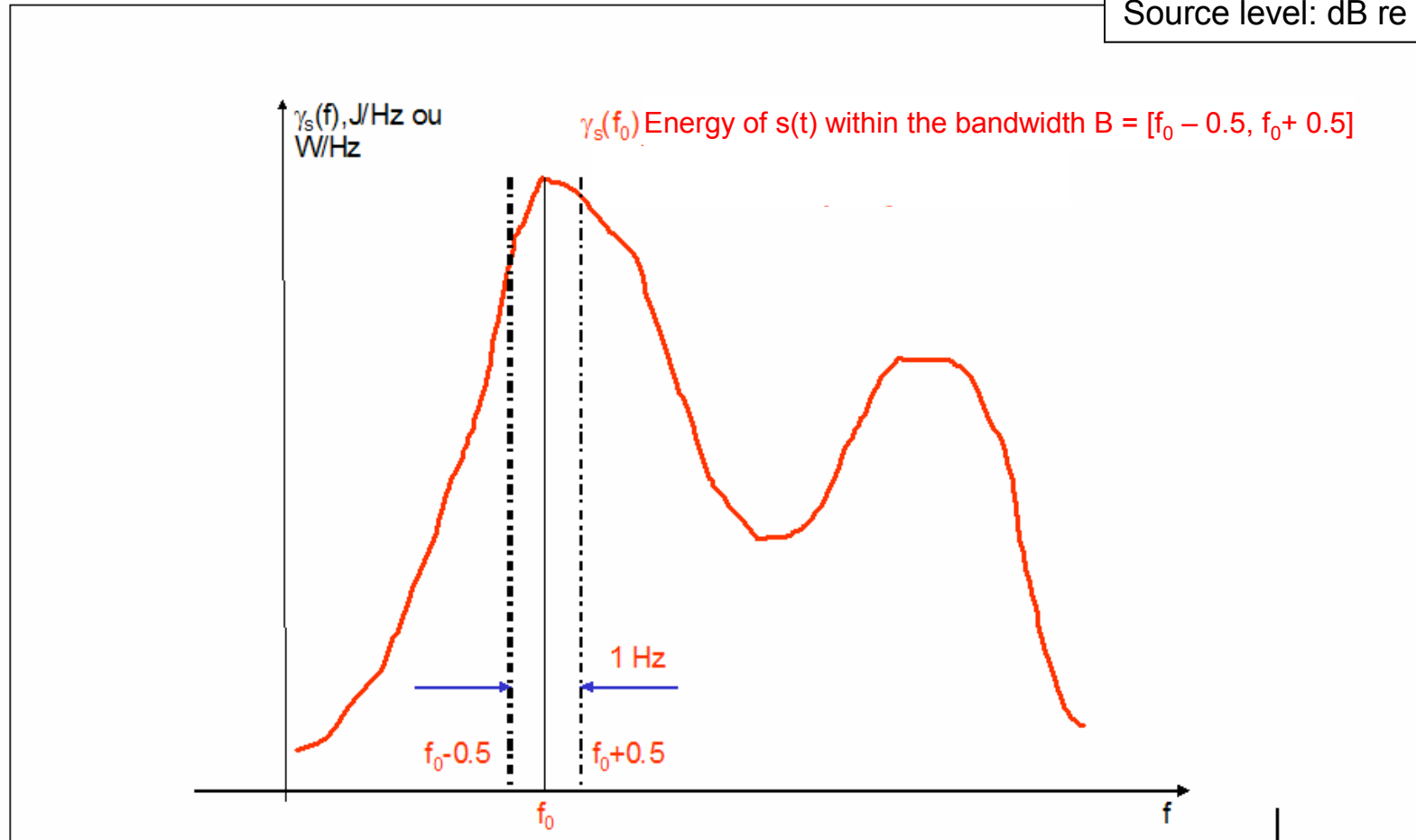
$$s(t), t \in]-\infty, \infty[\quad S(f) = \int_{-\infty}^{+\infty} s(t) \exp(-2\pi f t) dt$$



For random signals we estimate the power spectral density

= frequency distribution of the power of a random signal

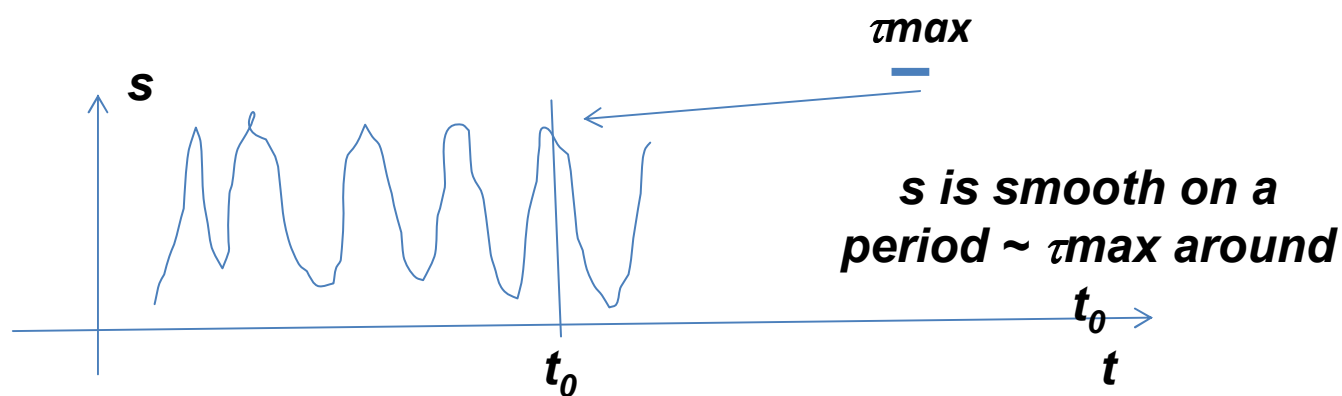
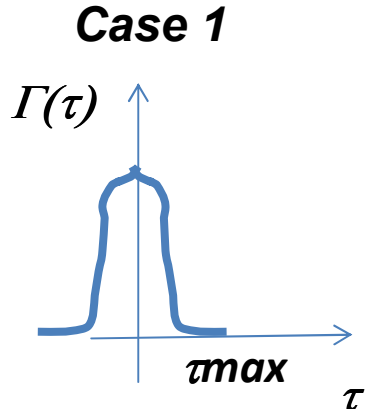
Received level : dB re $1\mu\text{Pa}^2/\text{Hz}$
Source level: dB re $1\mu\text{Pa}^2/\text{Hz}@1\text{m}$



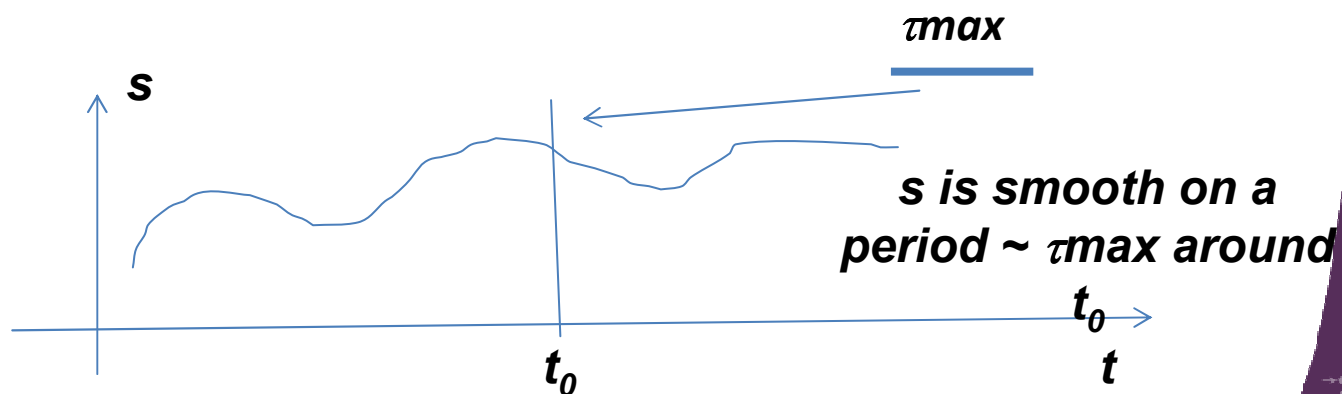
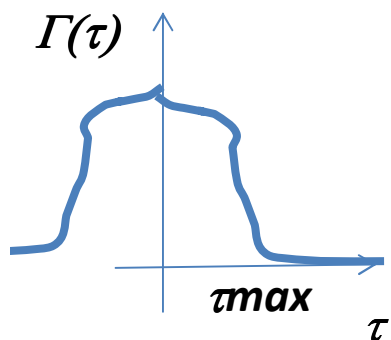
A tool for power spectral density estimation: the autocorrelation function

$$\Gamma_s(\tau) = \langle s(t), s(t - \tau) \rangle$$

Case 1



Case 2



$\Gamma_s(\tau)$ commands the dynamic of variation of $s(t)$

Fast variation : high frequency

Slow variation : low frequency

Autocorrelation function

$$\Gamma_s(\tau) = \langle s(t), s(t - \tau) \rangle$$

Autocorrelation function

$$= \lim_{T \rightarrow \infty} \frac{1}{T} \int_{-T/2}^{T/2} s(t)s(t - \tau) dt$$

For Deterministic signals

$$= E(s(t_0, \xi)s(t_0 - \tau, \xi))$$

For random signals S.O2

$$\gamma_s(f) = F(\Gamma_s(\tau)); (V^2 / \text{Hz})$$


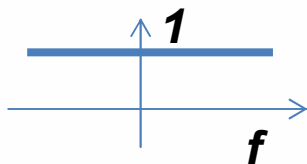
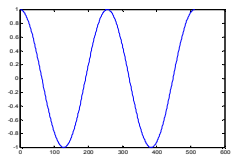
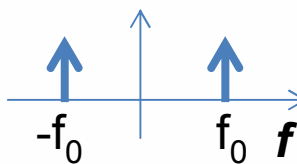
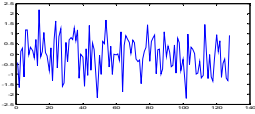
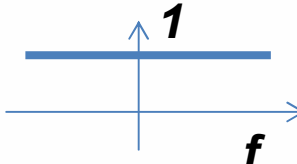
Power spectral density

$$= \lim_{T \rightarrow \infty} \frac{1}{T} |S_T(f)|^2$$

For Deterministic signals



Fourier transform of 'classical' signals

	$s(t)$	$S(f)$	
	$\delta(t)$	$\Delta(f) = 1 \forall f$	
	$\cos(2\pi f_0 t)$	$C(f) = 0,5\delta(f - f_0) + 0,5\delta(f + f_0)$	
	$bb(t, \epsilon)$ $\gamma(\tau) = \delta(\tau)$	$\gamma(f) = 1 \forall f$	

The use of a PC to apply the theory to real measures

Analogue signal with infinite temporal domain and infinite number of experiences

$$s(t, \varepsilon), t \in]-\infty, +\infty[$$

Signal carrying the entire information not usable

$$S(f) = \int_{-\infty}^{+\infty} s(t) \exp(-2\pi jft) dt$$

Spectrum carrying information
 $S(f)$



Physical phenomenon inducing a magnitude to change $s(t)$



$$\hat{S}(f) \stackrel{?}{=} S(f)$$

Digital signal with finite temporal domain and one experience

$$s(nT_e, \varepsilon_1), n \in [0, N-1]$$

Signal not carrying the entire information usable

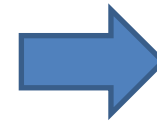


$$\hat{S}(f)$$

$$\hat{S}(f) = \sum_{n=0}^{N-1} s(nT_e) \exp(-2\pi jfnT_e)$$

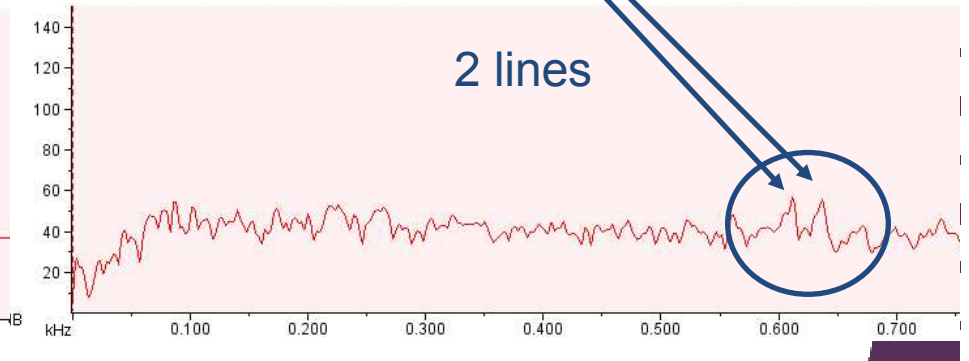
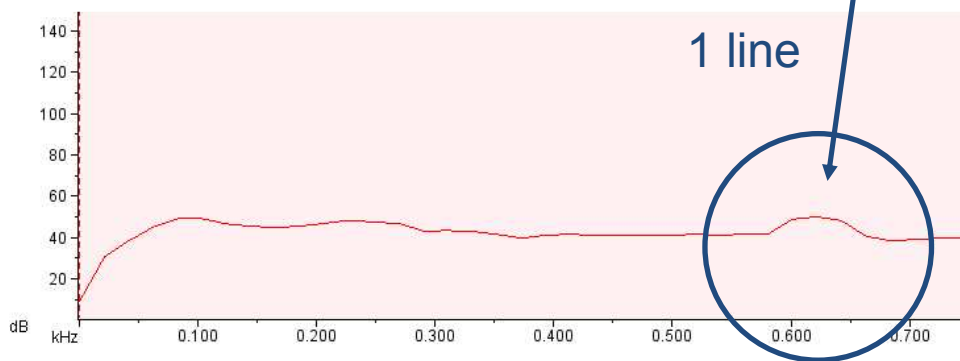
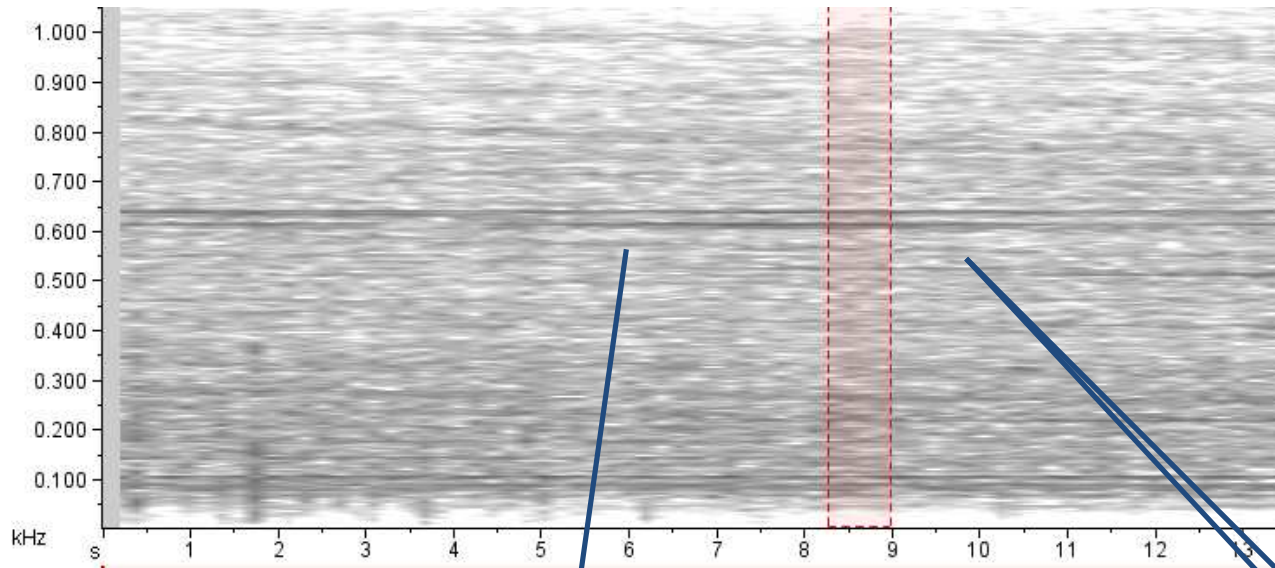


Frequency resolution



***How many propellers, blades ?
Which states ?***

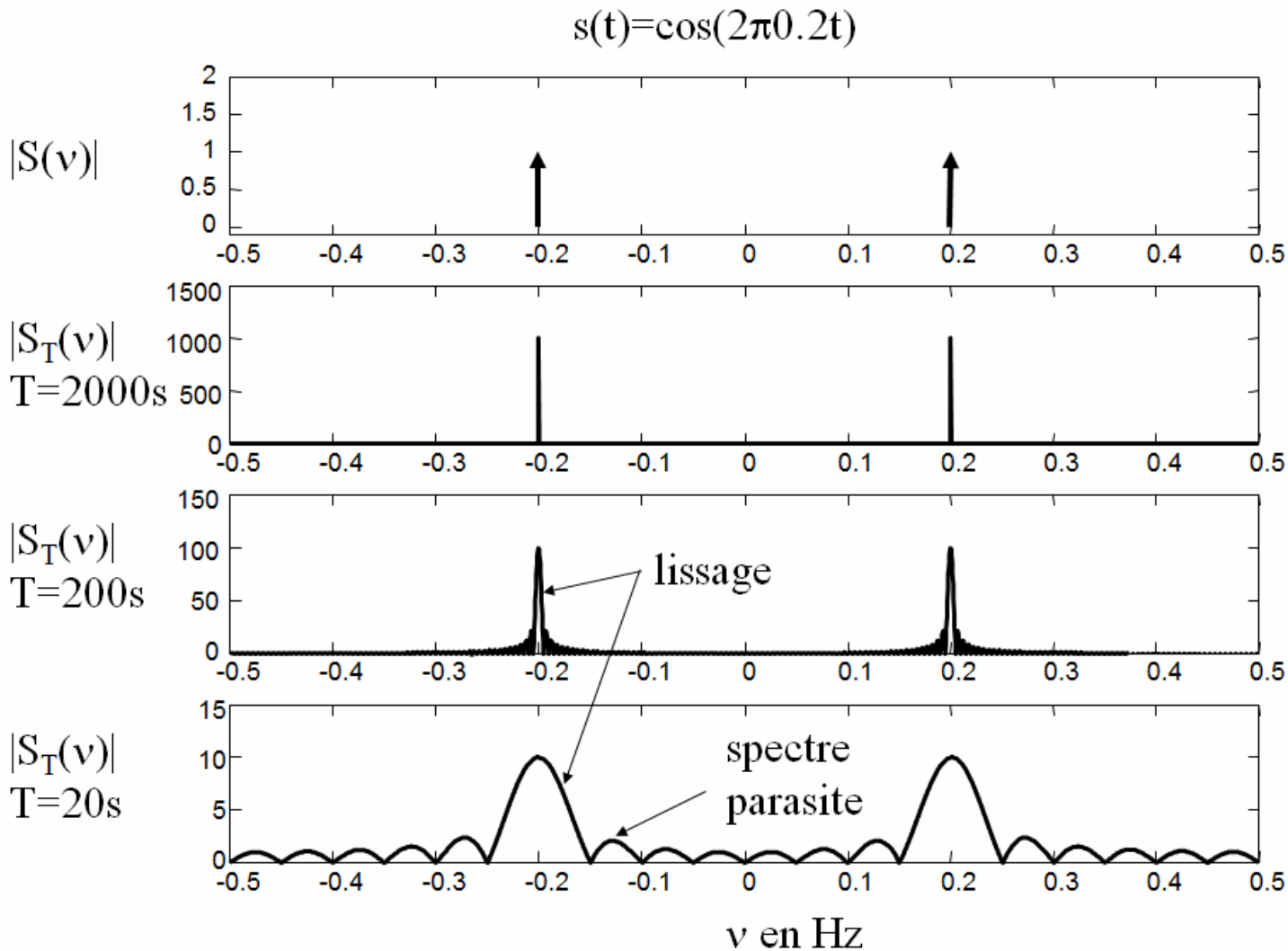
Frequency resolution



„bad‘ frequency resolution: „ lines „blured“

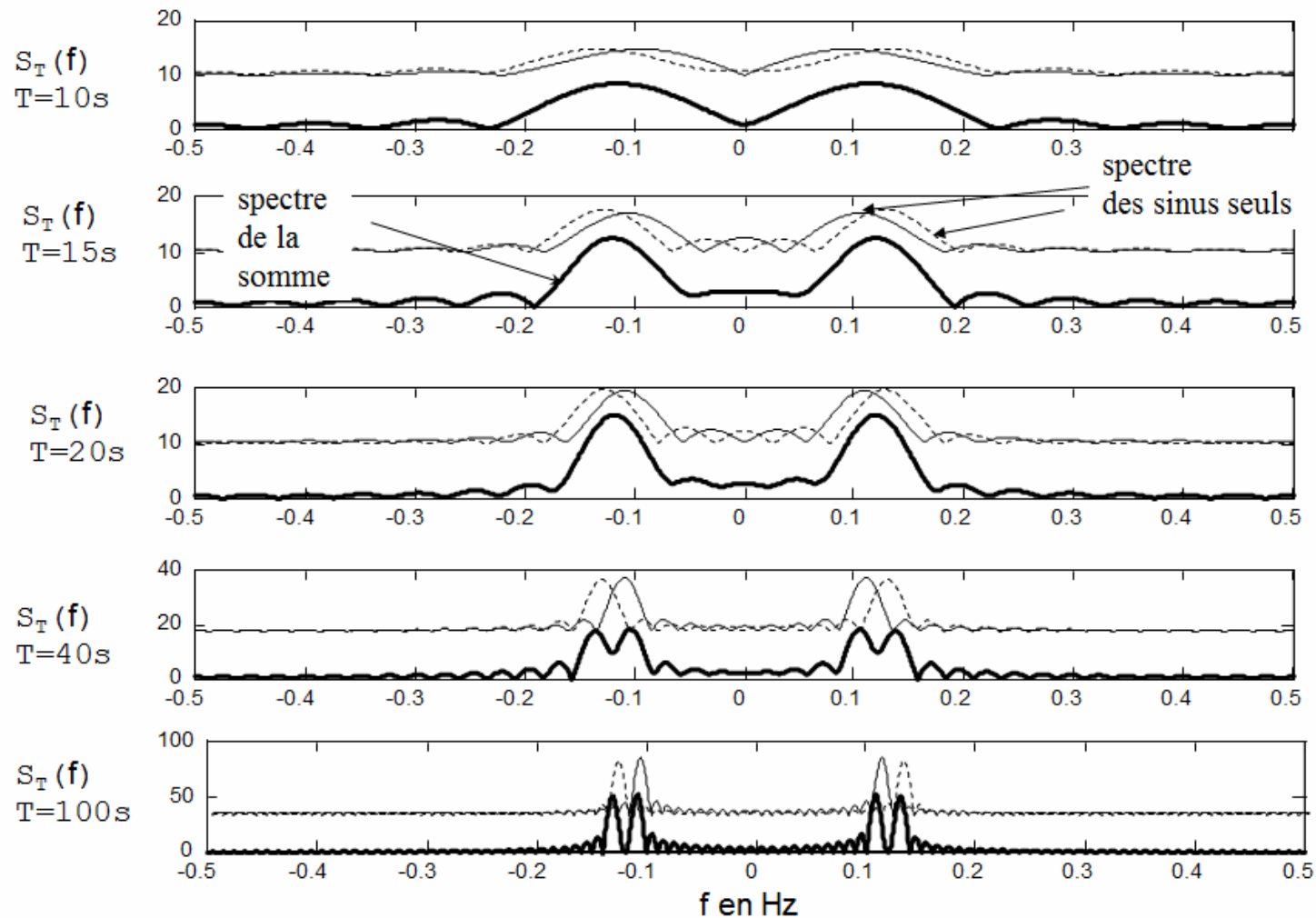
„good‘ frequency resolution: 2 lines

FFT errors: The frequency resolution – separation of two close frequencies



FFT errors: The frequency resolution – separation of two close frequencies

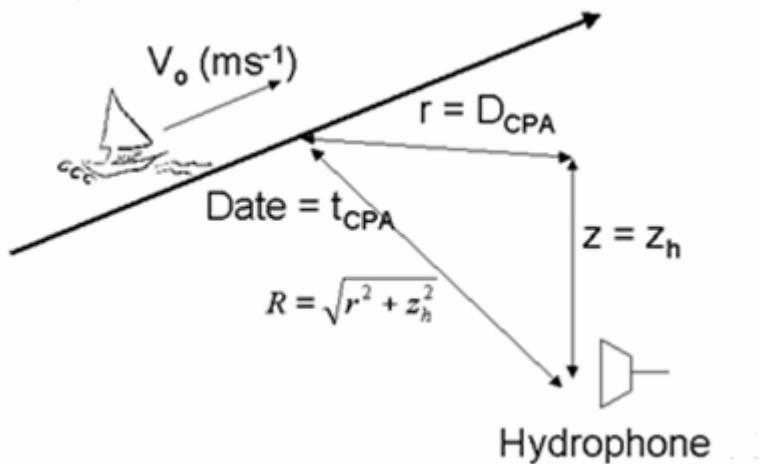
$$s(t) = \sin(2\pi 0.11t) + \sin(2\pi 0.13t)$$



FFT errors: The frequency resolution – separation of two close frequencies

Frequency resolution is the ability to distinguish the presence of two components of similar frequencies

$$\text{frequency resolution} \propto \frac{1}{T}$$

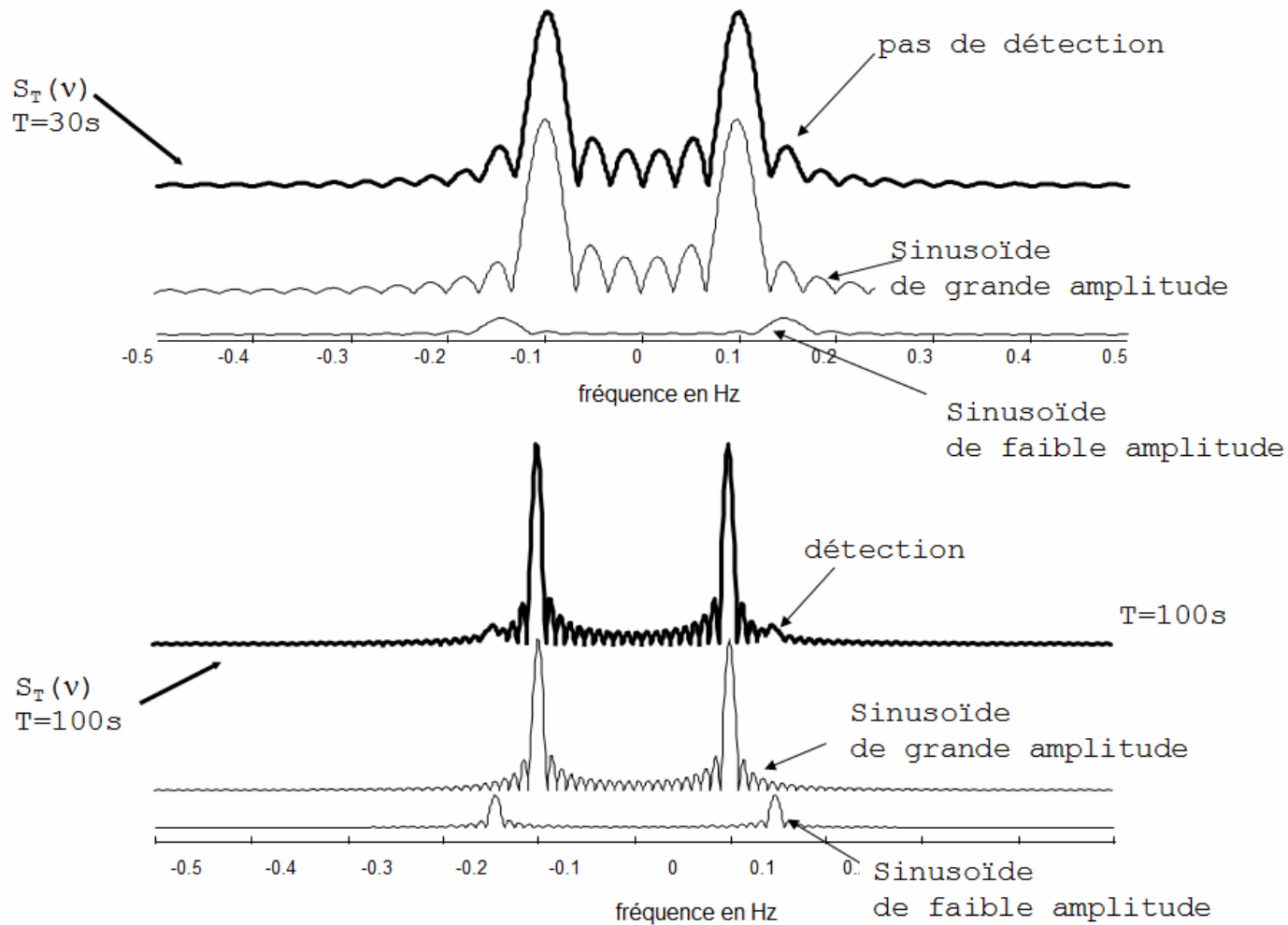


*trawler Domingo, Off Barcelona, Spain
September 2006*

- Radiale domingo + adobe

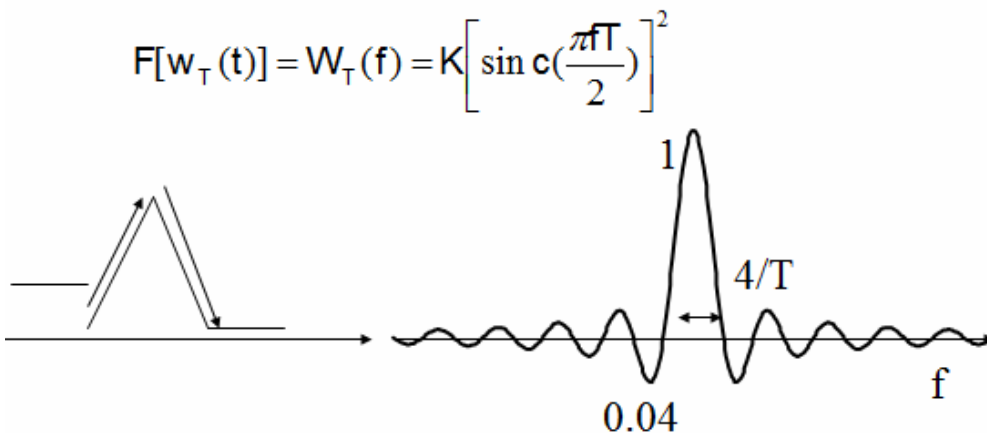
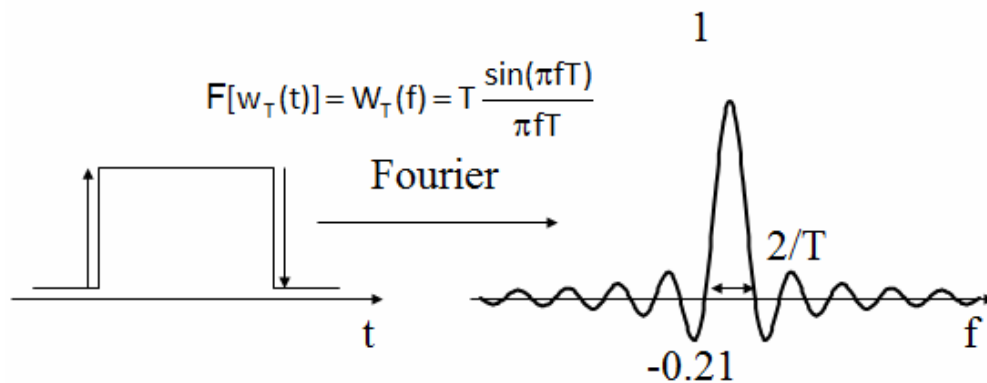
FFT errors: The amplitude resolution – simultaneous distinction of a faint and intense signal

$$s(t) = \sin(2\pi 0.1t) + 0.1\sin(2\pi 0.145t)$$



FFT errors: The amplitude resolution – simultaneous distinction of a faint and intense signal

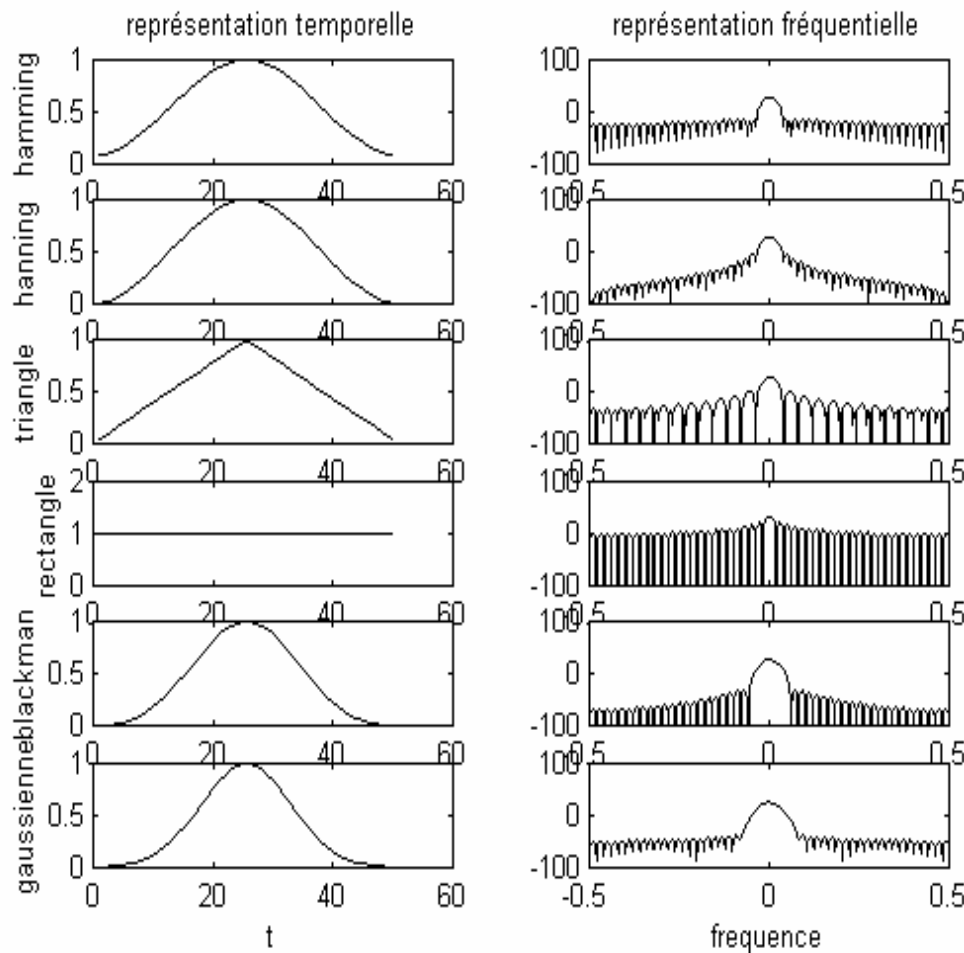
$$s(t, \xi), t \in]-\infty, +\infty[\quad s(nT_e, \xi_0), n \in [0, N-1]$$



$s_i(t) = w(t) \times s(t)$
 $w(t)$
 Windows with
 smoothed or sharp
 shape (upward and
 downward front)

FFT errors: The amplitude resolution – simultaneous distinction of a faint and intense signal

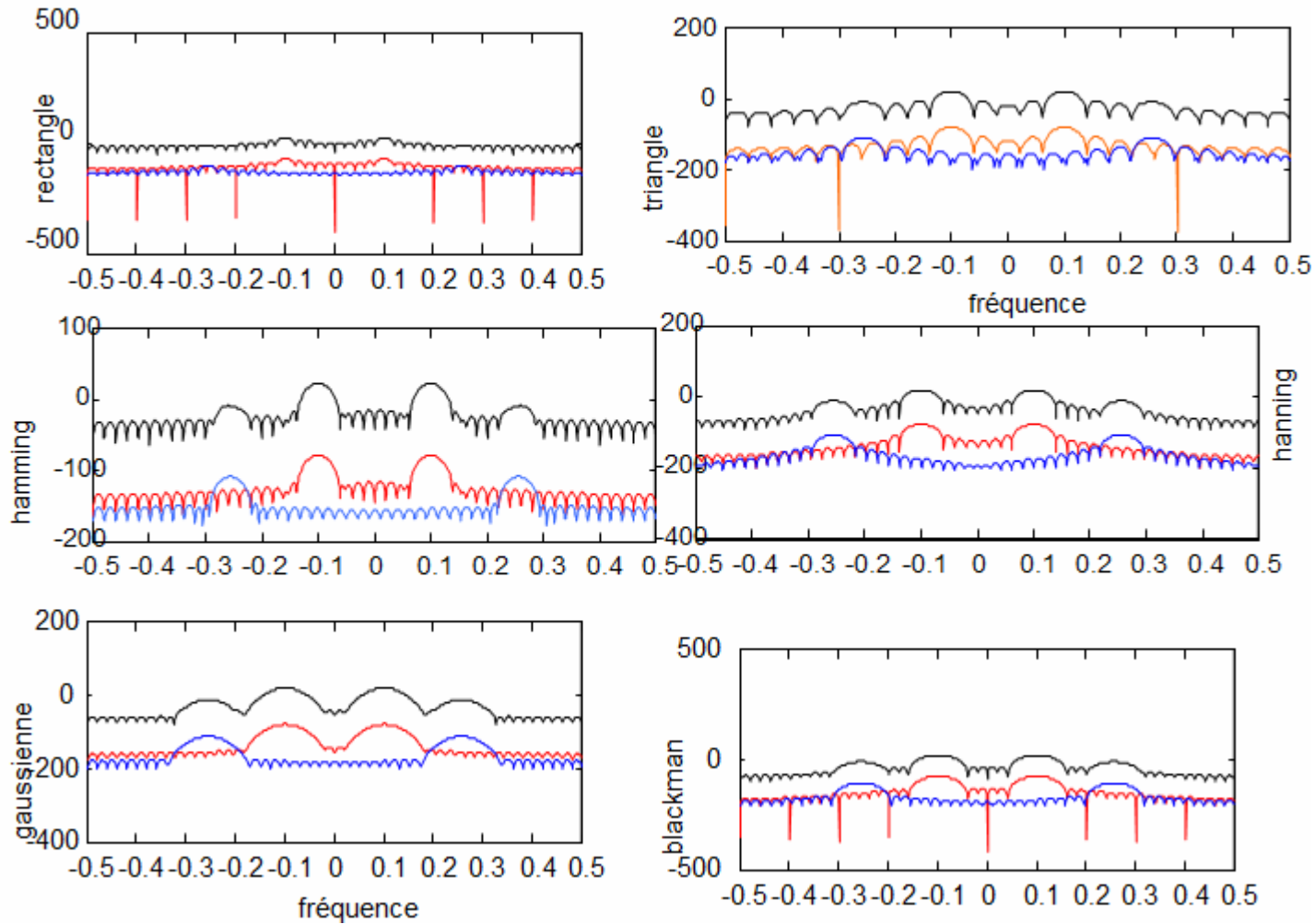
$$s(t, \xi), t \in]-\infty, +\infty[\quad s(nT_e, \xi_0), n \in [0, N-1]$$



$s_i(t) = w(t) \times s(t)$
 $w(t)$ Windows with smoothed or sharp shape (upward and downward front)

Types of analysis windows

$$s(t) = [\cos(2\pi 0.1t) + 0.03 \cos(2\pi 0.256t)]\text{porte}(T/2, t)$$



Take home message FFT errors

1] **Frequency resolution:** determines the ability to separate components of similar frequencies. The limiting value δf is inversely proportional to the duration of observation (window) and dependent on the type of the analysis window.

2] **Amplitude resolution:** determines the ability to detect a faint component in the presence of an intense one. It is dependent on the analysis window. In the case of a rectangular window, a component with a 5 times smaller amplitude compared to another component might not be detected.

3] **To increase the amplitude resolution,**
We must chose a weighting Windows with a smooth shape. As a consequence, the size (duration) of the analysis window is reduced, implying a degradation of the frequency resolution.



Power spectral density of Random signal

Periodogram

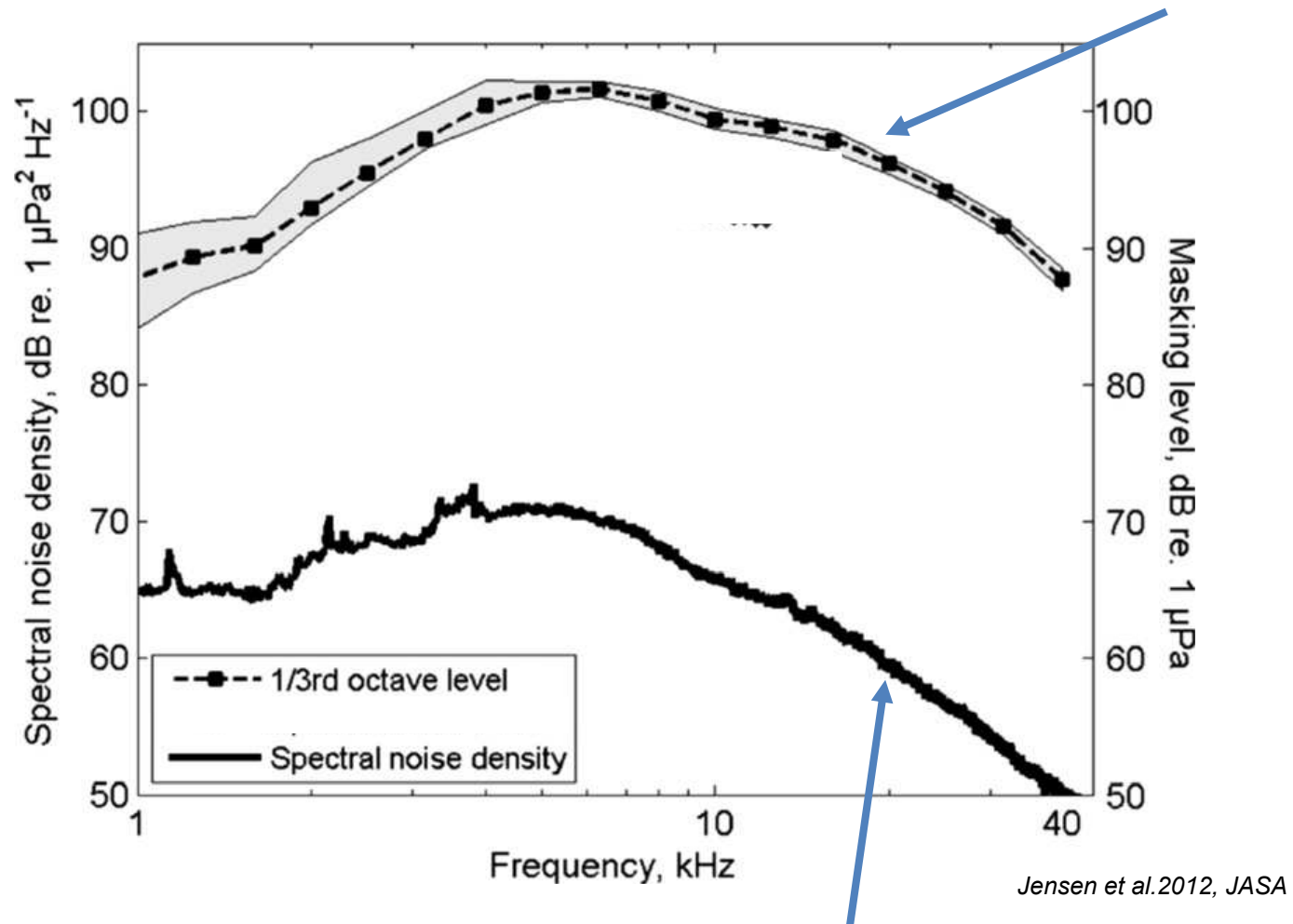
$$s = [s(1, \xi_1); s(2, \xi_1); s(3, \xi_1) \dots; s(N, \xi_1)]$$

$$\tilde{\gamma}_s(f) = \frac{1}{Nf_s} |\text{FFT}(s)|^2$$

***Estimated with FFT => corrupted with error
(frequency resolution, amplitude resolution, dispersion)***

Types of spectra – choice depends on use

Octave or 1/3 octave levels: Noise impact studies on mammalian ears (masking)



Narrowband (1Hz bands) levels: Ambient noise descriptions

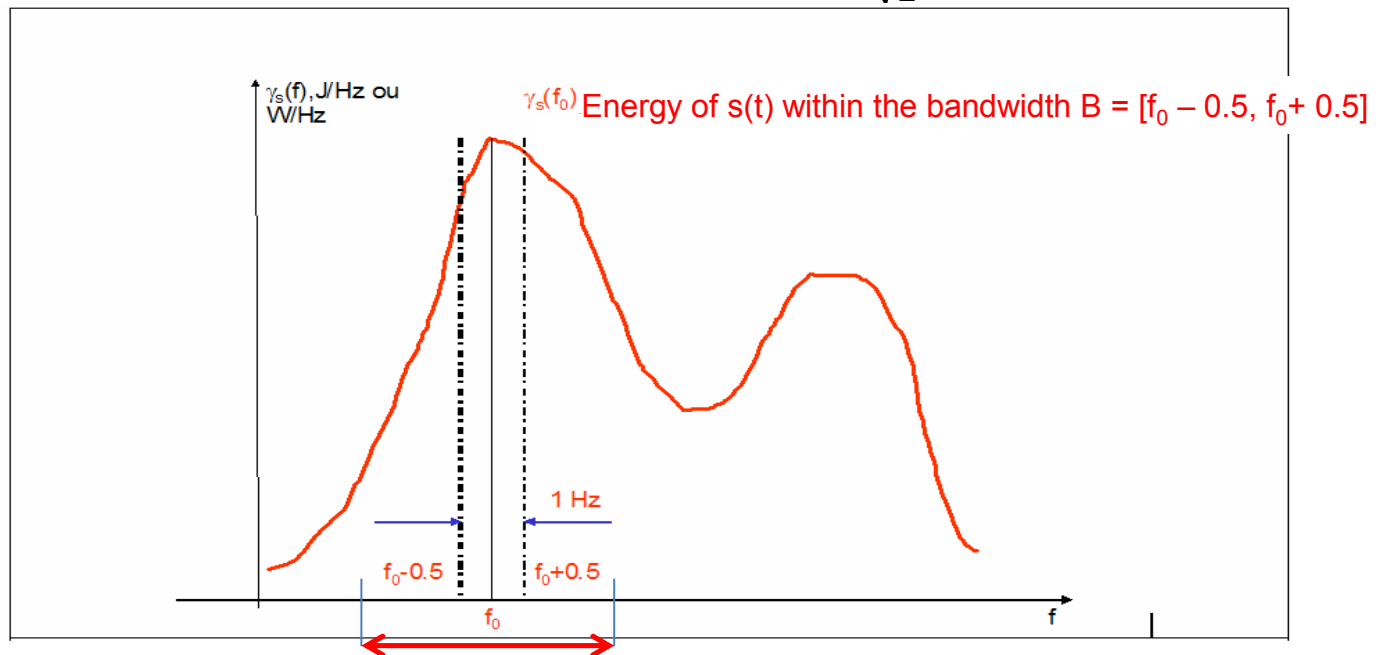
From the narrowband to the wideband, octave and 1/3 octava-band spectra

1/3 d'Octave band around f_0

$$B = [f_1 = \frac{f_0}{2^{1/6}}, f_2 = 2^{1/6} f_0]$$

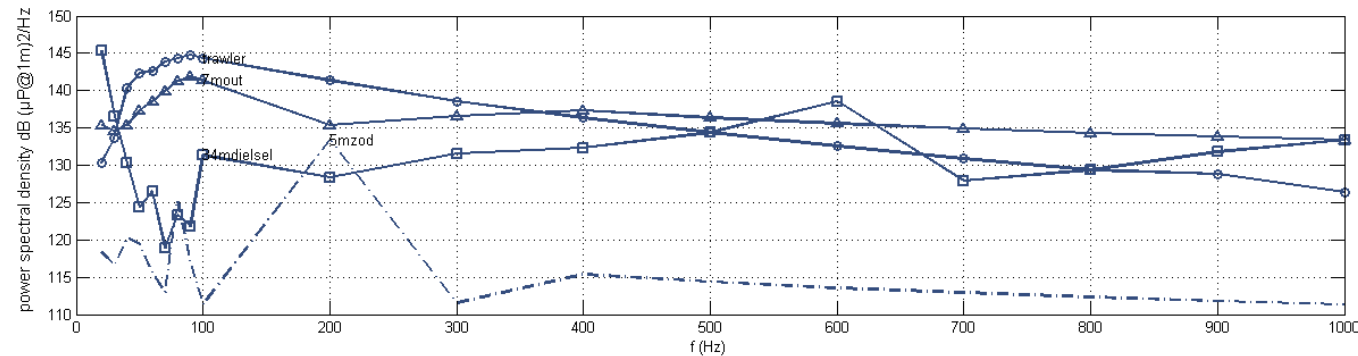
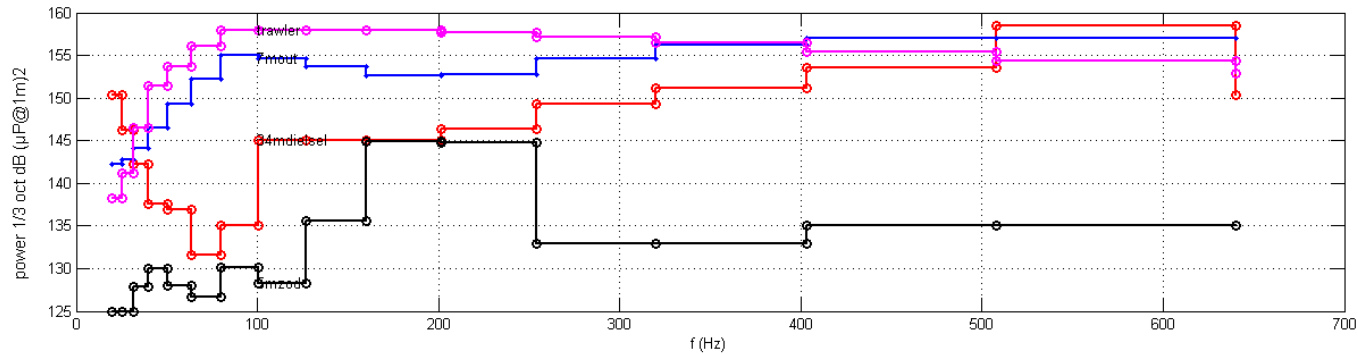
Octave band around f_0

$$B = [f_1 = \frac{f_0}{\sqrt{2}}, f_2 = \sqrt{2} f_0]$$



$$sl(B) = \int_{f_1}^{f_2} \gamma(f) df$$

From the narrowband to the wideband, octave and 1/3 octava-band spectra

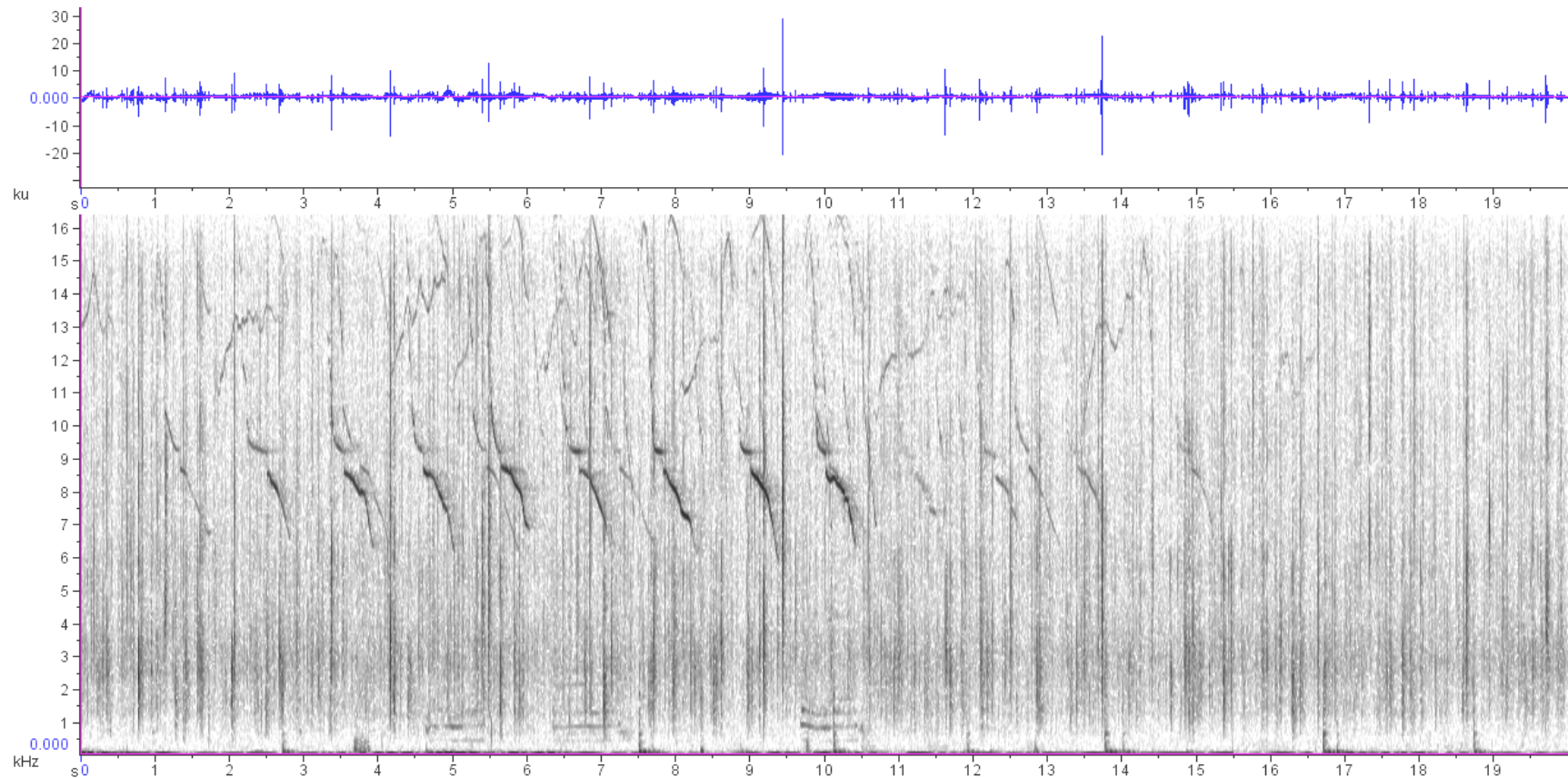


Outline

- Introduction
- Introduction to sound
- Measurement chain
- Spectral analysis of acoustic measurements
- **Time-frequency representation**
- Applied examples from our own research



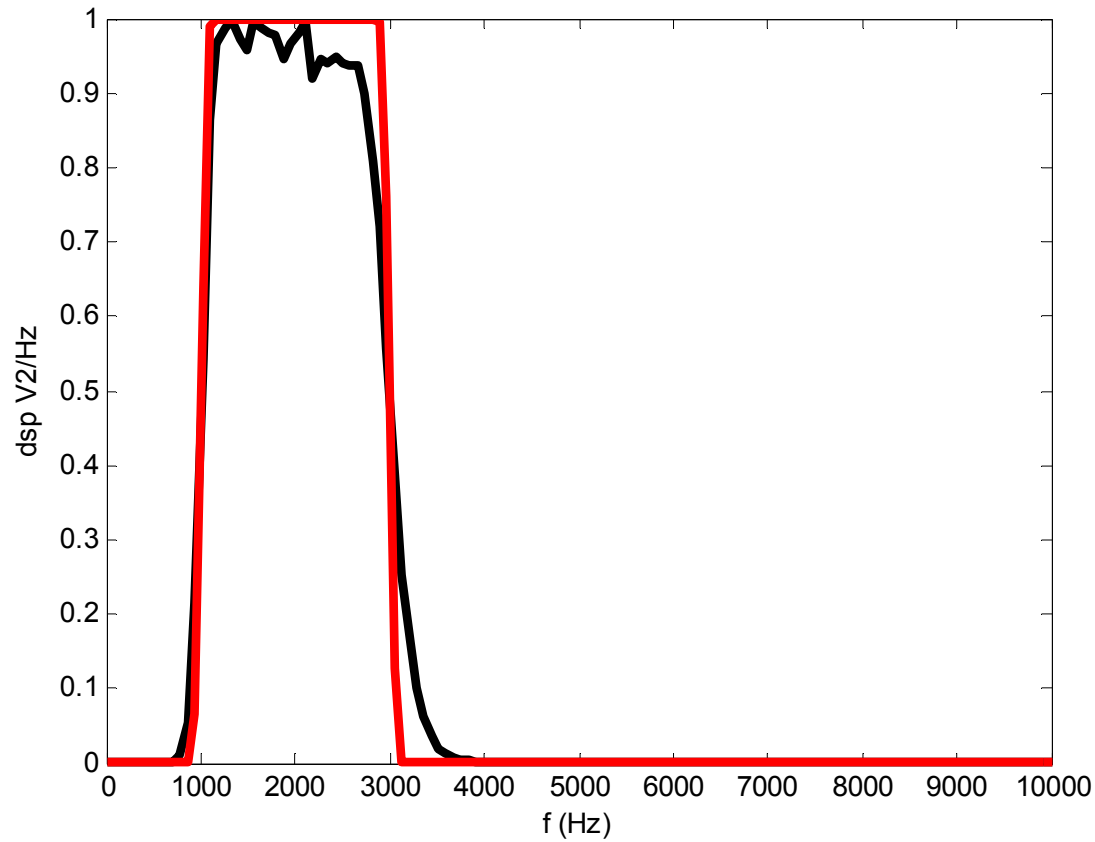
Time-frequency representation Spectrogram



Introducing the spectrogram – why?

Sound 1

Sound 2



- live

The limitations of the Fourier Transform for non-stationary signals

The Fourier transform transforms a temporal signal into a frequency signal

It indicates the frequency content of a signal...

...but does not date the frequency content!

=> Reasons why it is appropriate for stationary signals, with a stationary signal = a signal whose frequency or spectral content do not change with respect to time!



Non stationary signals – frequency-modulated signals

Single frequency

$$s(t) = \cos(2\pi f_0 t)$$

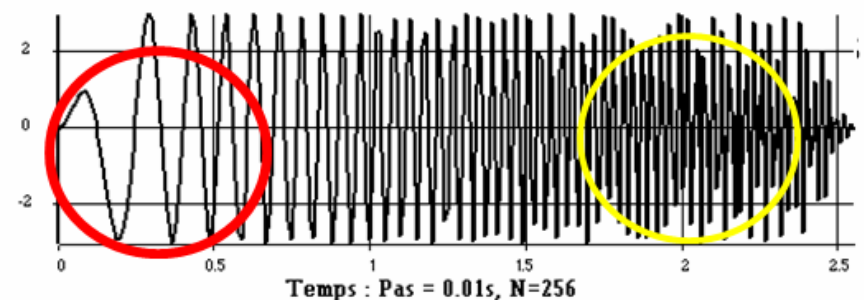
$$s(t) = \cos(\varphi(t)), \varphi(t) = 2\pi \int_0^t f_0 dt$$

$$f_0 = \frac{1}{2\pi} \frac{d\varphi(t)}{dt}$$

Varying frequency

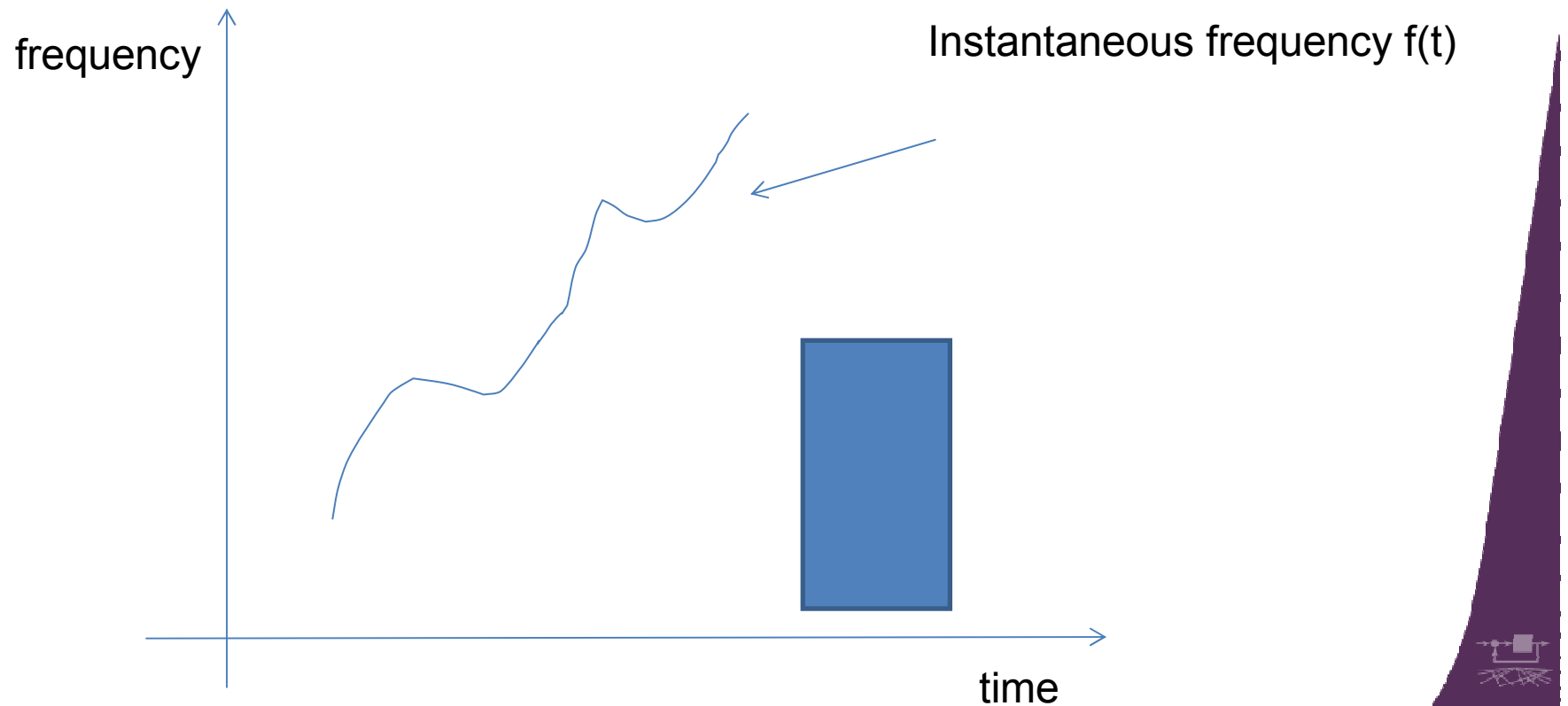
$$s(t) = \cos(\varphi(t))$$

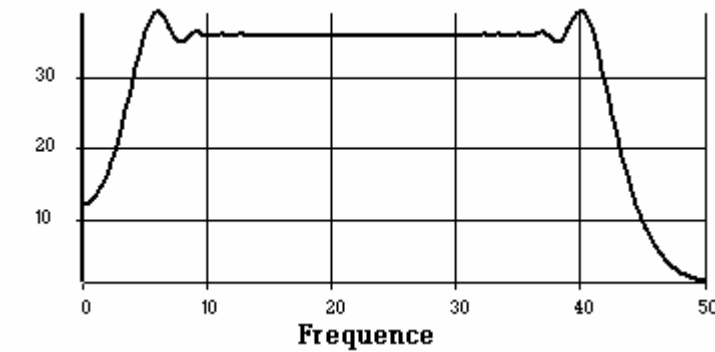
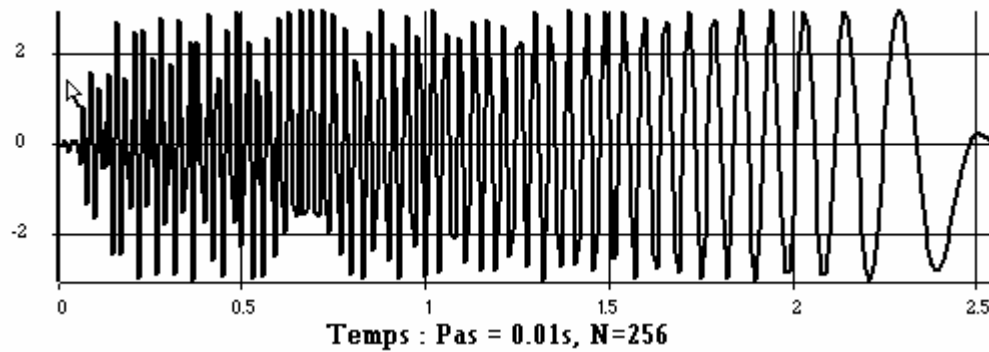
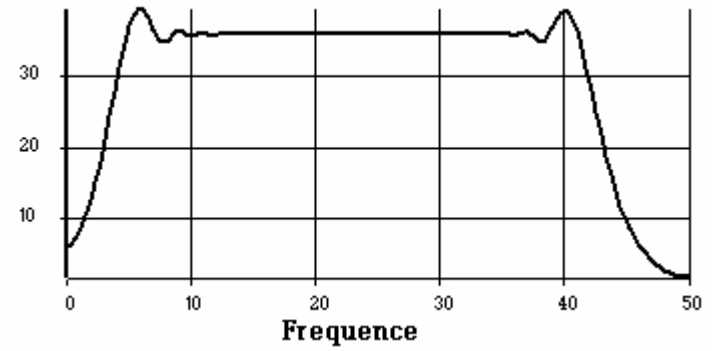
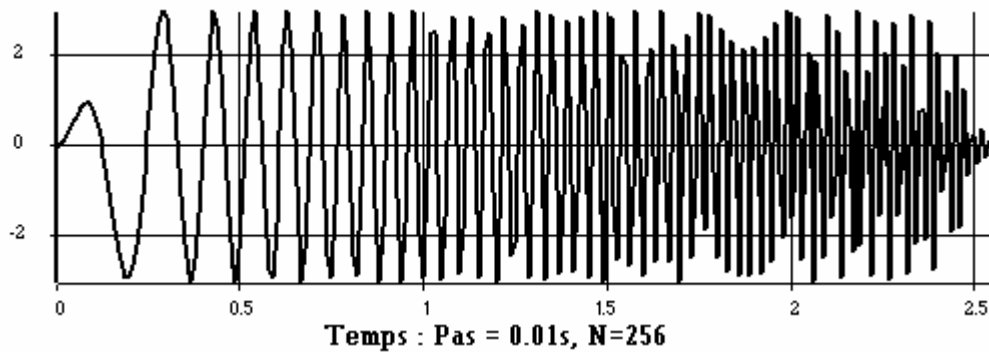
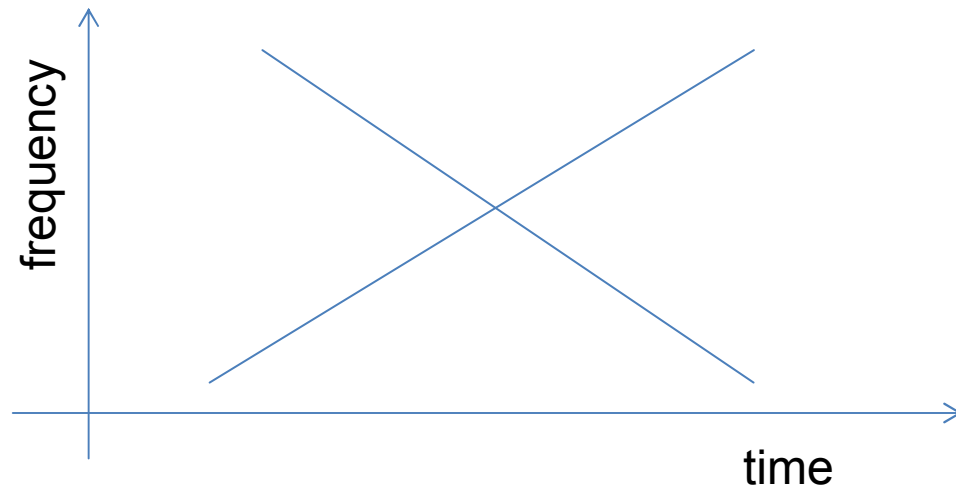
$$f_i(t) = \frac{1}{2\pi} \frac{d\varphi(t)}{dt}$$



Need of a time-frequency representation: which frequency $f(t)$ at time t ?

We want to map the power of a signal in a time-frequency plane





For non-stationary signals

- Goal: for deterministic non-stationary signals, how to get from a frequency to a time-frequency representation
- The frequency : number of cycles per second
- Intrinsic problem : frequency is already time-dependant in a time-frequency representation we look for the instantaneous frequency (number of cycles during dt around t)....



The short-term Fourier Transform (STFT)

The Spectrogram

STFT corresponds to an adaptation of the Fourier transform
– a spectral representation of consequent time segments

$$S(t_0, f_0) = \int s(t) \times w_T(t - t_0) \exp(-2\pi j f_0 t) dt$$

$$S(t_0, f_0) = F(s(t) \times w_T(t - t_0))$$

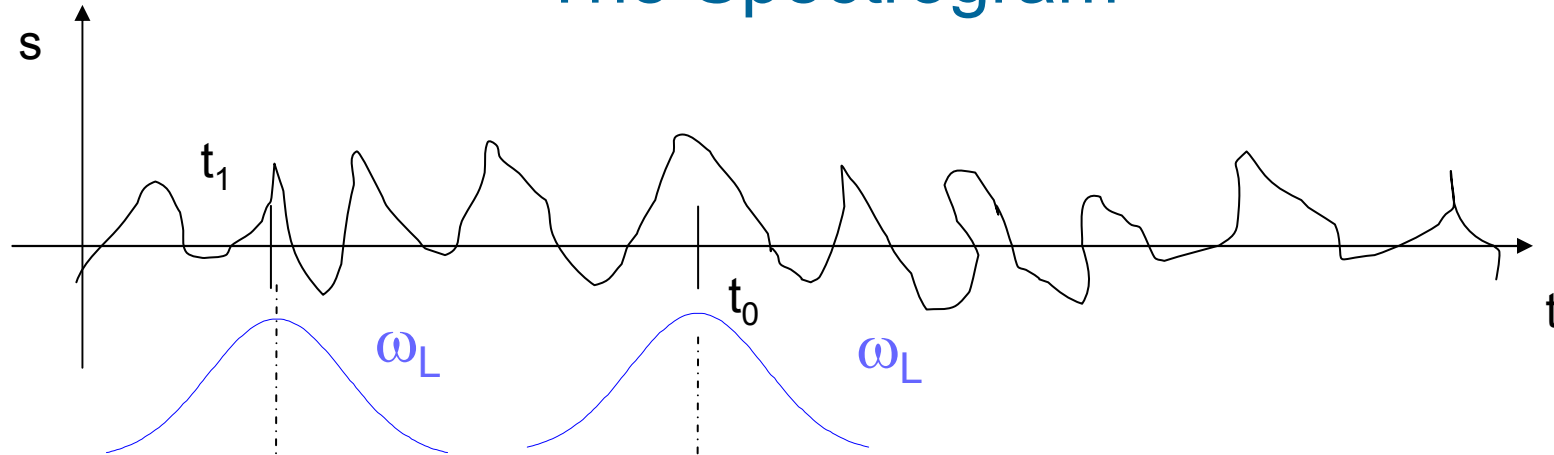
The spectrogram = the squared magnitude of the STFT of a signal $s(t)$

$$S_{spect}(t_0, f_0) = |S(t_0, f_0)|^2$$

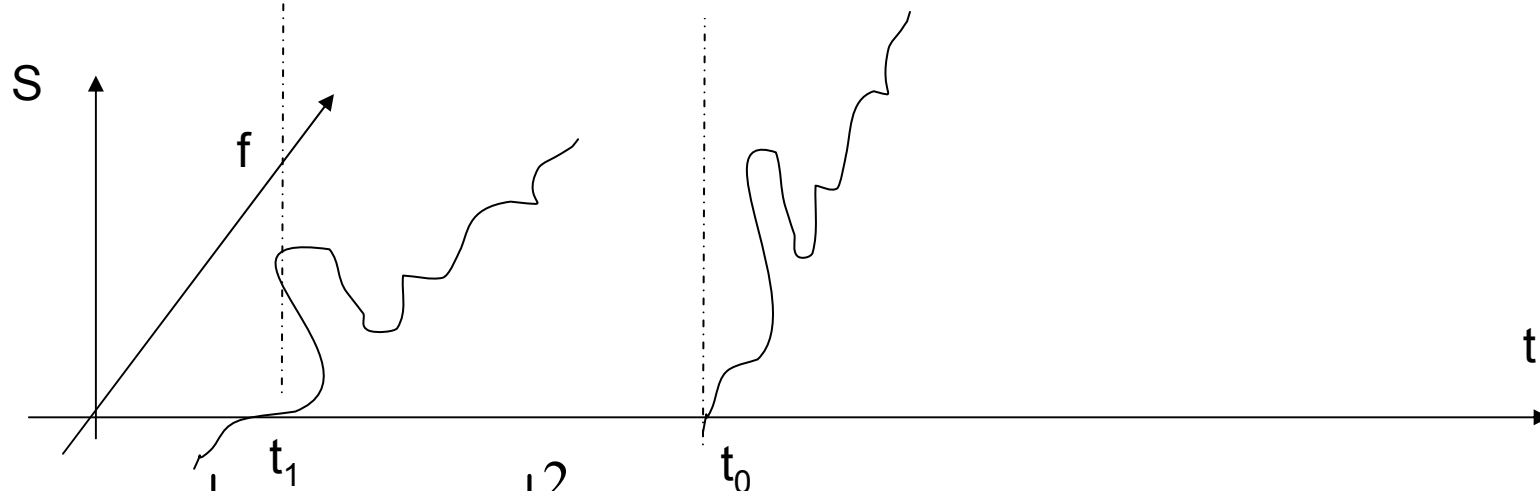
The spectrogram = a map of signal energy in time-frequency plane



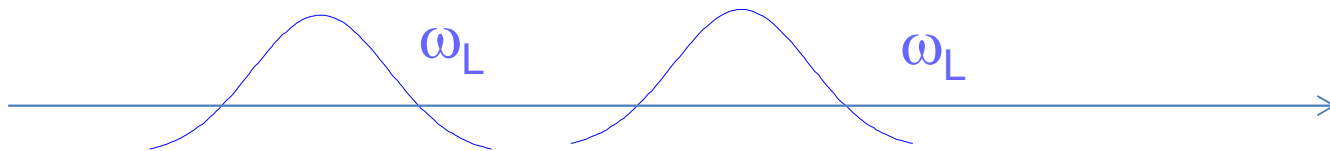
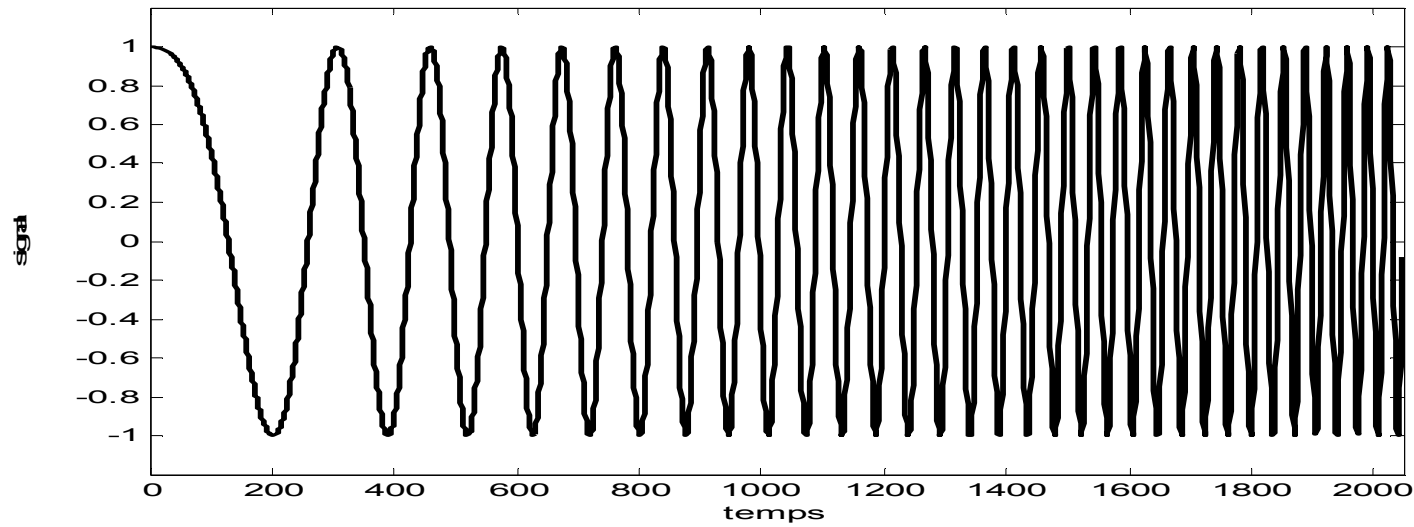
The short-term Fourier Transform (STFT) The Spectrogram



$$S(t_0, f) = F(s(t) \times \omega_L(t - t_0))$$

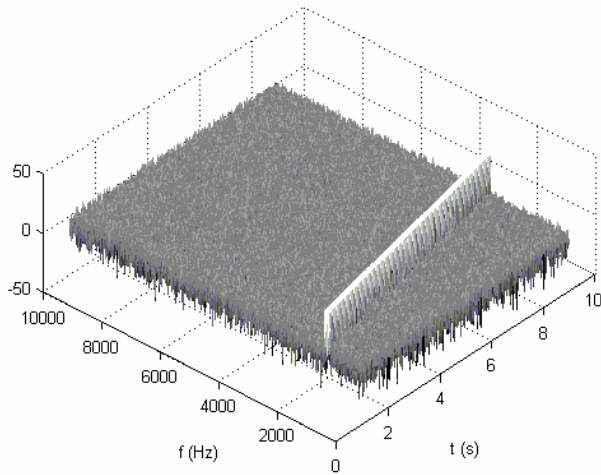


$$|S(t_0, f)|^2 = \text{spectrogram}$$

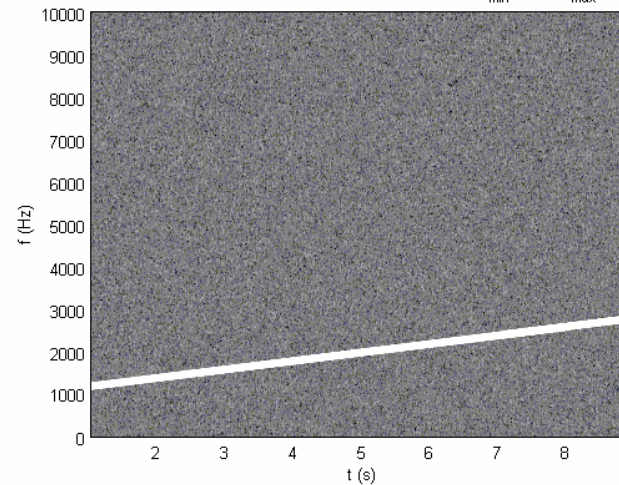


$$S(t_0, f) = F(s(t) \times \omega_L(t - t_0))$$

Narrow Band NPL (dB ref 1 $\mu\text{Pa}^2\text{Hz}^{-1}$, fichier: son2.wav; t_{\min} (s)=1; t_{\max} (s)=9



Narrow Band NPL (dB ref 1 $\mu\text{Pa}^2\text{Hz}^{-1}$, fichier: son2.wav; t_{\min} (s)=1; t_{\max} (s)=9



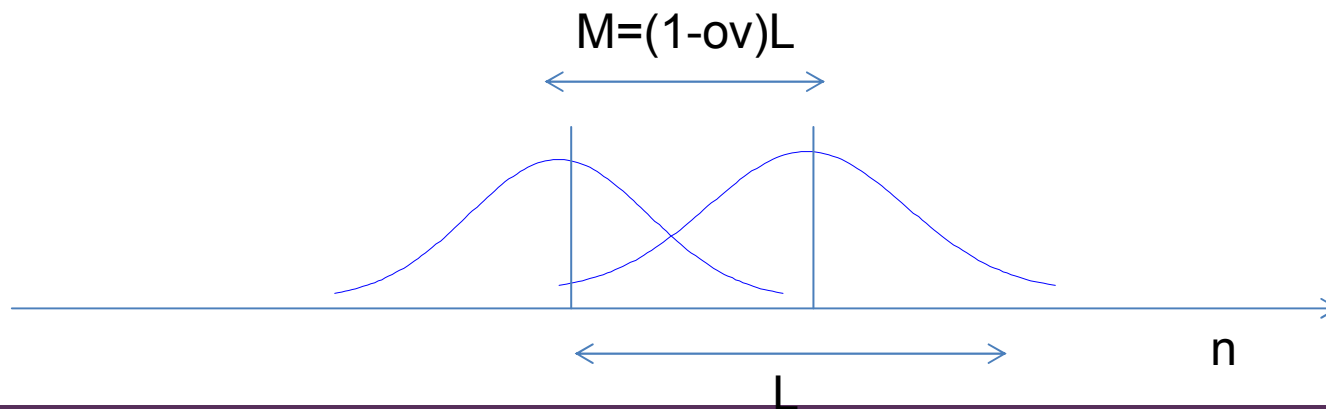
The short-term Fourier Transform (STFT) The Spectrogram

Numerical implementation:

$$S(iM, j) = FFT_L(s(n) \times w_L(n - iM)), j \in \{0, \dots, L-1\}$$

$$t(s) = iM$$

$$f(\text{Hz}) = \frac{j}{L} f_e$$



- live,
 - Linear Frequency modulation
 - Dolphin's whistles



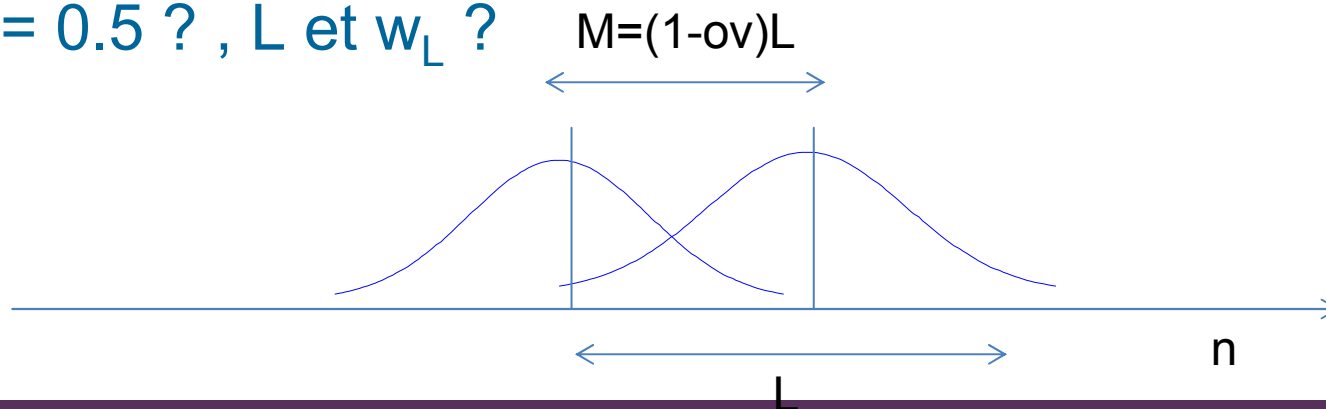
The short-term Fourier Transform (STFT) The Spectrogram

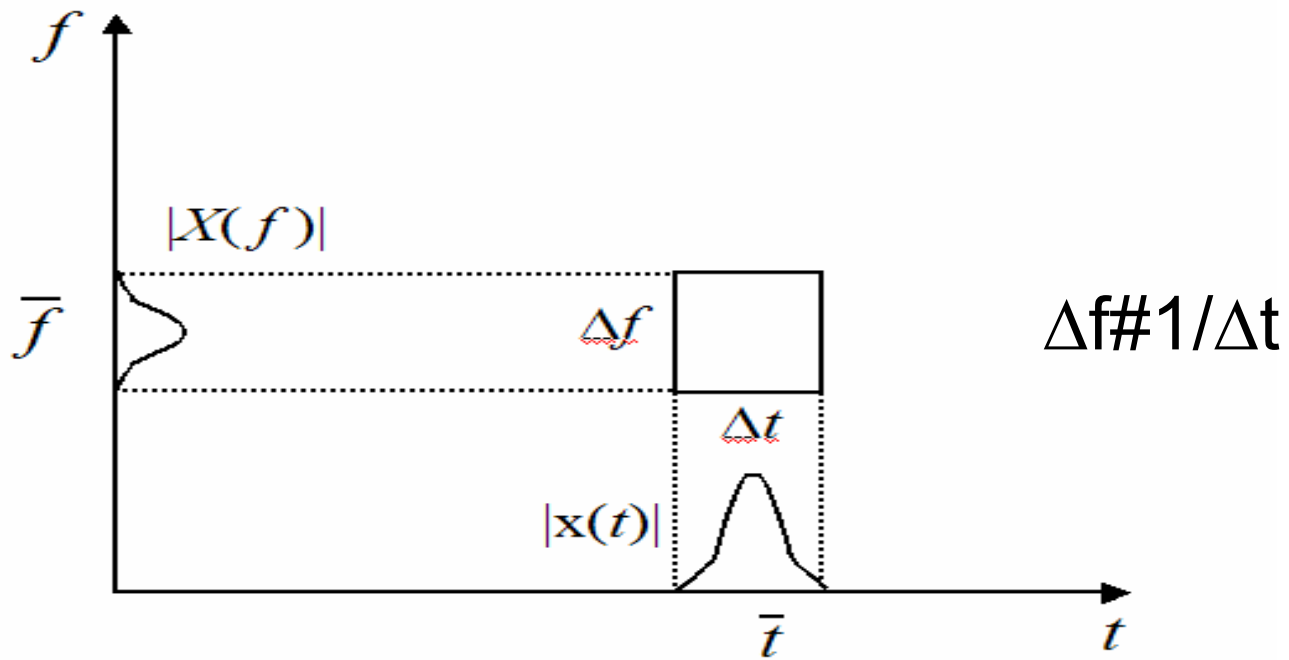
The degrees of freedom of the STFT

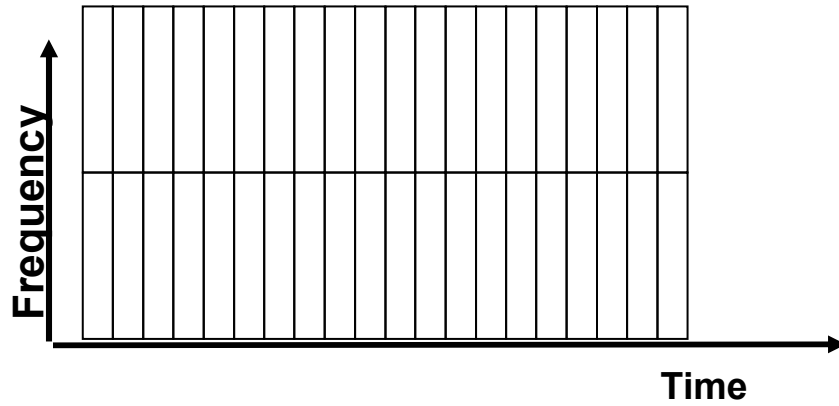
- window length : L
- window type : w_L
- window overlap : ov

The choice of the degrees of freedom determines the properties of the time-frequency representation

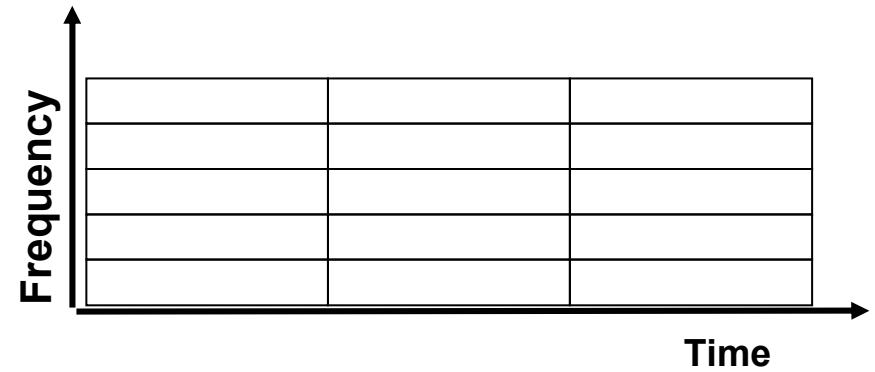
$ov = 0.5 ? , L$ et $w_L ?$



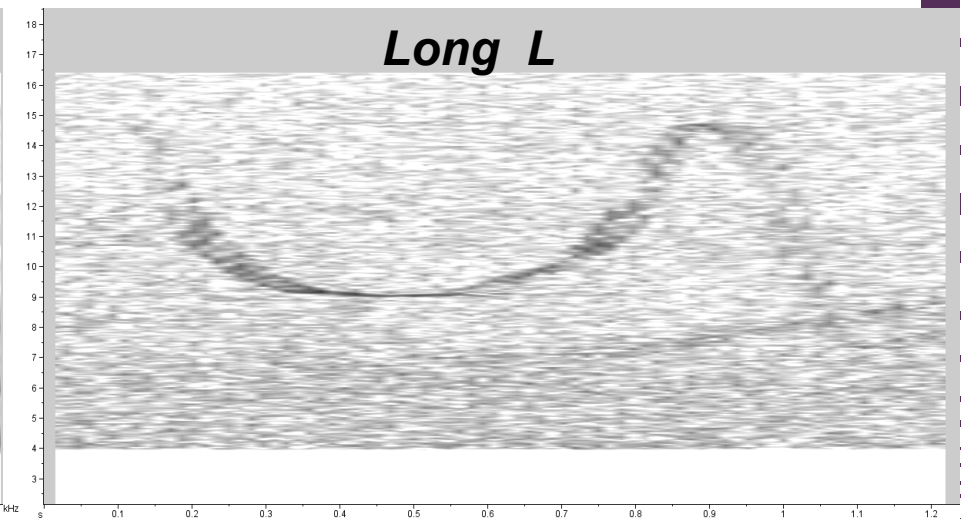
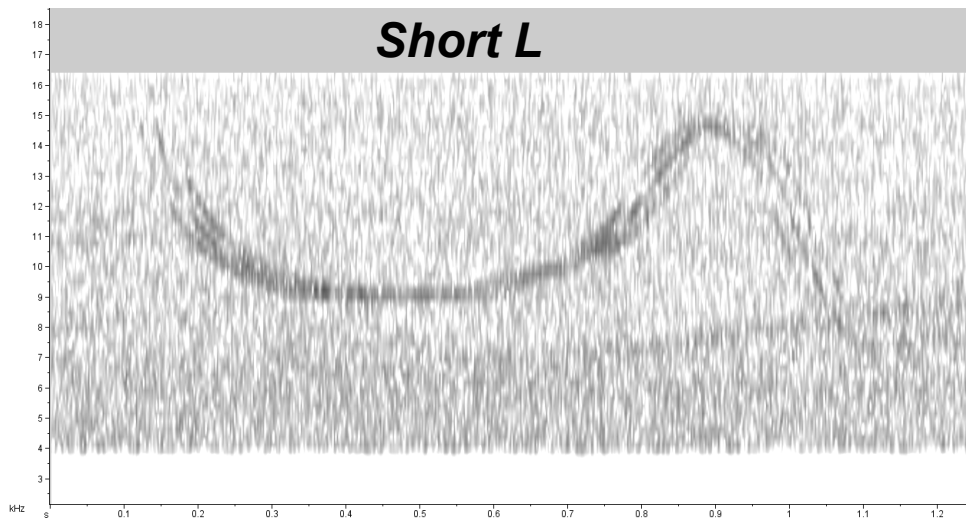




L= small:
 Good time resolution
 Bad frequency resolution



L= high :
 Bad time resolution
 Good frequency resolution



The short-term Fourier Transform (STFT) The Spectrogram

The degrees of freedom of the STFT:

- the window length : L
compromise between time and frequency resolution
- the type of window : w_L
compromise between frequency and amplitude resolution
- the window overlap : $ov > 0.5$



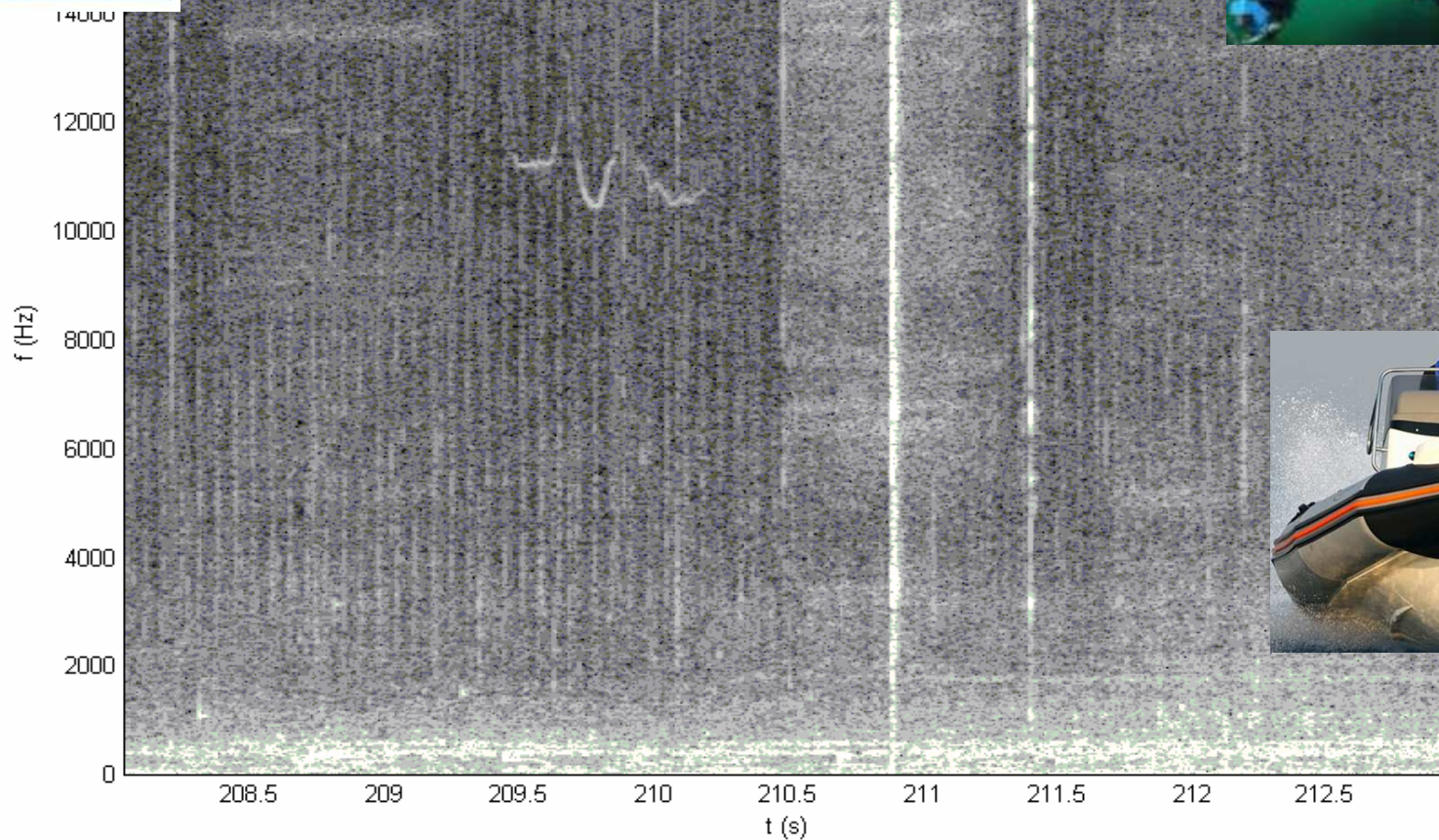
- live on real data :
sifflement.wav



Extraction of key parts of a spectrogram



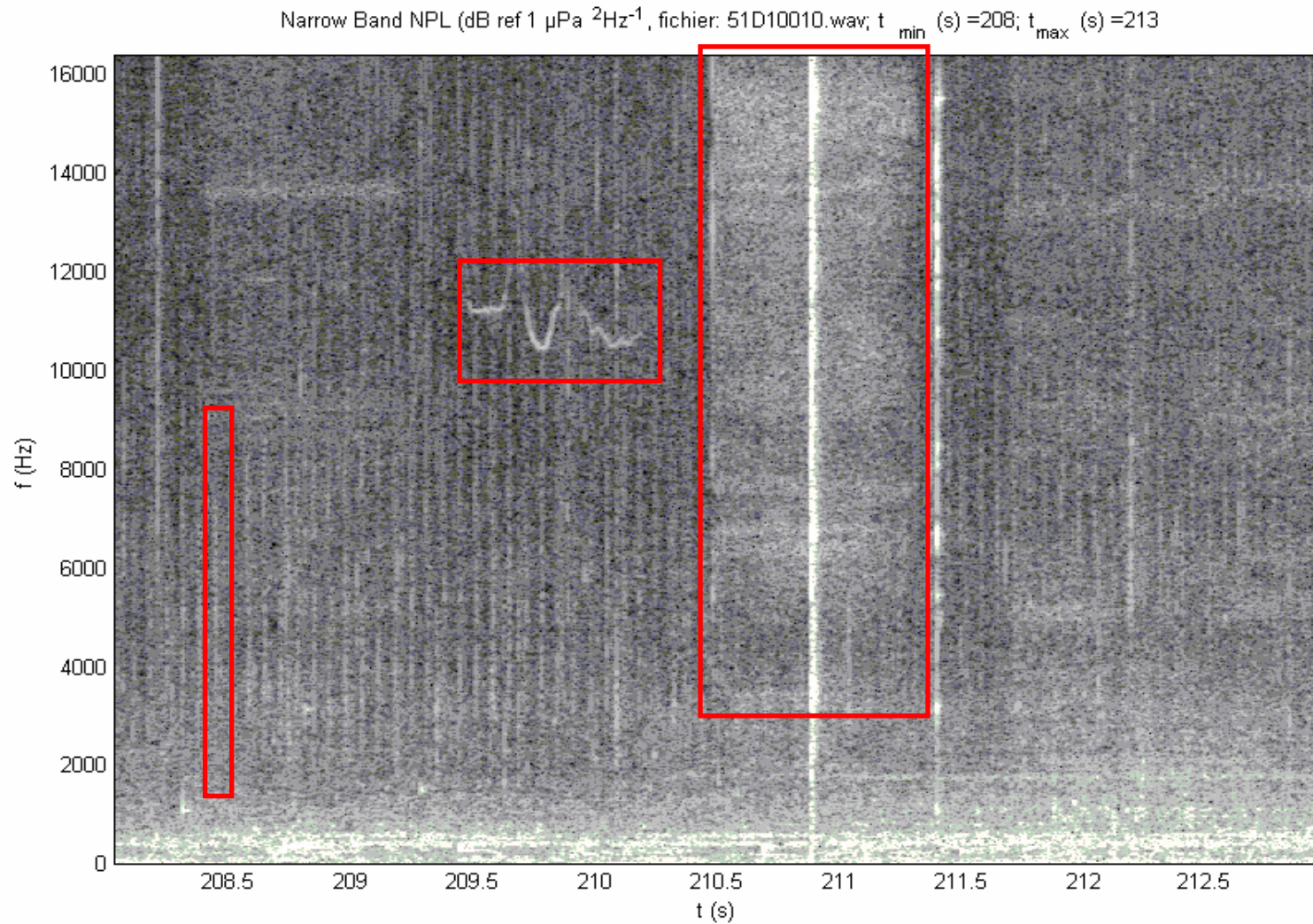
Narrow Band NPL (dB ref 1 $\mu\text{Pa}^2\text{Hz}^{-1}$, fichier: 51D10010.wav; t_{\min} (s)=208; t_{\max} (s)=



Lucia



Extraction of key parts of a spectrogram



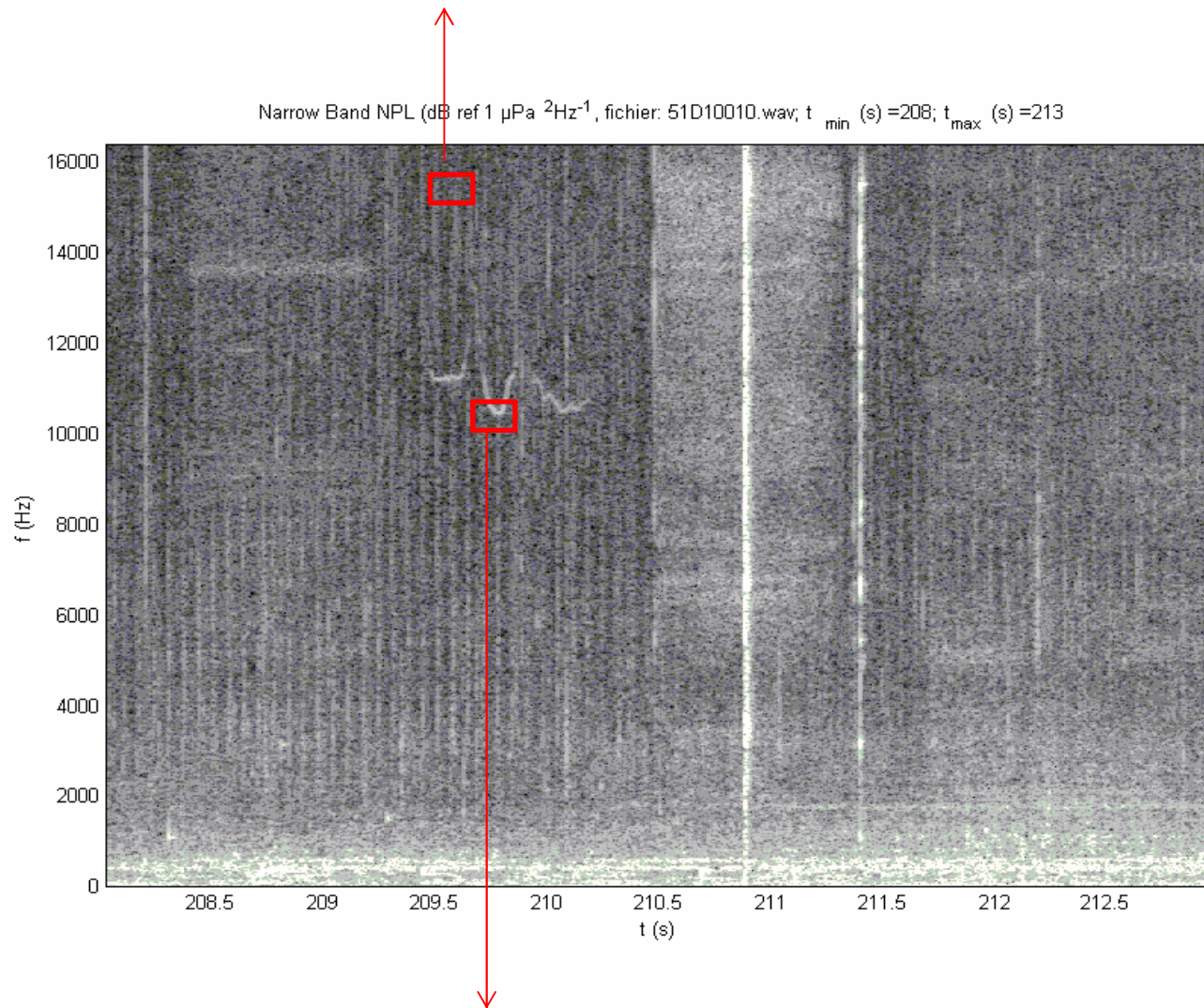
Extraction of key parts of a spectrogram

Method

- Compute a spectrogram
- Segment the spectrogram into binary areas
 - 0=> H0 absence of target signal
 - 1=> H1 presence of target signal

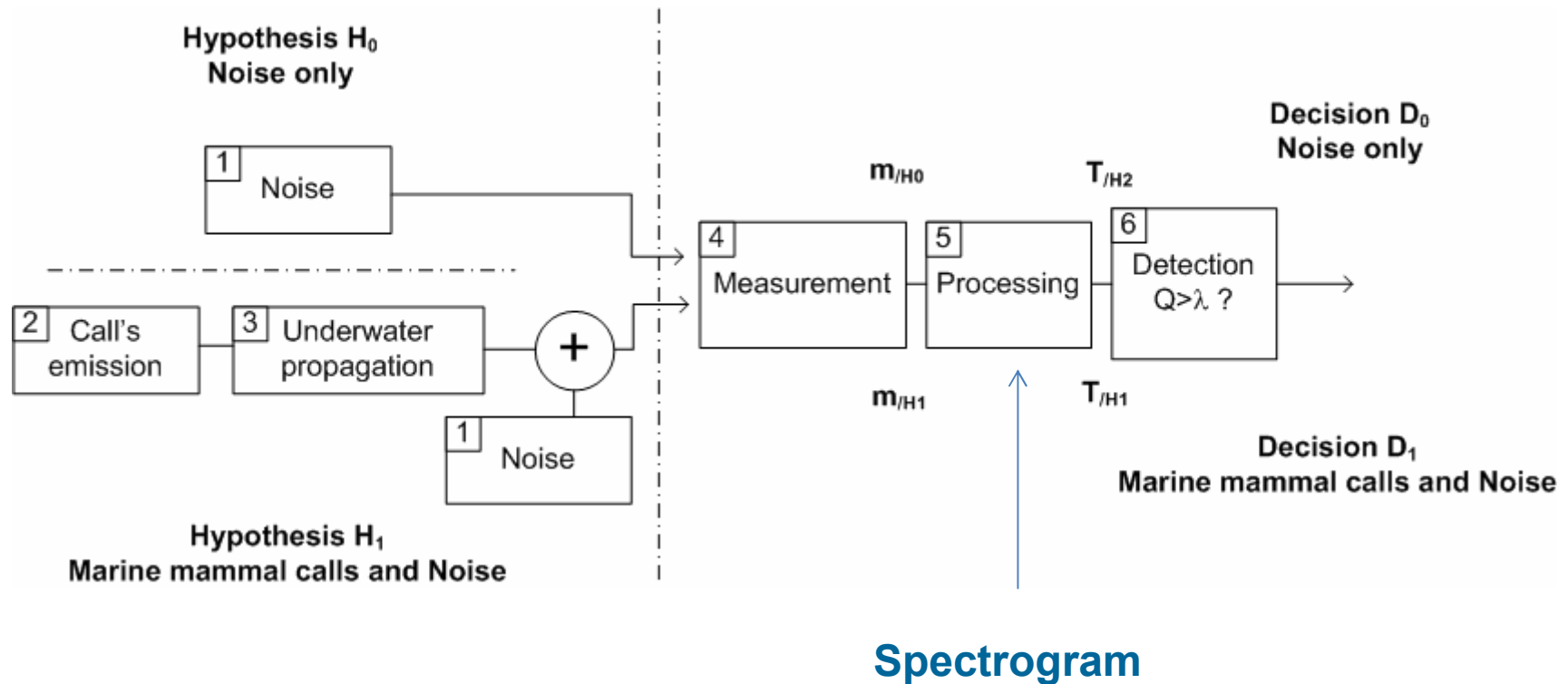


H0: signal absent, if D0 : good decision, if D1 : bad decision – false alarm (Pfa)

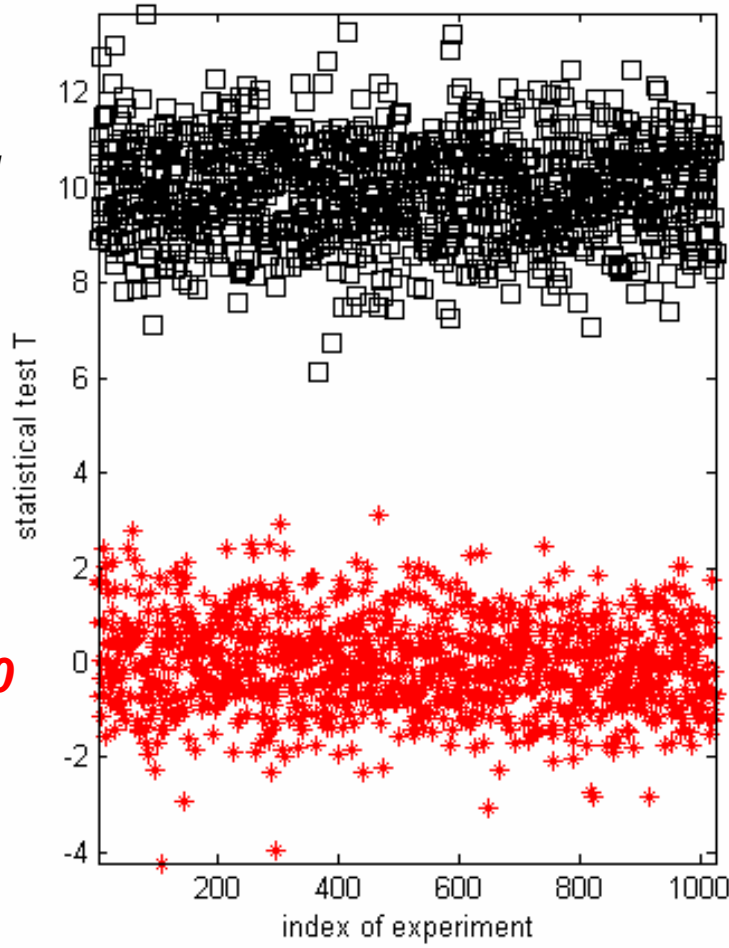


H1: signal present, if D1 : good decision (Pd), if D0 : no bad decision

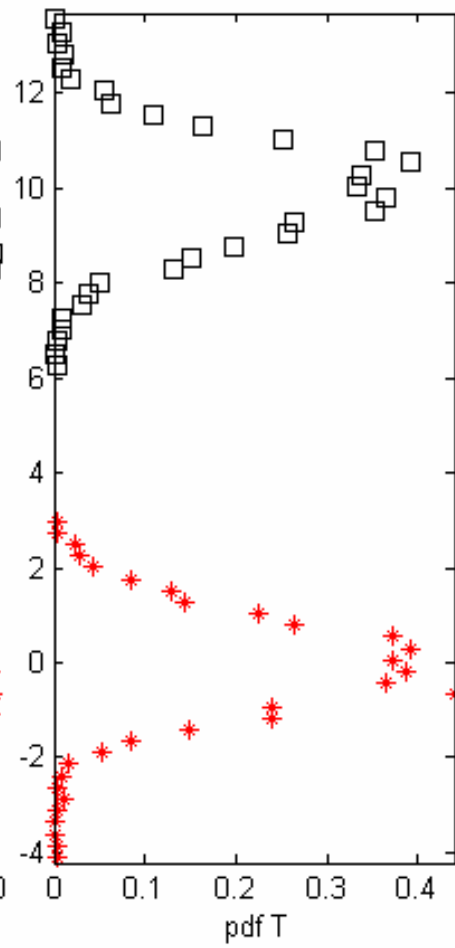
General architecture of a signal detector



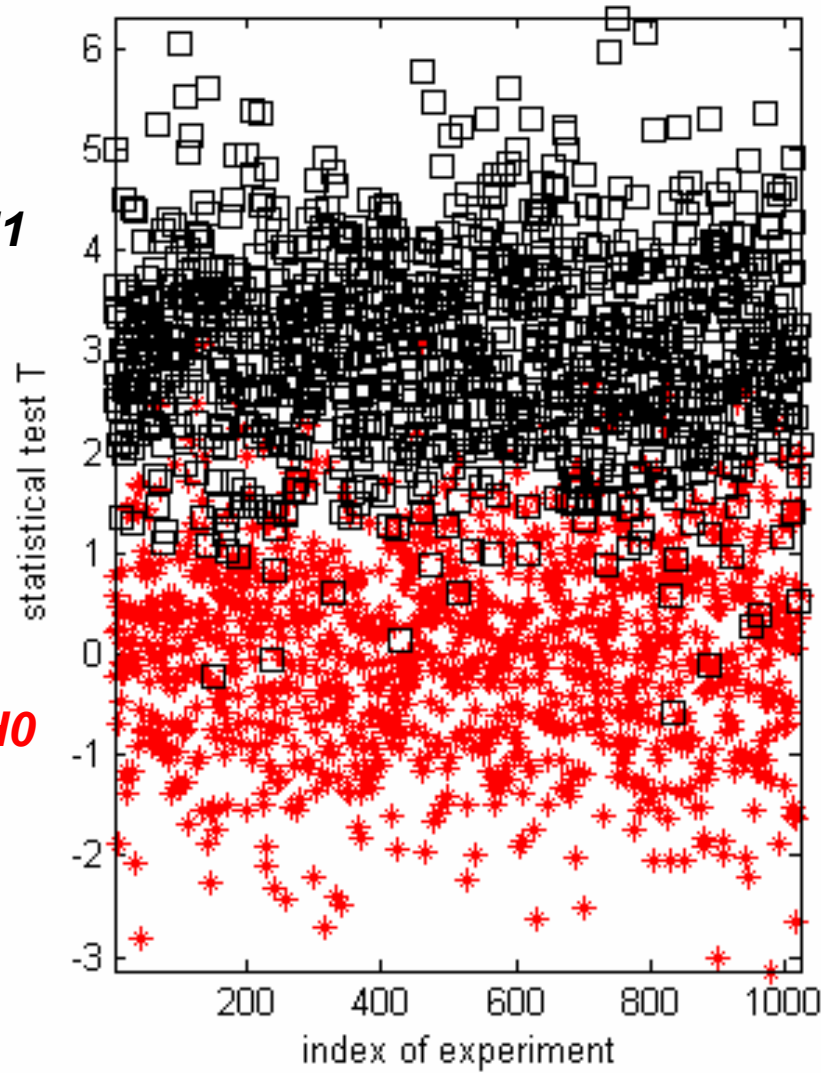
T/H1



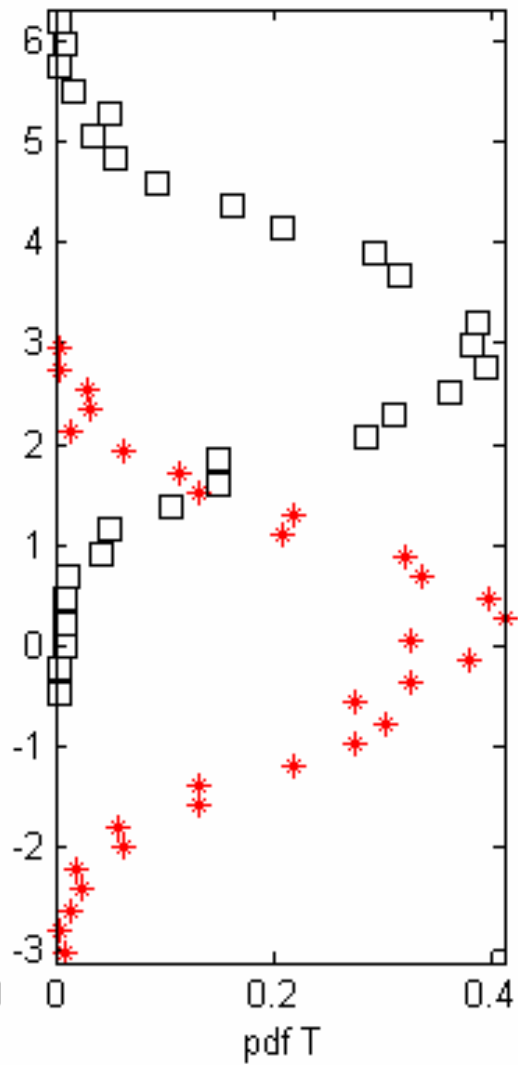
T/H0



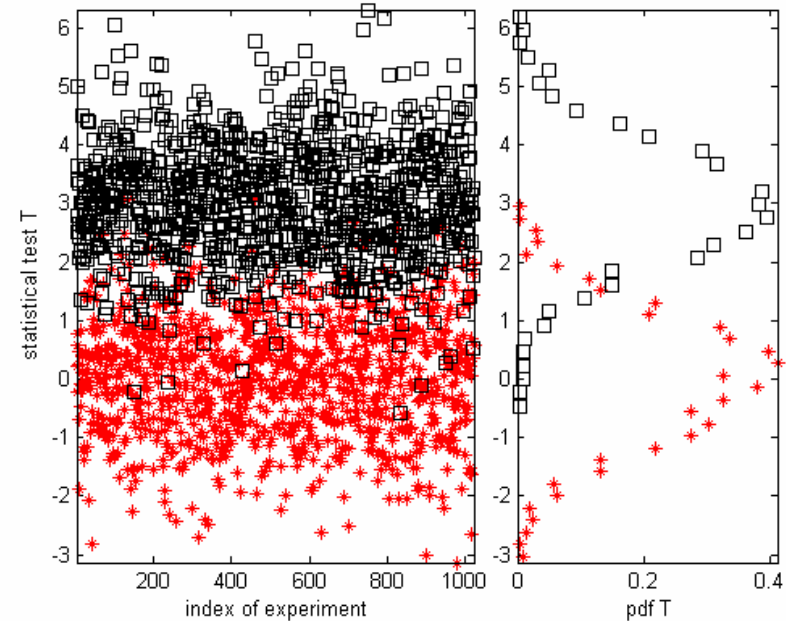
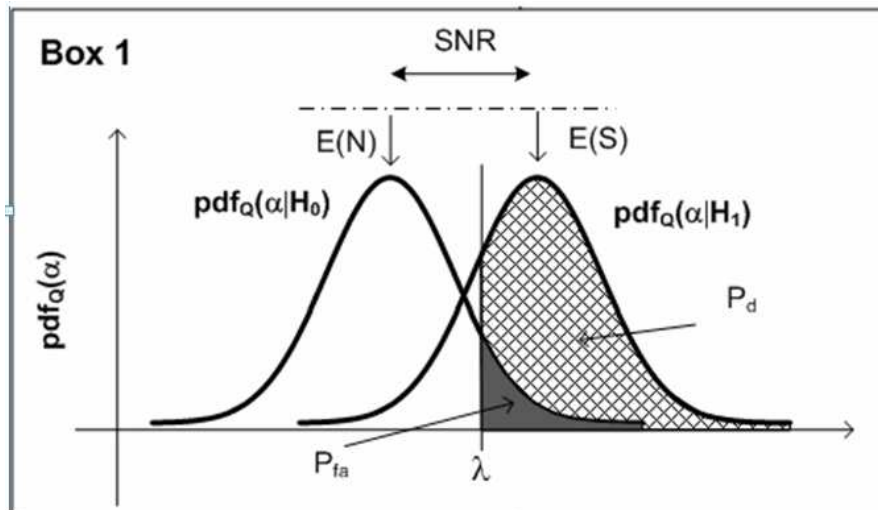
T/H1



T/H0



Pfa et Pd



$$P_{fa} = \int_{\lambda}^{+\infty} \text{pdf}_Q(\alpha|H_0) d\alpha = 1 - \text{cdf}_Q(\lambda|H_0)$$

$$P_d = \int_{\lambda}^{+\infty} \text{pdf}_Q(\alpha|H_1) d\alpha = 1 - \text{cdf}_Q(\lambda|H_1)$$

Detector with a constant false alarm rate

- In many application of signal detection, $f_Q(q)|H_1$ is not well known.
- We define a detector with constant false alarm rate

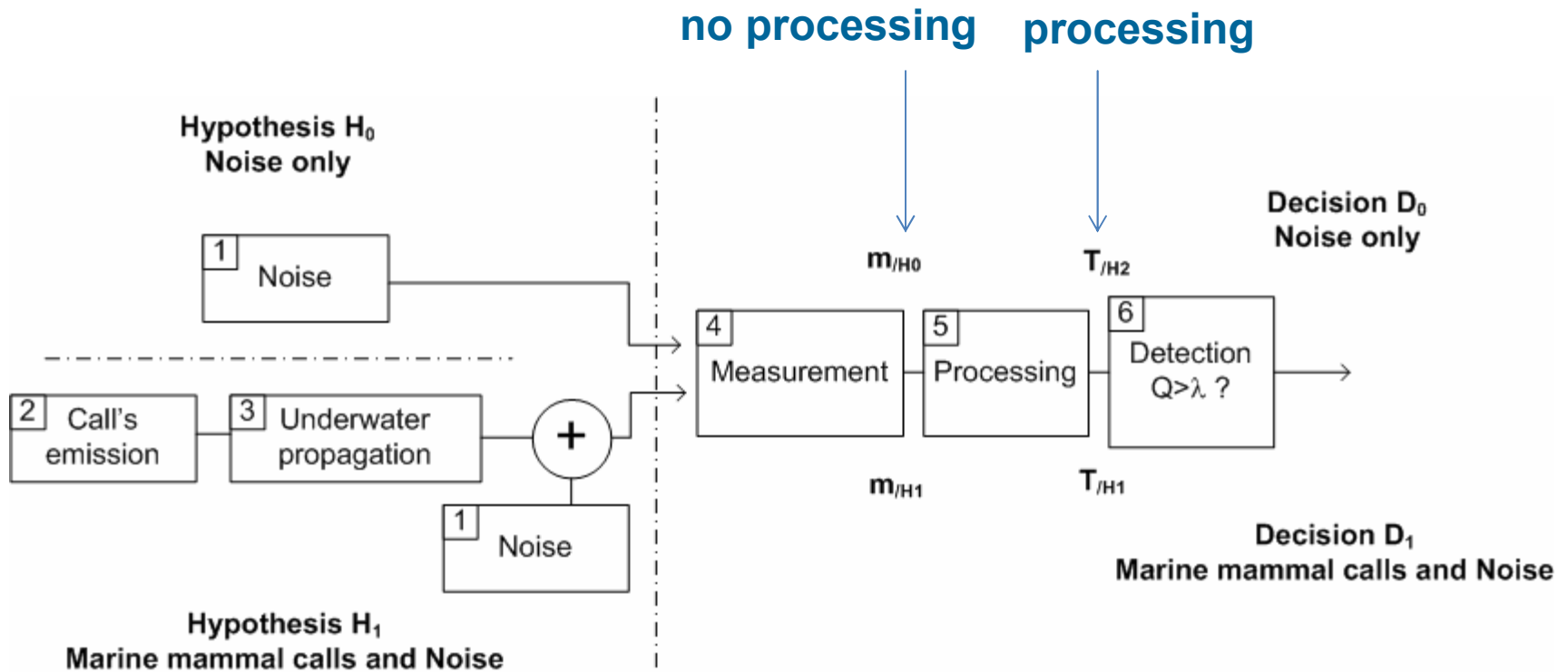
$$P_{fa} = 1 - cdf_Q(\lambda|H_0)$$

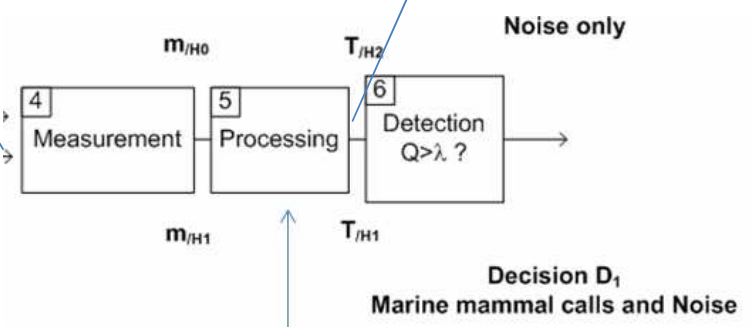
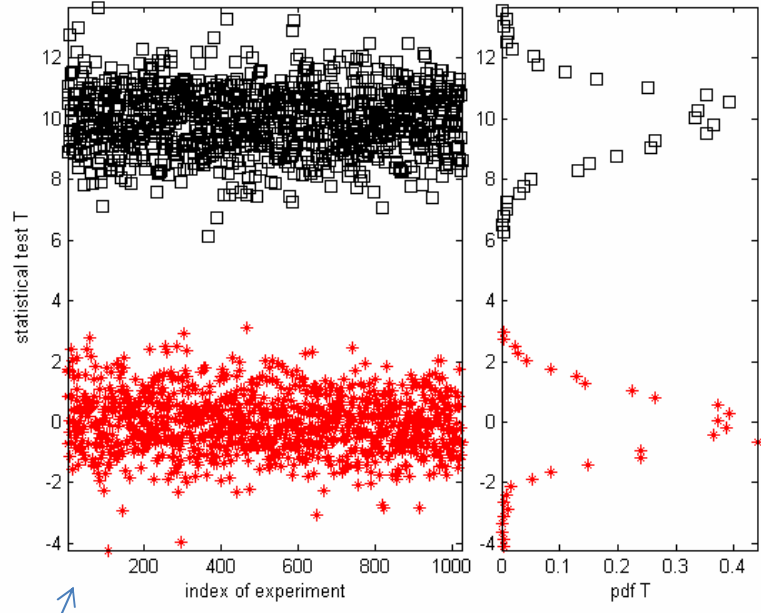
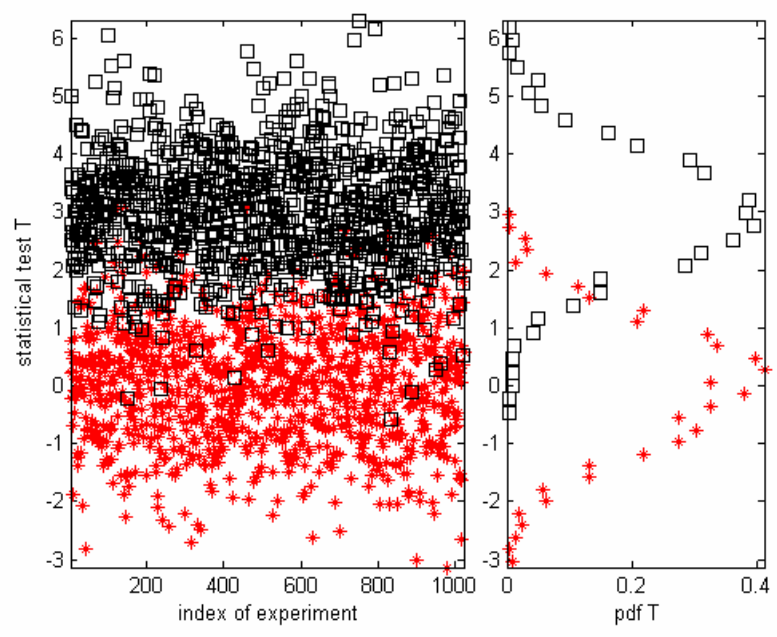
$$\lambda = cdf_Q^{-1}(1 - P_{fa}|H_0)$$

$$Pd = 1 - cdf_Q(cdf_Q^{-1}(1 - P_{fa}|H_0)|H_1)$$



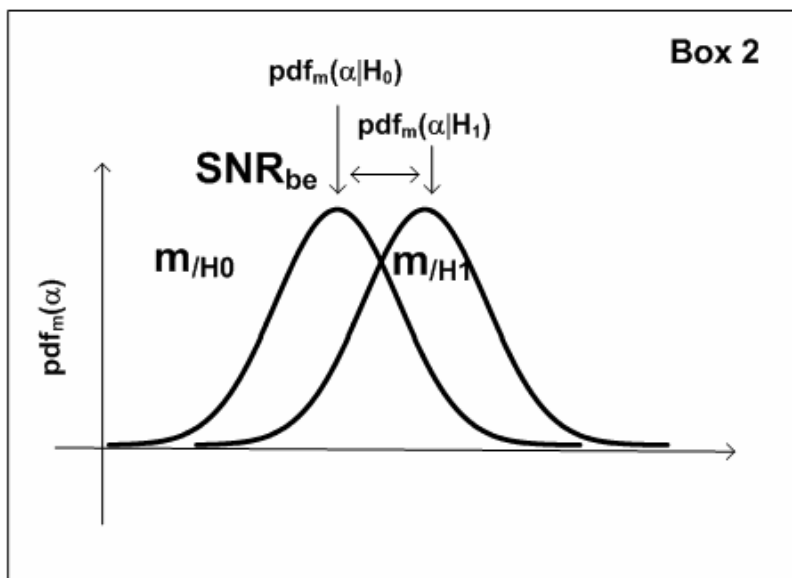
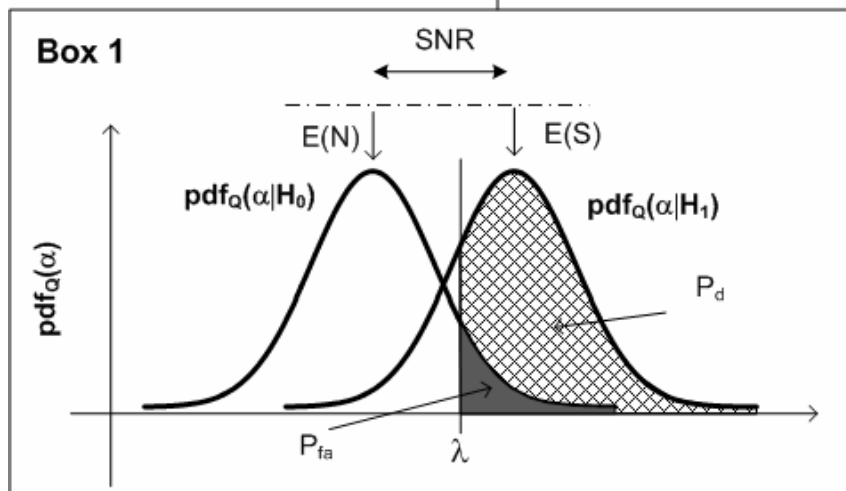
Interest of data processing for signal detection



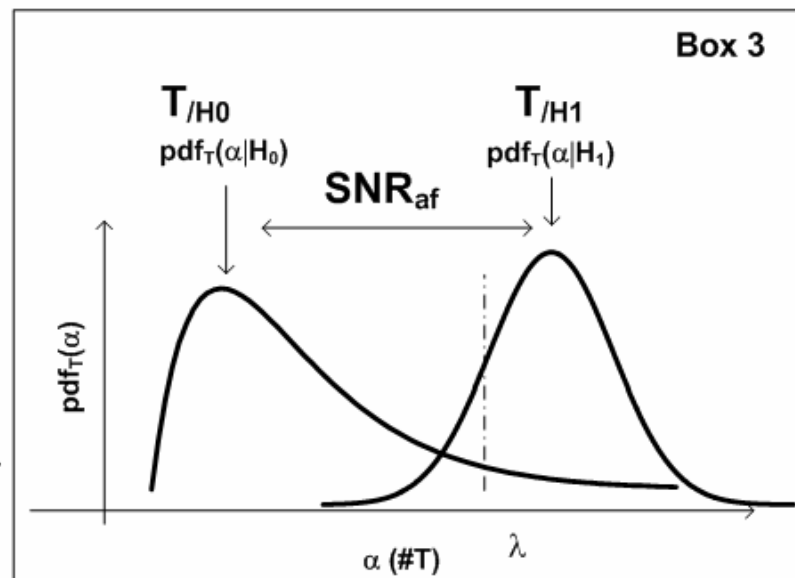


Spectrogram





SNR_{af} > SNR_{be} ?



After block 5
« processing »

The processing: computation of the spectrogram

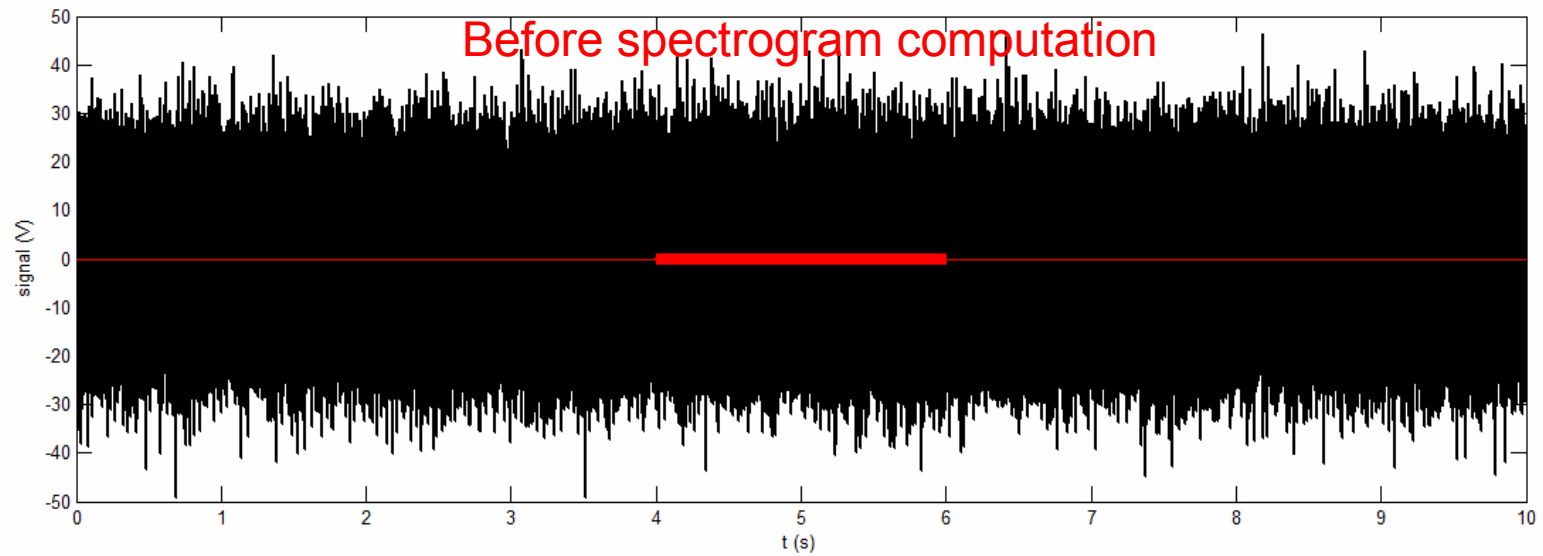
$$f_Q^{H_0}(q) = \frac{1}{L\sigma^2} \exp\left(-\frac{q}{L\sigma^2}\right), q \geq 0$$

$$F_Q^{H_0}(q) = 1 - \exp\left(-\frac{q}{L\sigma^2}\right)$$

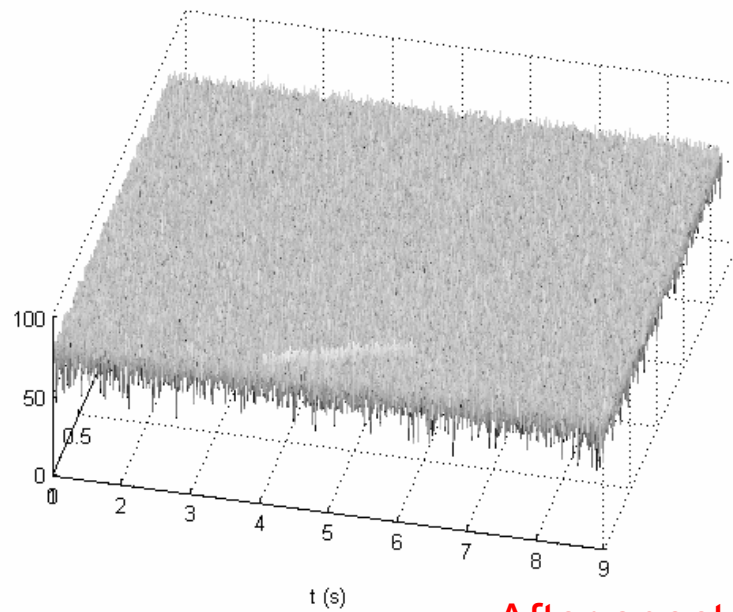
$$\lambda = L\sigma^2 \log(P_{fa})$$

For a stationary
Gaussian noise

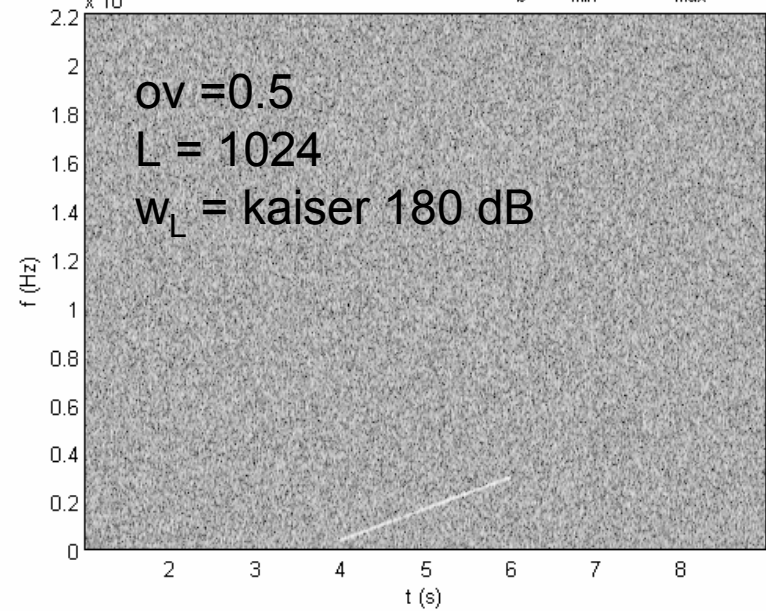




Narrow Band NPL (dB ref 1 $\mu\text{Pa}^2\text{Hz}^{-1}$, fichier: lfm_bruit; t_{\min} (s)=1; t_{\max} (s)=9

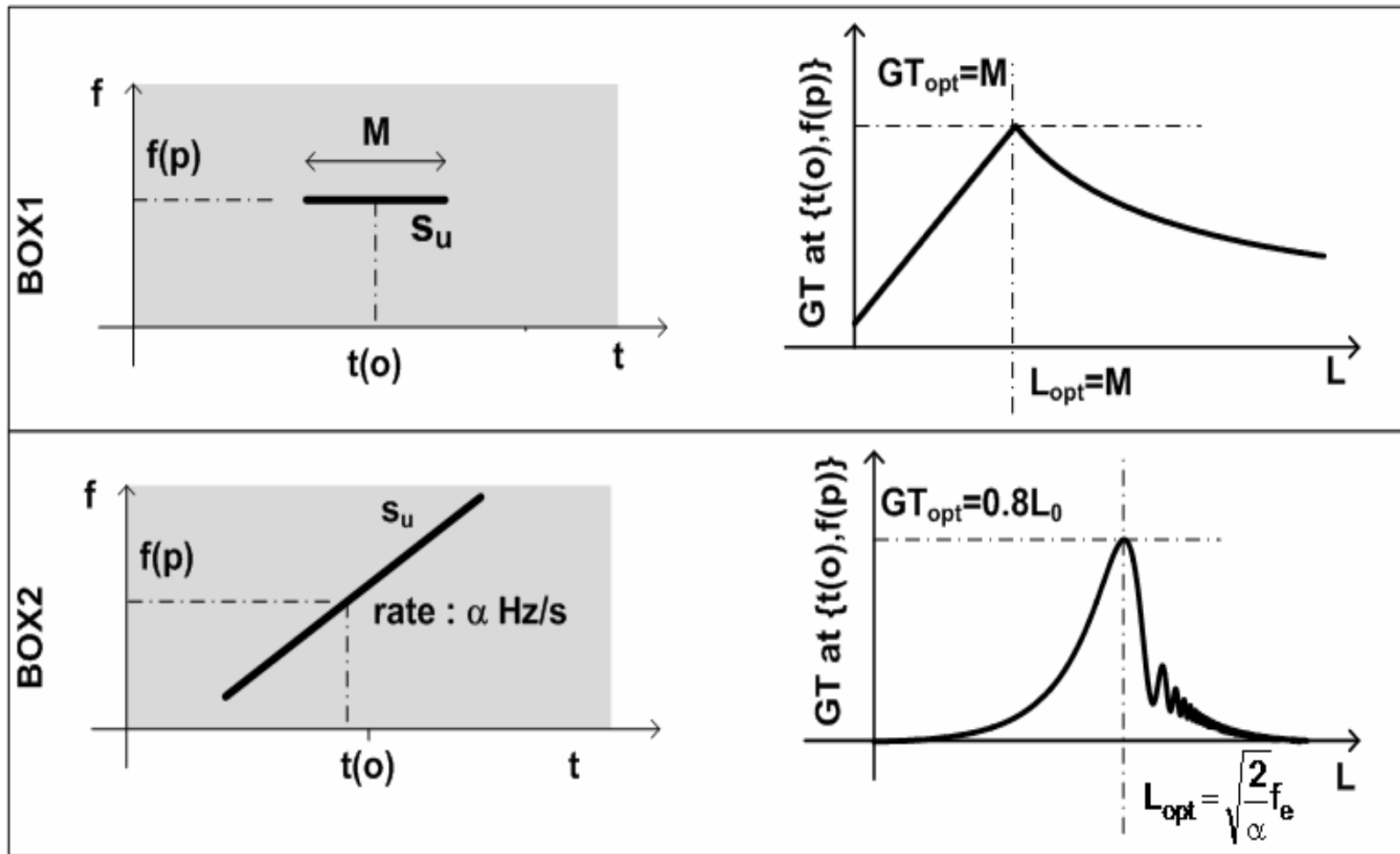


Narrow Band NPL (dB ref 1 $\mu\text{Pa}^2\text{Hz}^{-1}$, fichier: lfm_bruit; t_{\min} (s)=1; t_{\max} (s)=9

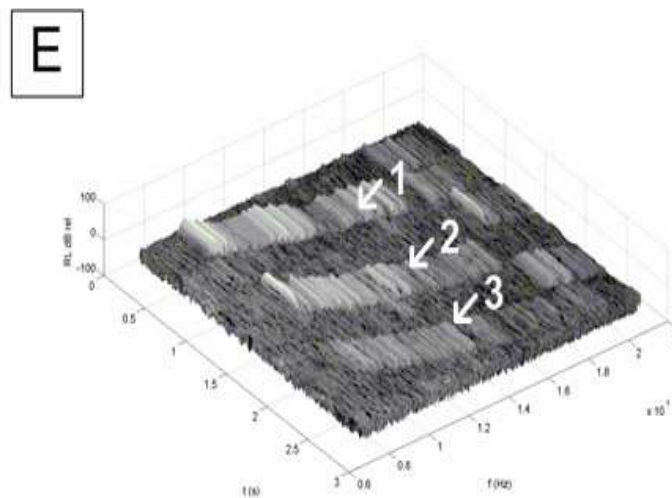
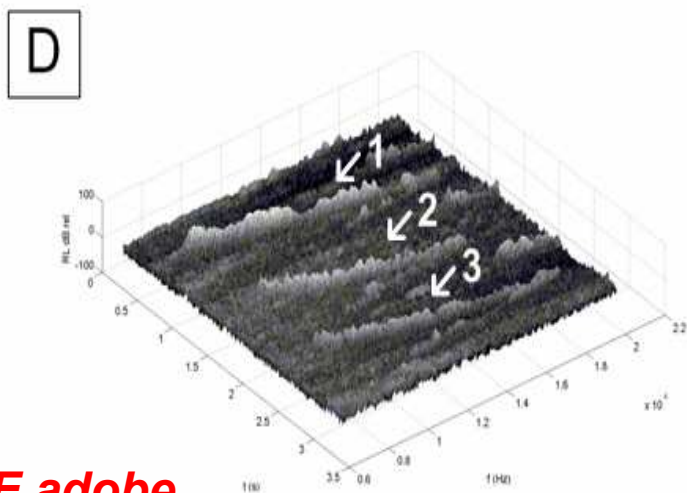
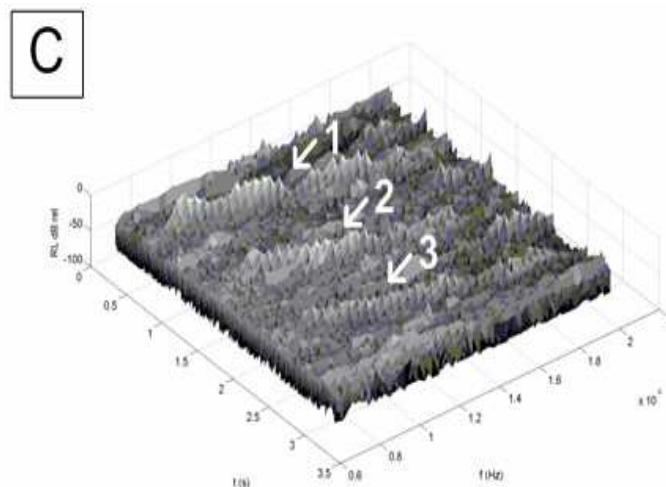
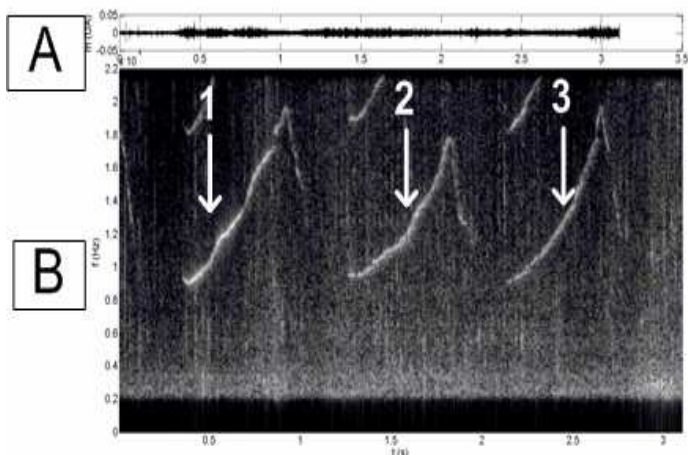


After spectrogram computation

Processing gain = function (L, signal)



Bottlenose dolphins, Molène

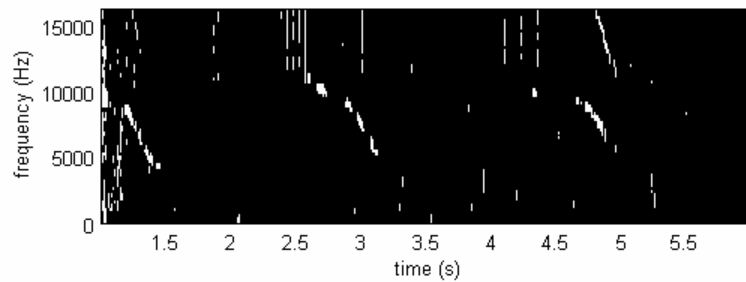
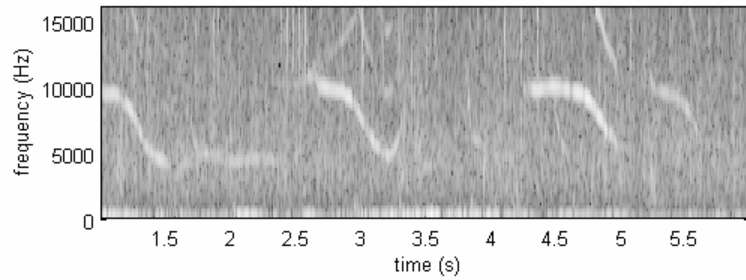


LIVE adobe

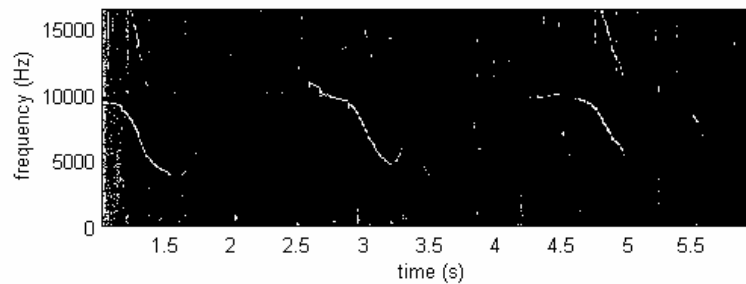
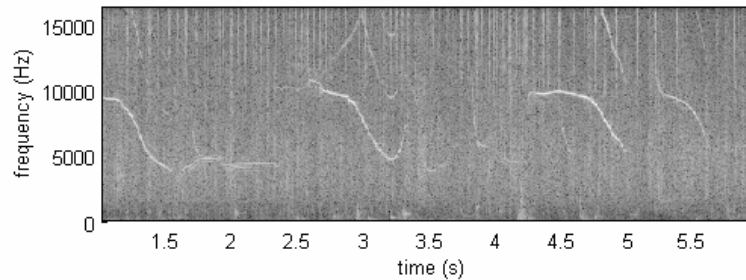
$P_{fa}=10^{-6}$

Example 2 : influence of L

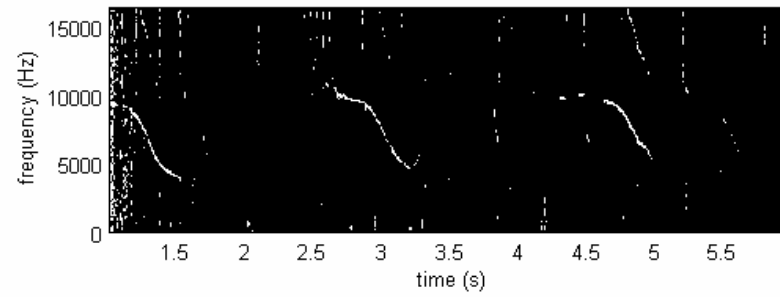
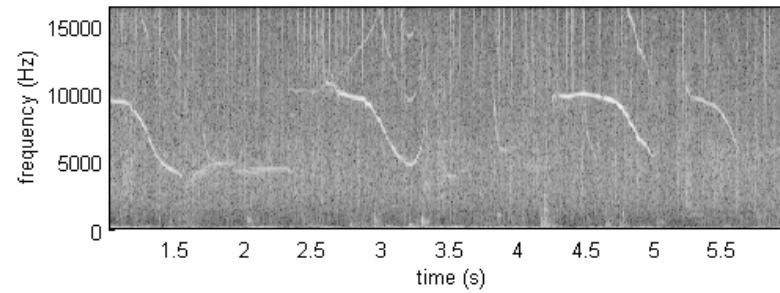
L=128



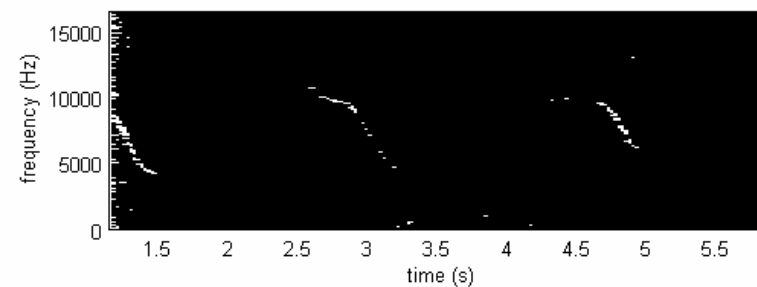
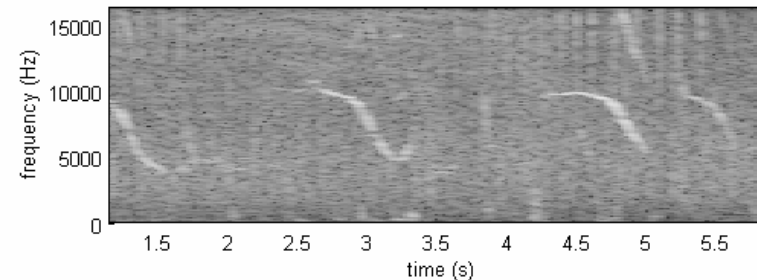
L=1024



L=512

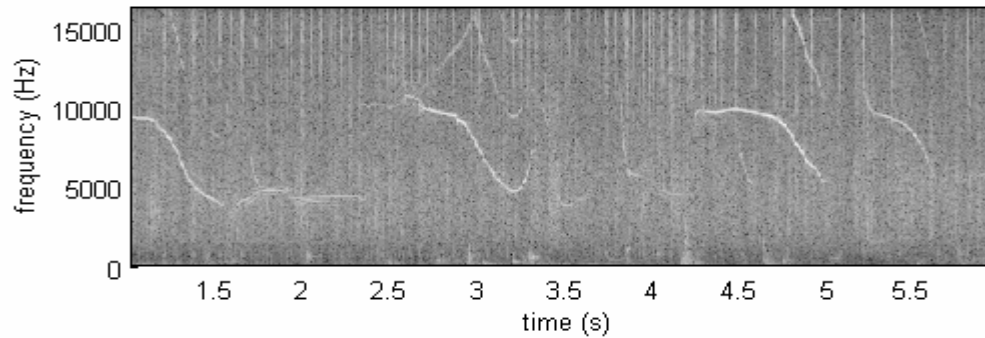


L=8192

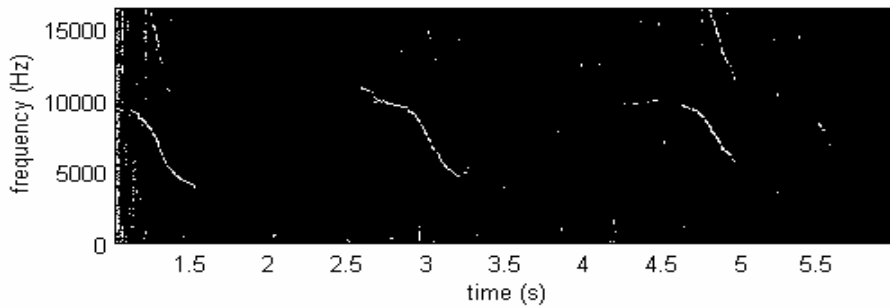


Example 1 : influence of the Pfa

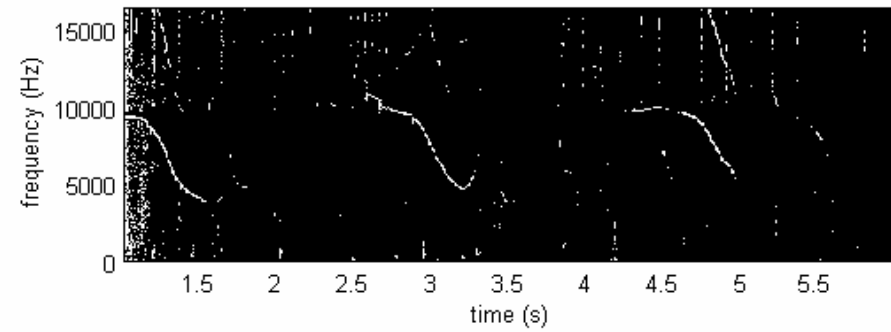
L=1024



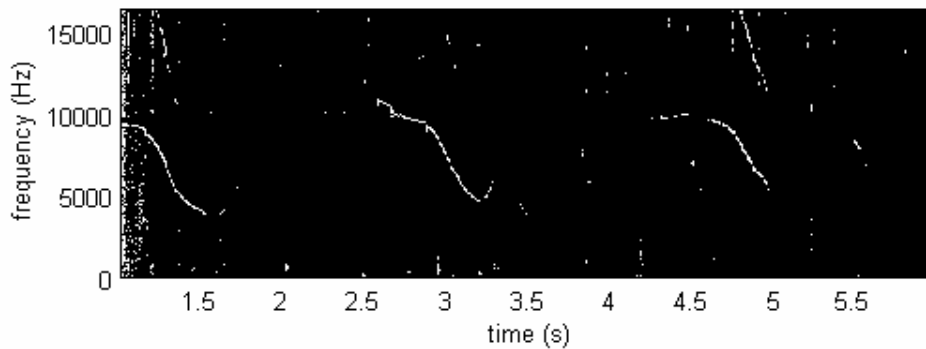
Pfa=10⁻⁸



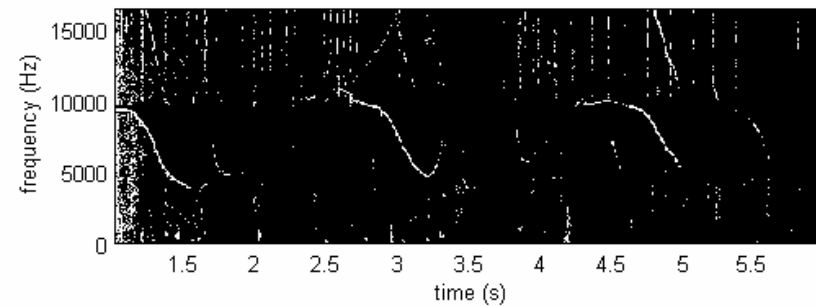
Pfa=10⁻⁴



Pfa=10⁻⁶



Pfa=10⁻³



Specific literature

General

- R. Urick - Principles of Underwater Sound
- W.W.L. Au & M.C. Hastings - Principles of Marine Bioacoustics

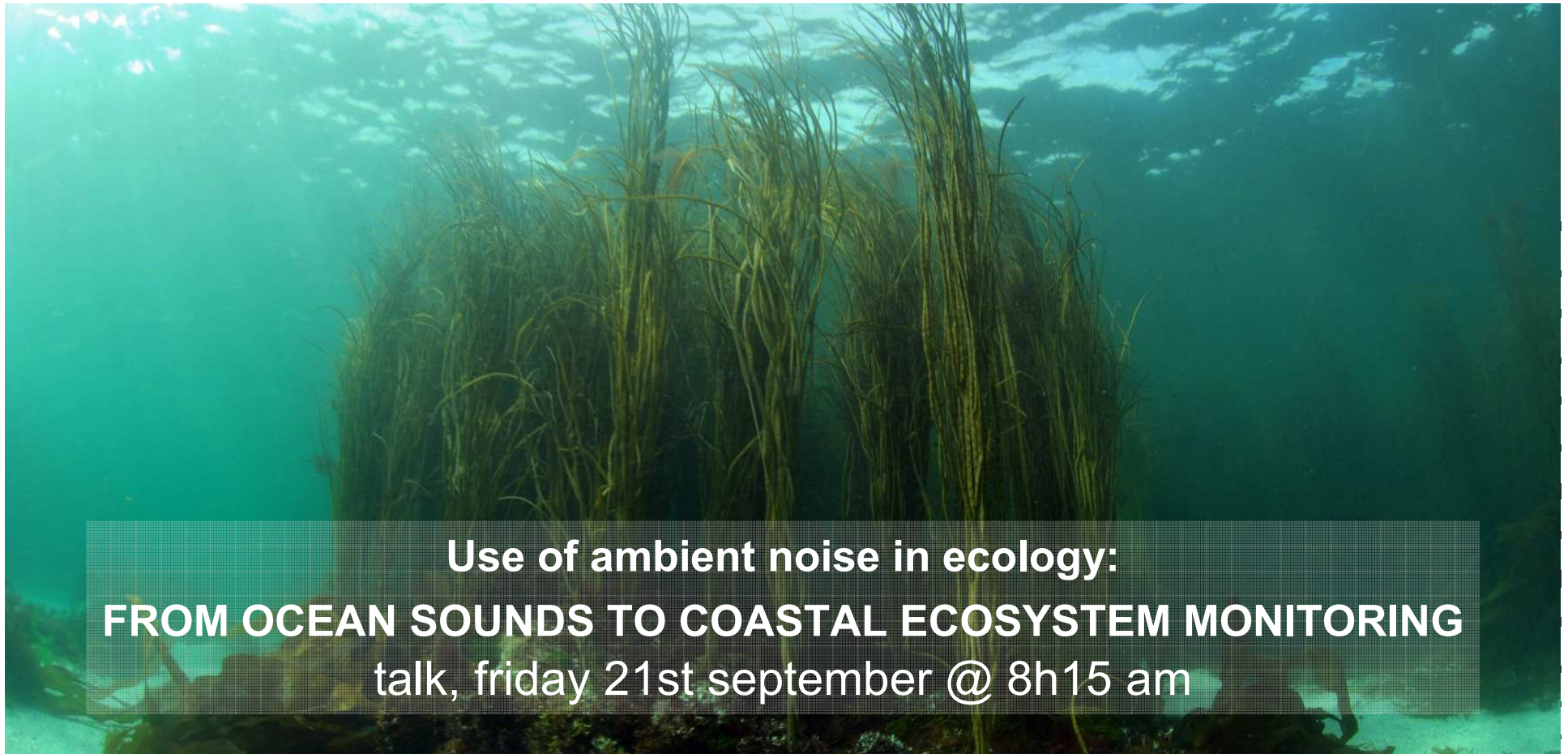
Signal processing (detection, time-frequency)

- Hlawatsch, F. & Boudreaux-Bartels, G. F. (1992), 'Linear and quadratic time-frequency signal representations', Signal processing magazine, IEEE 9(2), 21-67.
- Kay, S. (1998), Fundamentals of statistical signal processing, detection theory, Prentice Hall, New jersey.

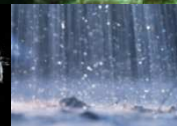
Outline

- Introduction
- Introduction to sound
- Measurement chain
- Spectral analysis of acoustic measurements
- Time-frequency representation
- **Applied examples from our own research**

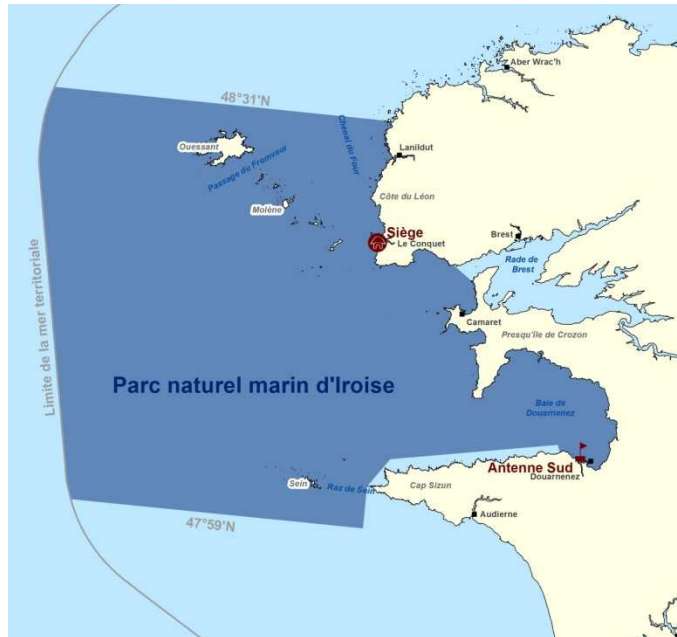
Environmental applications - Molène 2011: dolphins & ships



Use of ambient noise in ecology:
FROM OCEAN SOUNDS TO COASTAL ECOSYSTEM MONITORING
talk, friday 21st september @ 8h15 am



Study site



- weather station
- models (weather, tides, currents...)



Study site

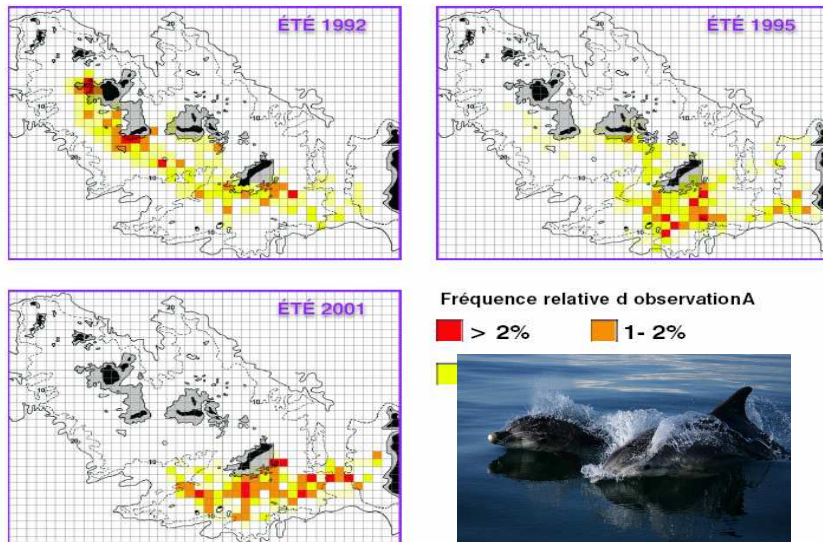


Figure 7

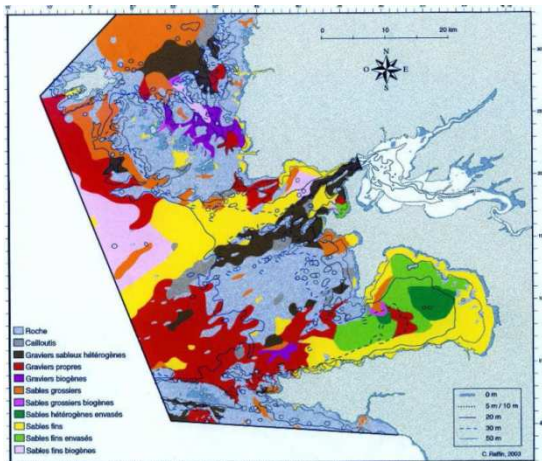
Répartition spatiale des grands dauphins au sein de l'archipel de Molène au cours des étés 1992, 1995 et 2001.

Resident population of ~40 bottlenose dolphins
(*Tursiops truncatus*)

6-10m



800 – 1000 animal species
300 - 400 species of algae & plants, (J. Grall, OSU RdB)



Alpheus macrocheles
1000 / ha
(Grall, J. OSU Brest, 2011)



Echinus esculentus
2000 / ha (100mx100m)
(Grall, J. OSU Brest, 2011)

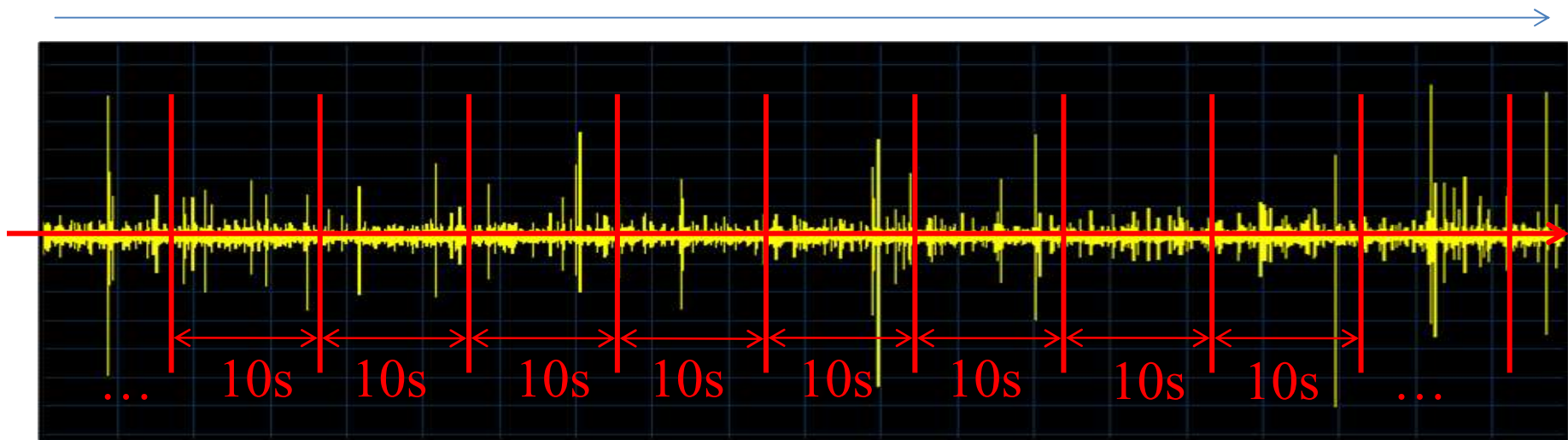
Objectives

- How to describe the soundscape of Molène: which acoustic descriptors? Which algorithms ?
- Reconstruct an acoustic landscape through time series (3x6 months) of the descriptors
- Analyse the time series: their contribution to the description and understanding of the environment

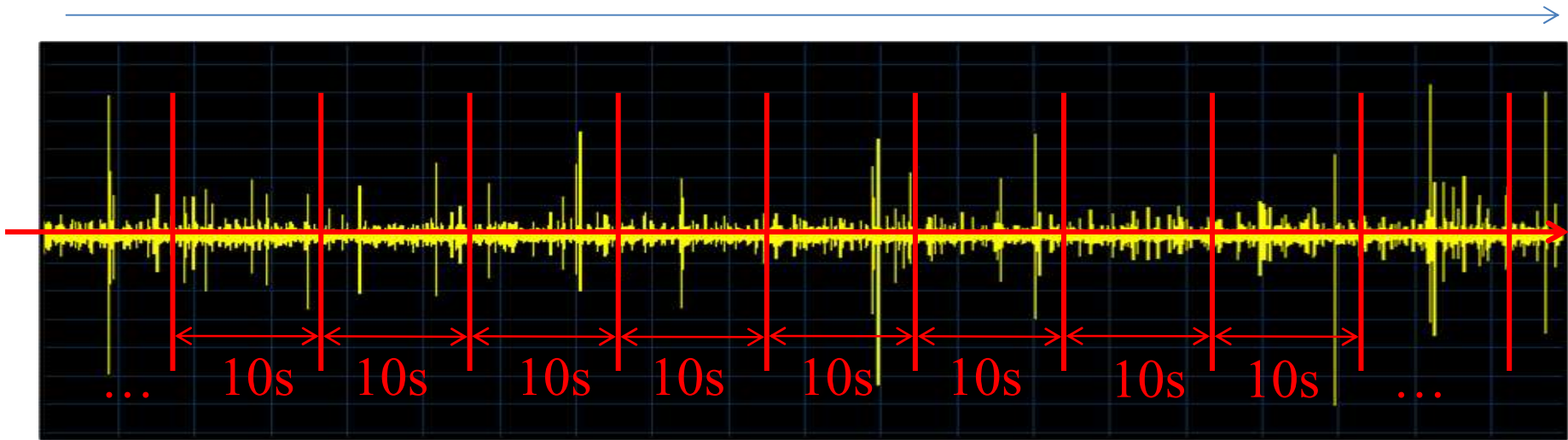
- Biophony (bottlenose dolphin, benthic activity,)
- Géophony (wind, rain)
- Anthropophony (mainly boats)

Some numbers

- 1 year = signal processing development & pilot experiments
- 6 months observations (3 terabytes raw data, 3 recorders 3x15 k€ , boat trips ~ 6 k€)

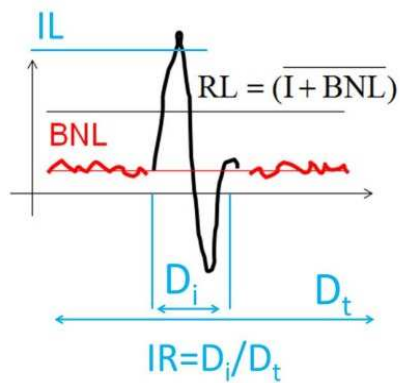


- two months of data processing & analysis
 - => 35 days PC calculations
 - => 1.5 Mio segments

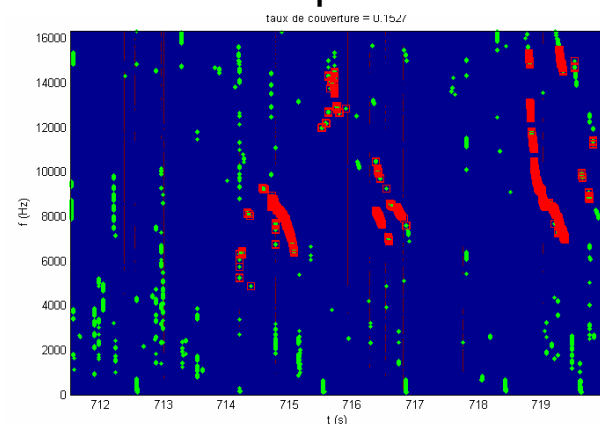


Processing algorithms

Ambient noise



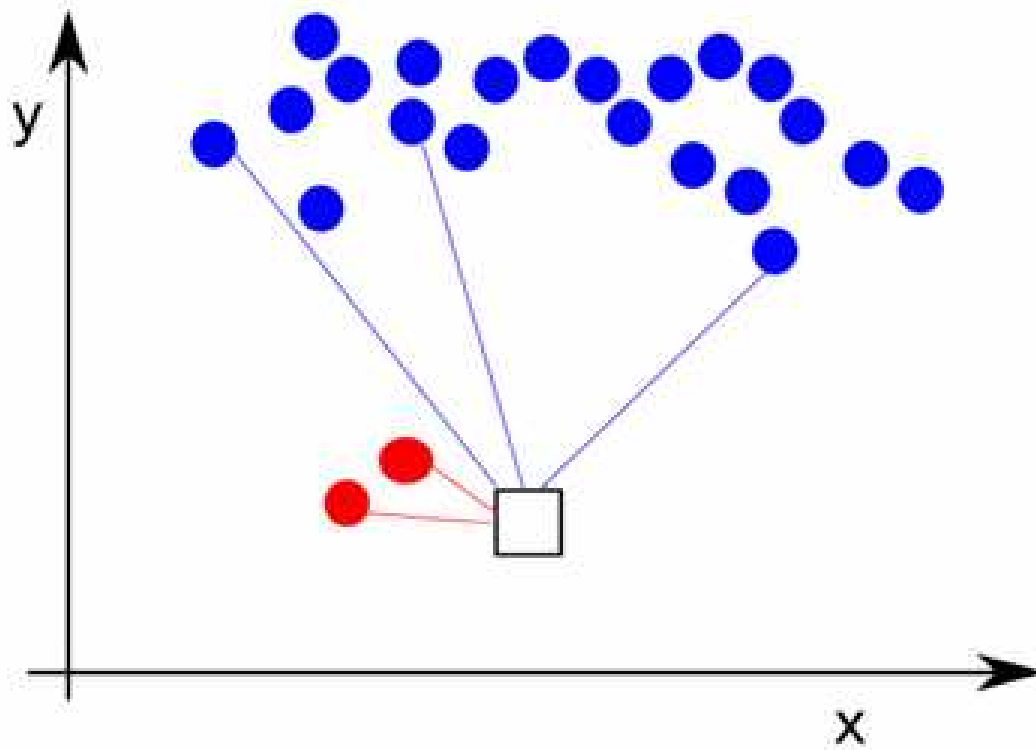
Dolphin detection



Acoustic descriptors

Ambient noise vs. close sources

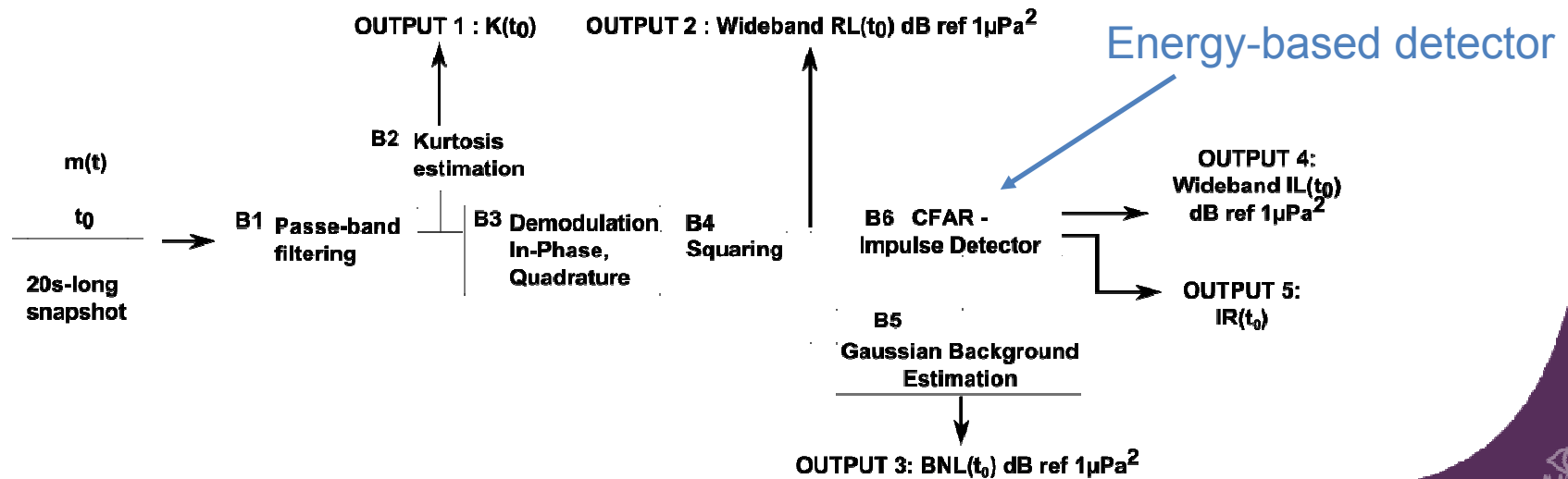
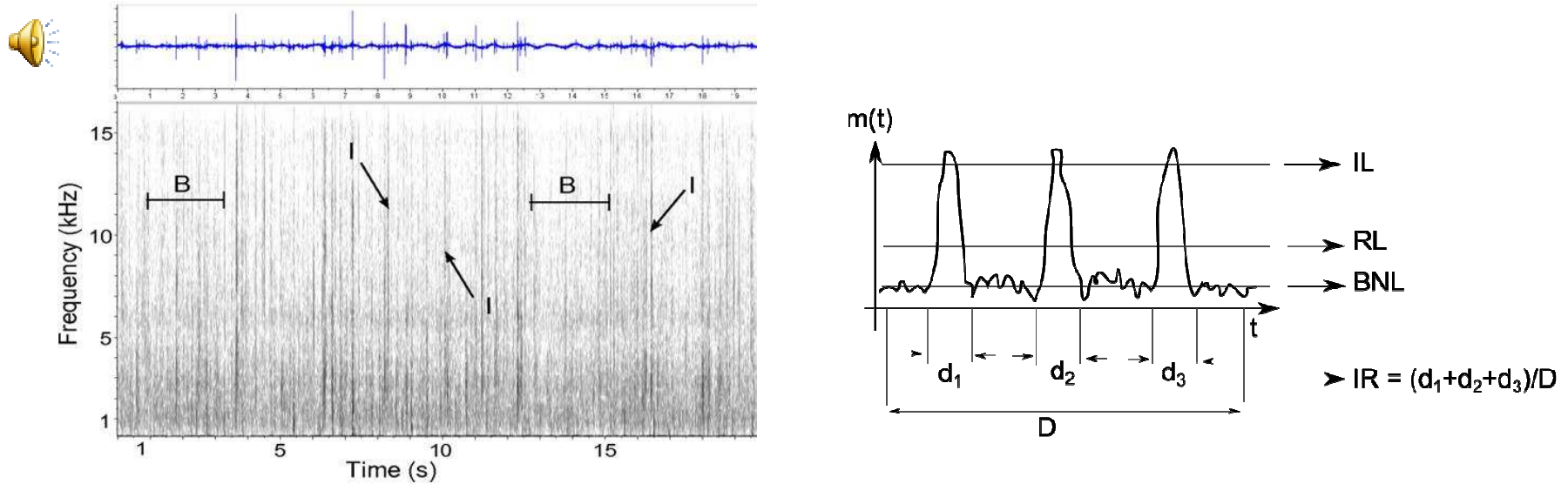
Ambient noise



Individually distinctive sources

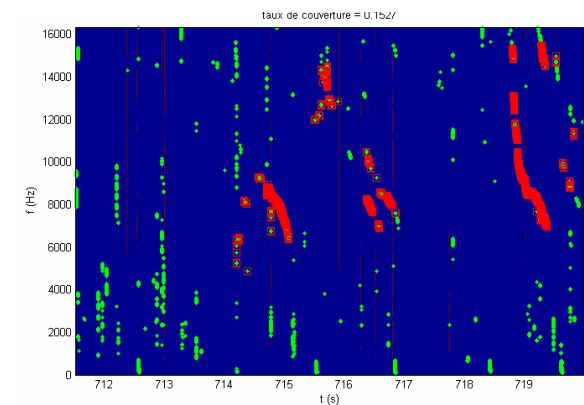
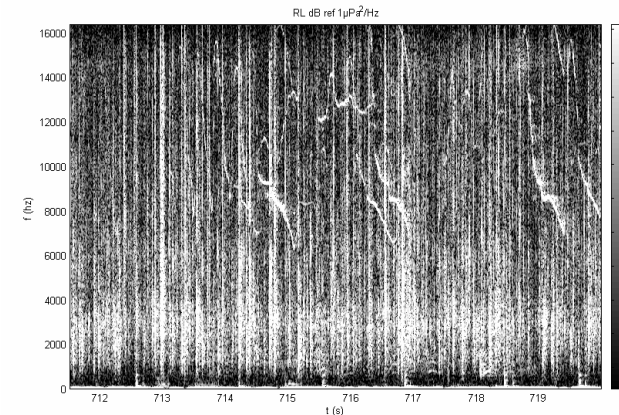
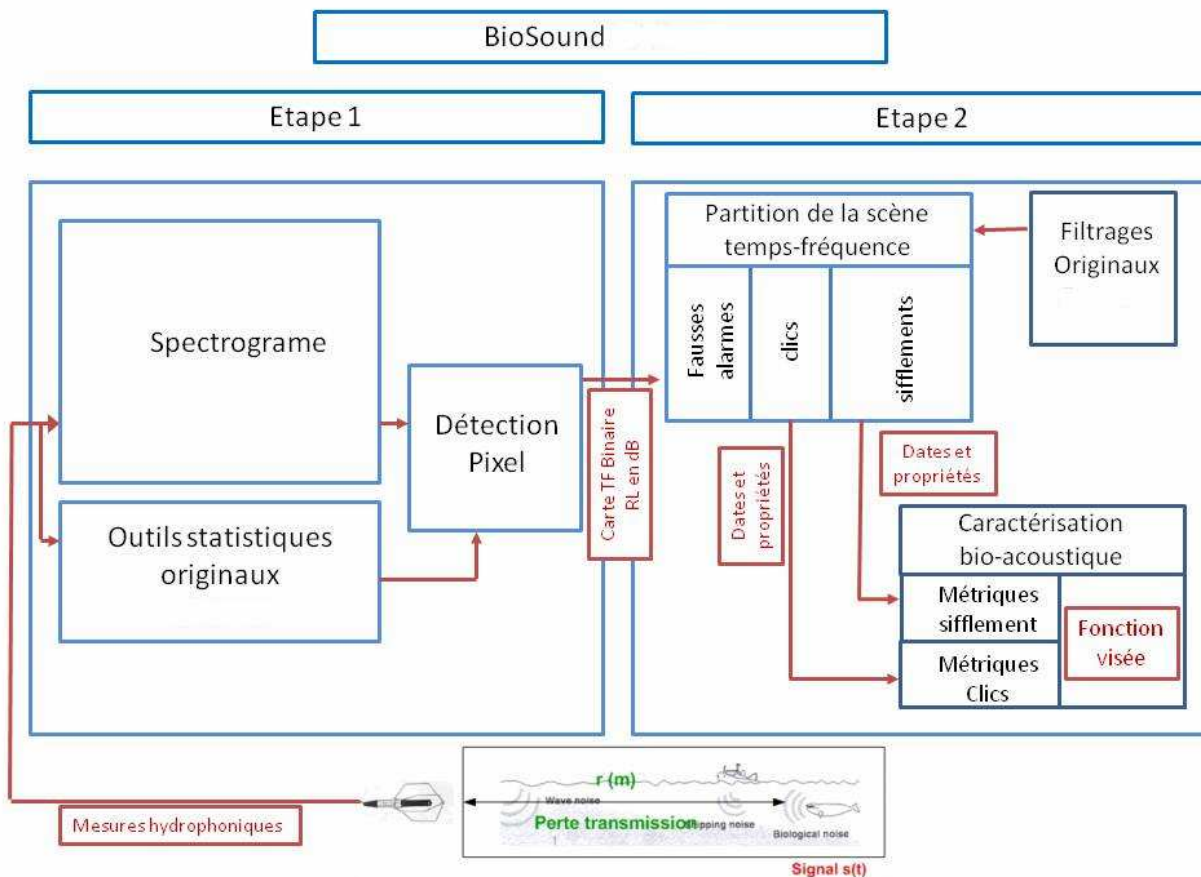
Algorithms – Ambient noise

wideband analysis (RL, BNL, IR, IL)



Algorithms – Frequency modulations

whistle detections (WR)



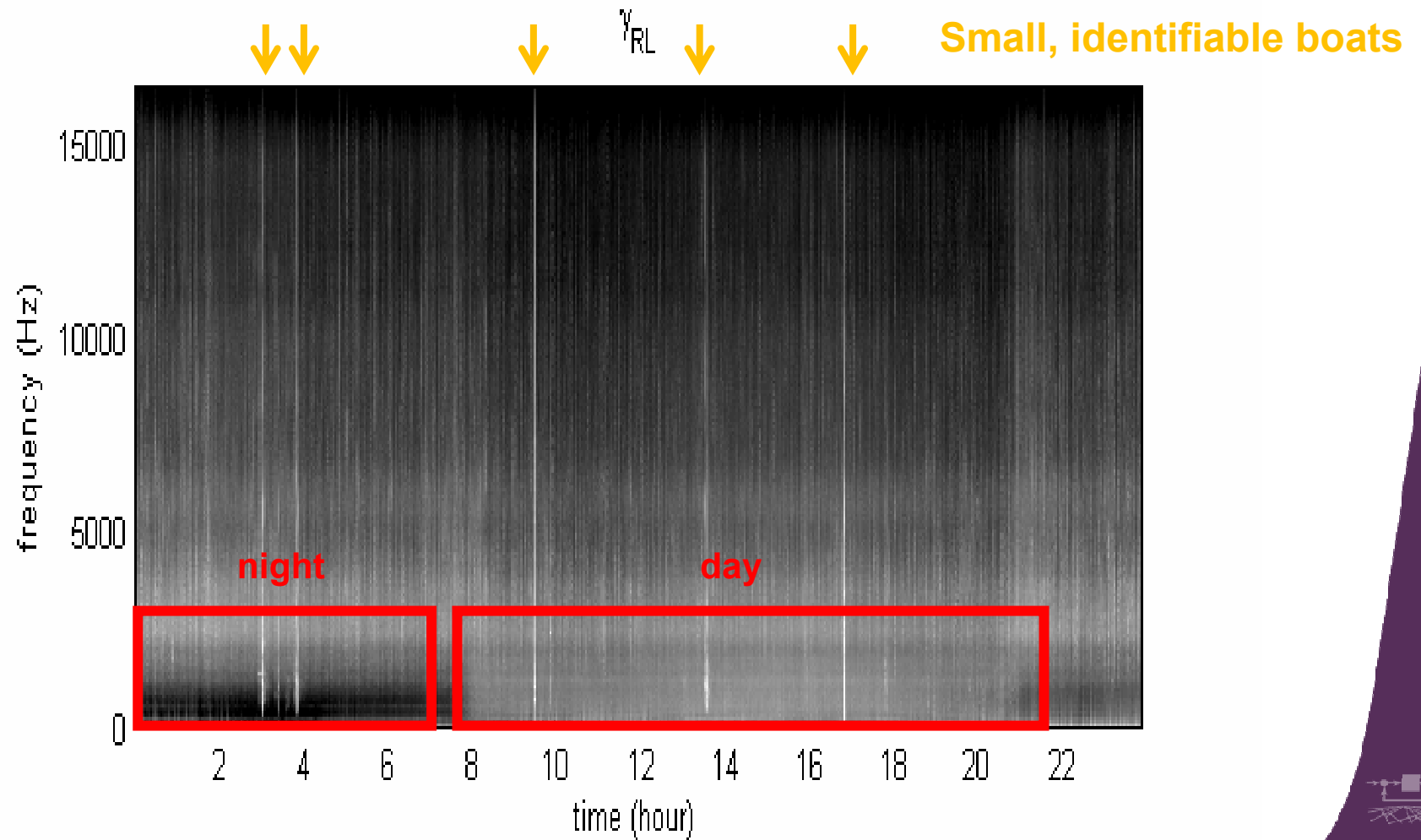
Spectrogram-based detector

Anthropogenic activity in the Parc Naturel Marin d'Iroise



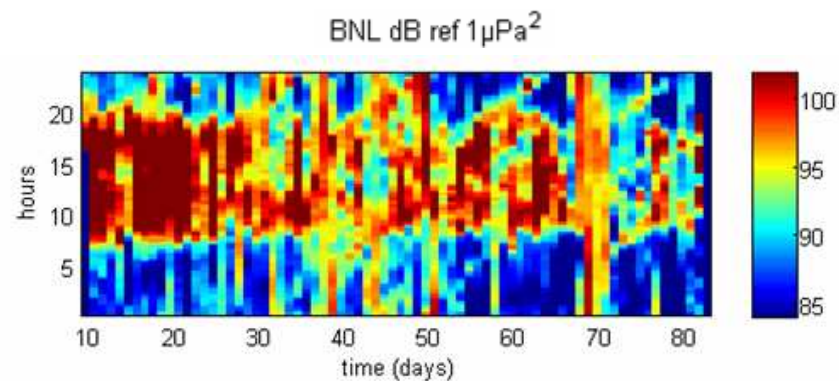
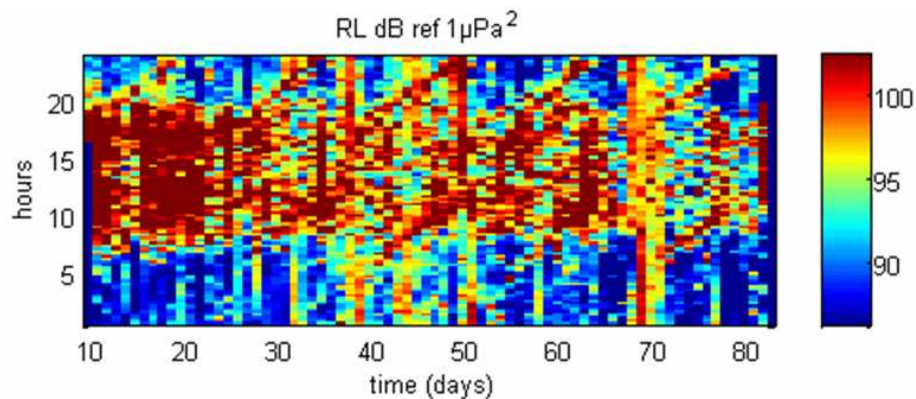
24h spectrogram

data inspection, choice of analysis band

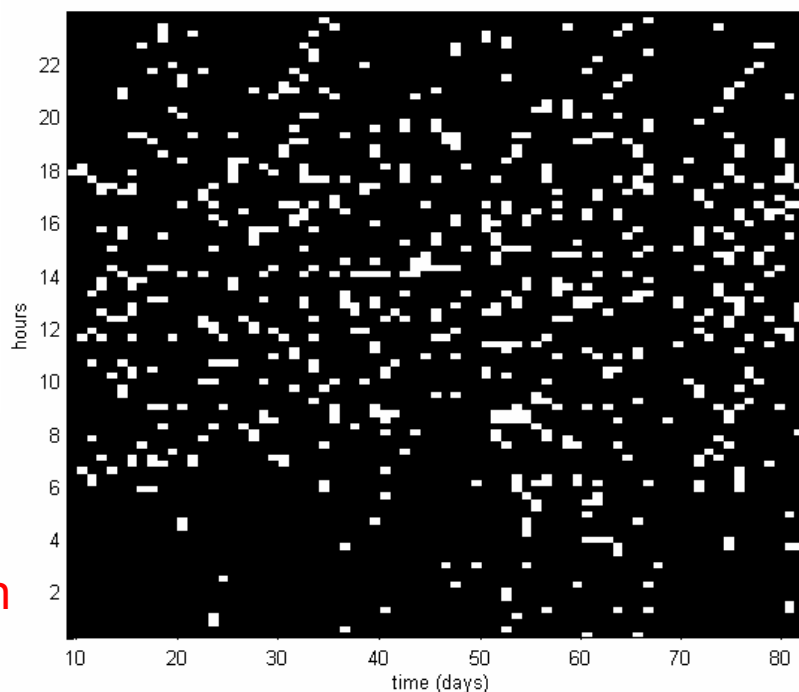
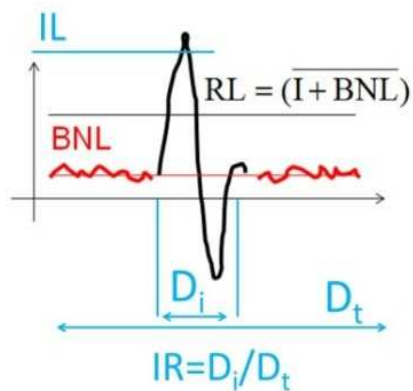


Anthropogenic ambient noise – low frequencies

Small, identifiable boats

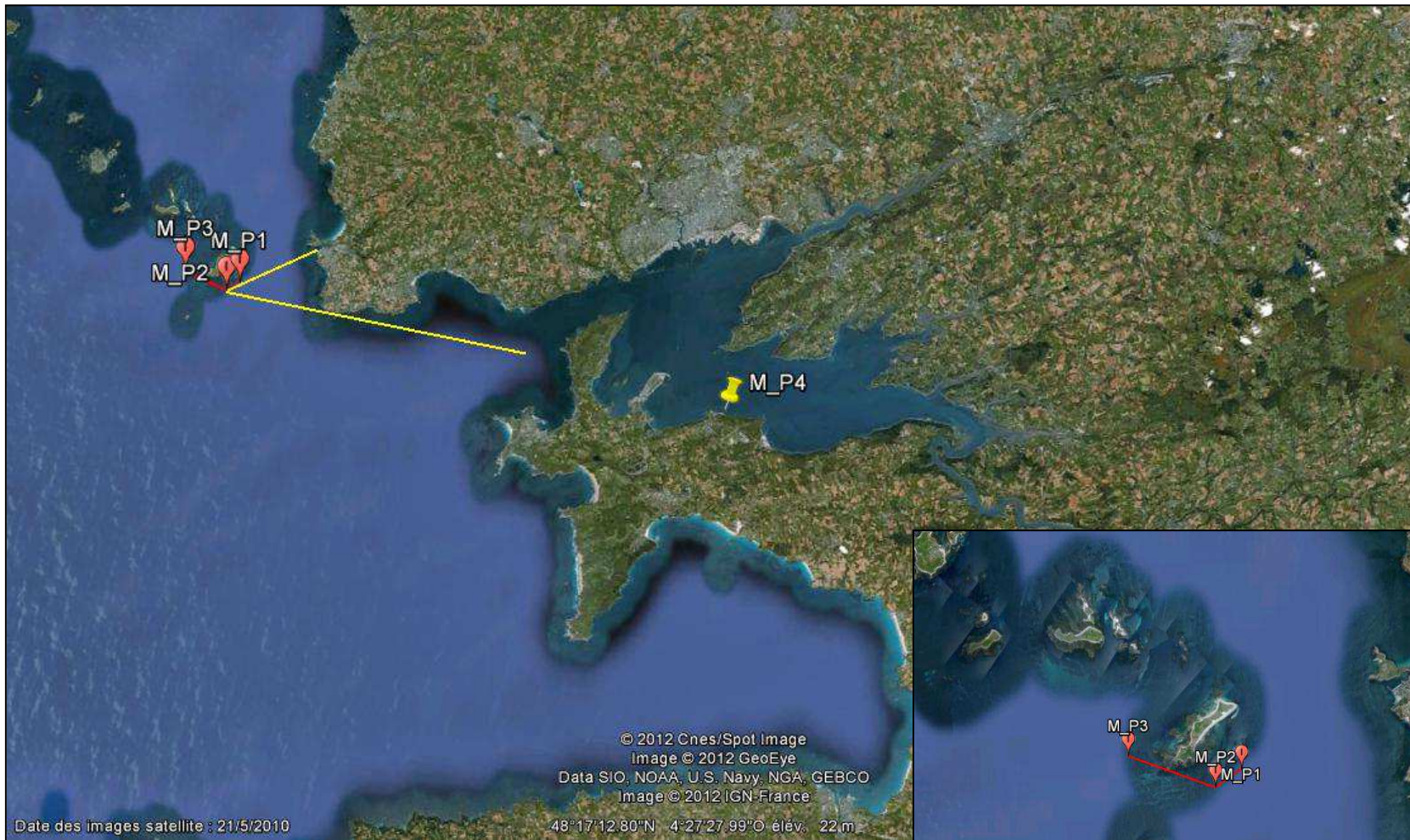


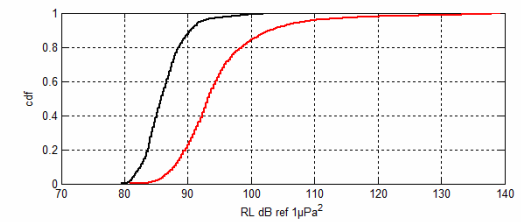
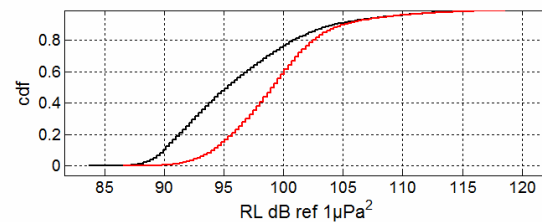
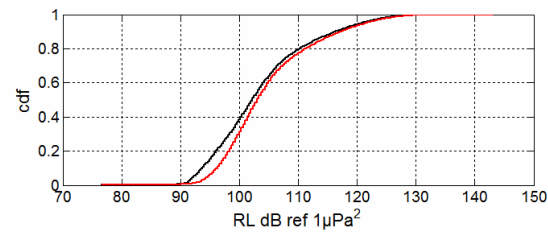
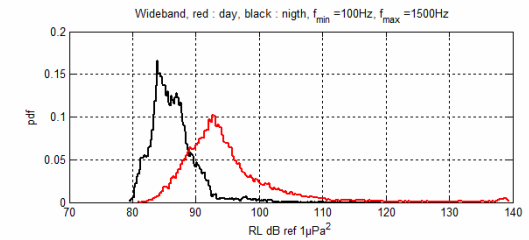
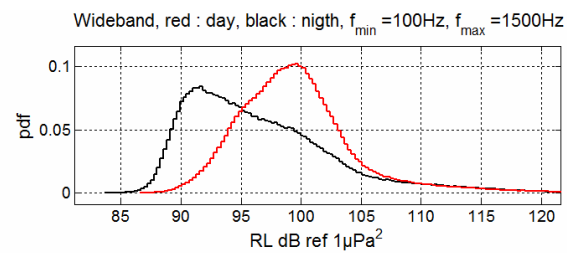
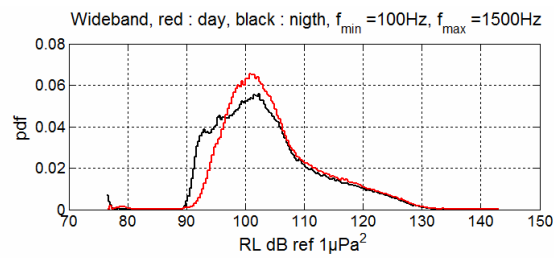
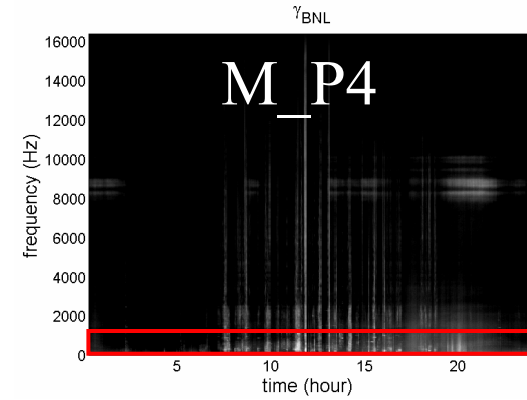
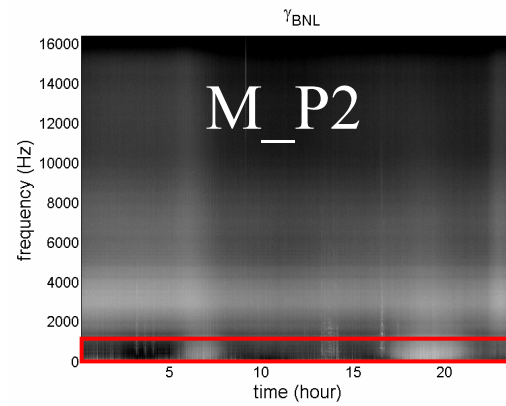
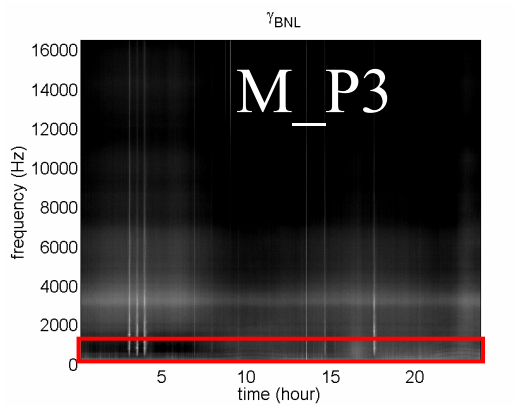
RL-BNL > Seuil => binarization



Energy-based detector
Analysis window size = 10min

Anthropogenic background noise

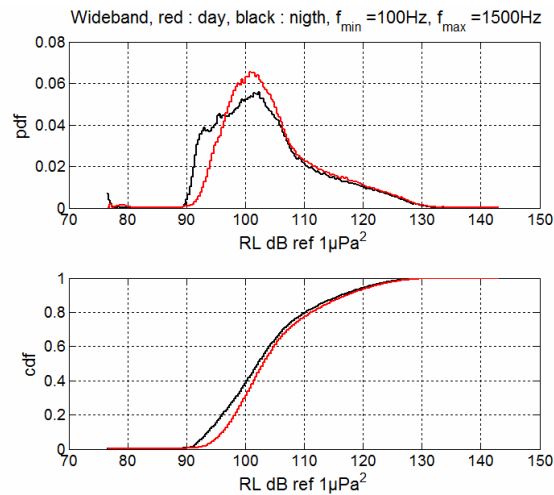






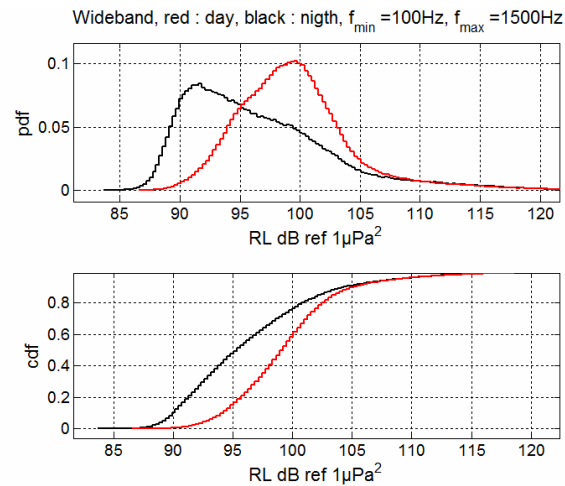
M_P3

Non-affected site:
No, night-day difference



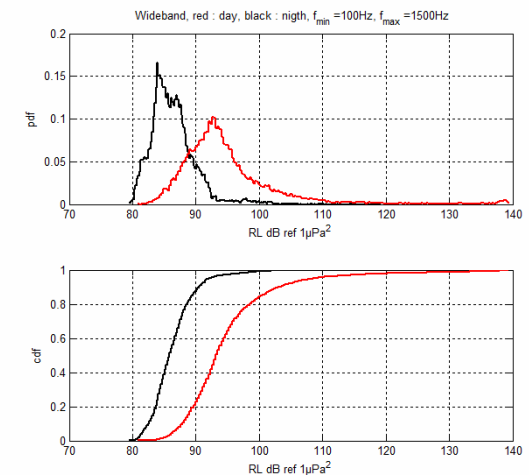
M_P2

Affected site:
8dB between day & night
propagation?!



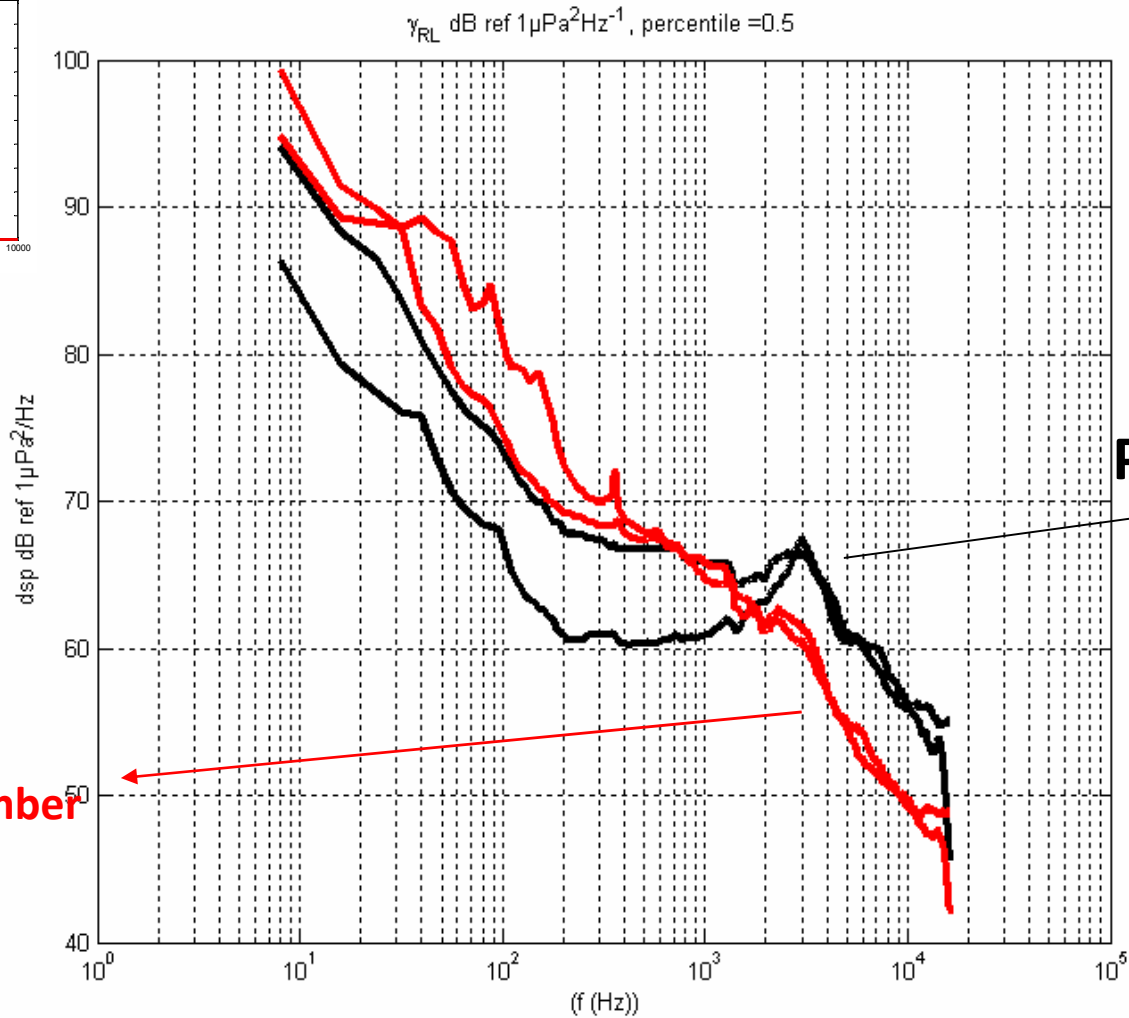
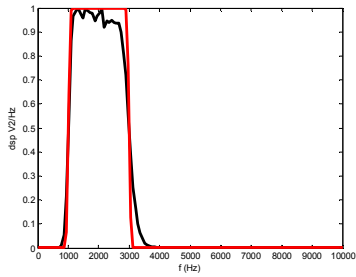
M_P4

Noise source: Rade
de Brest – 8dB
between night & day



Intermezzo...

power apectral density of Molène ambient noise

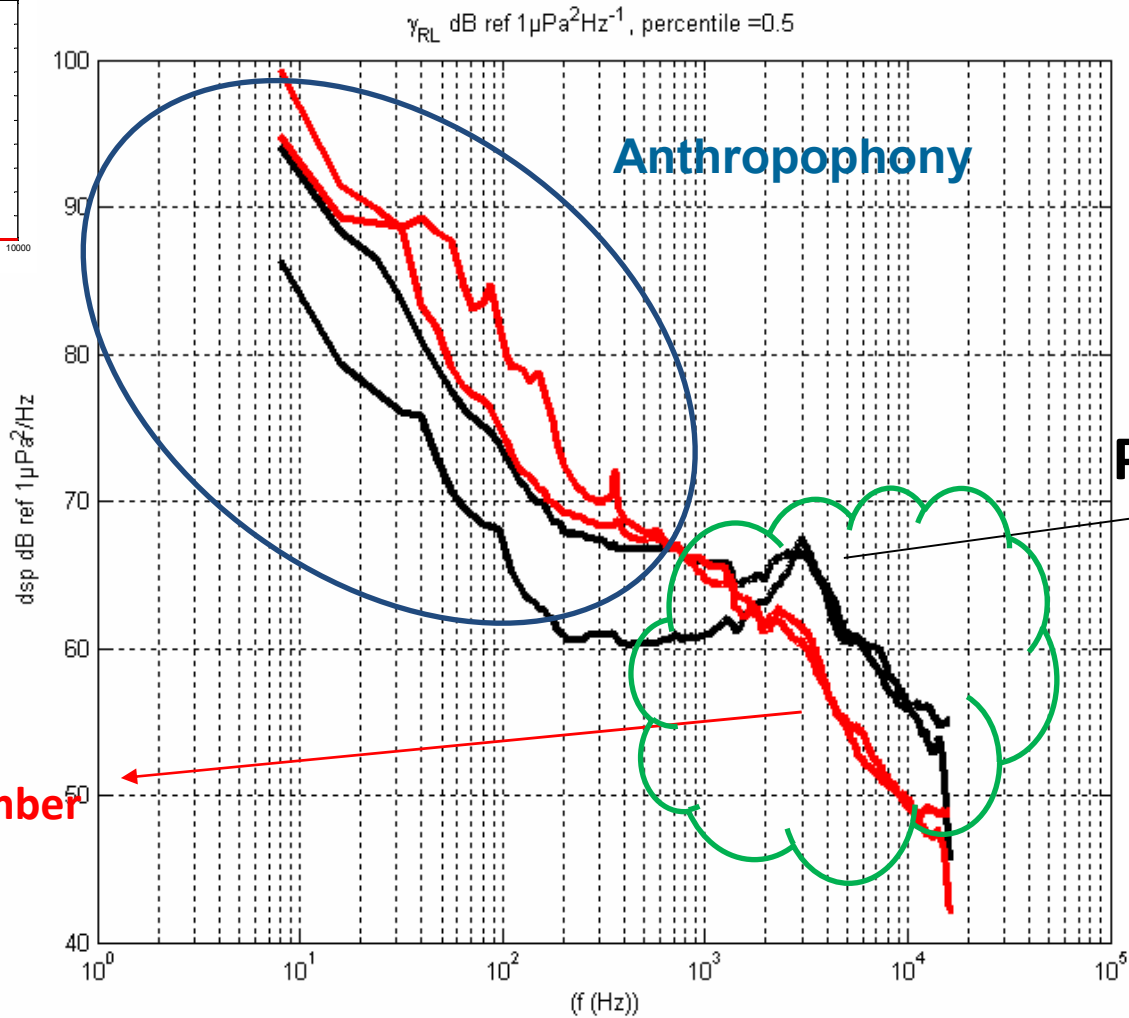
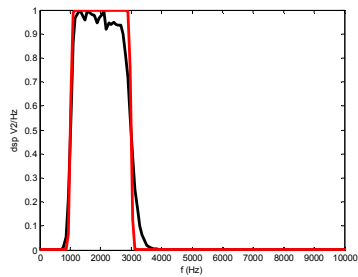


P1, july, september

P2, july, september

Intermezzo...

power apectral density of Molène ambient noise



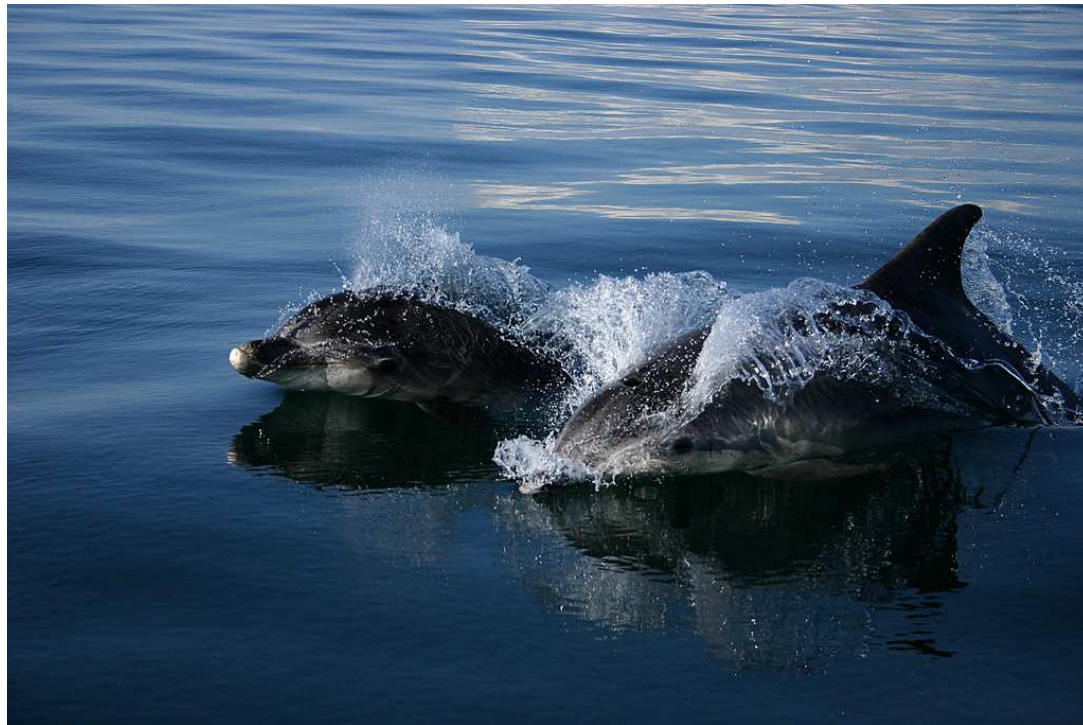
P1, july, september

P2, july, september

Biophony

Habitat use by the bottlenose dolphins (*Tursiops truncatus*) of the PNMI

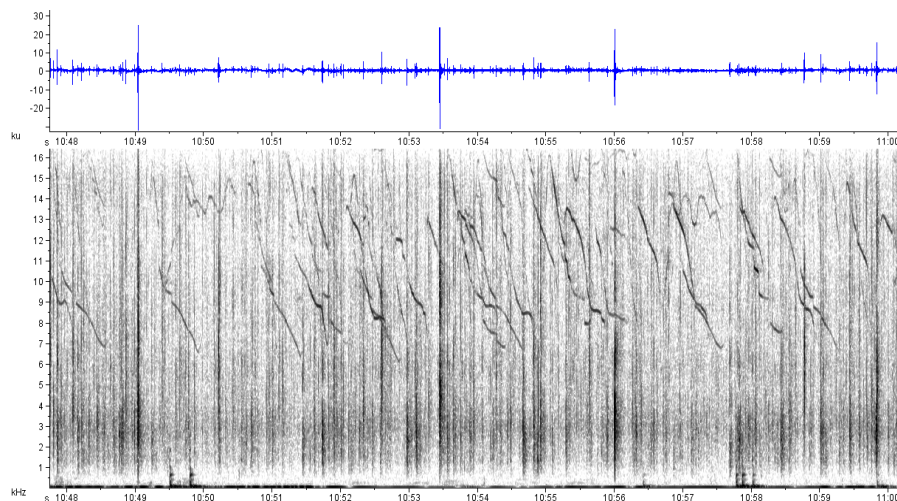




Période: 6/6/2011 – 20/11/2011

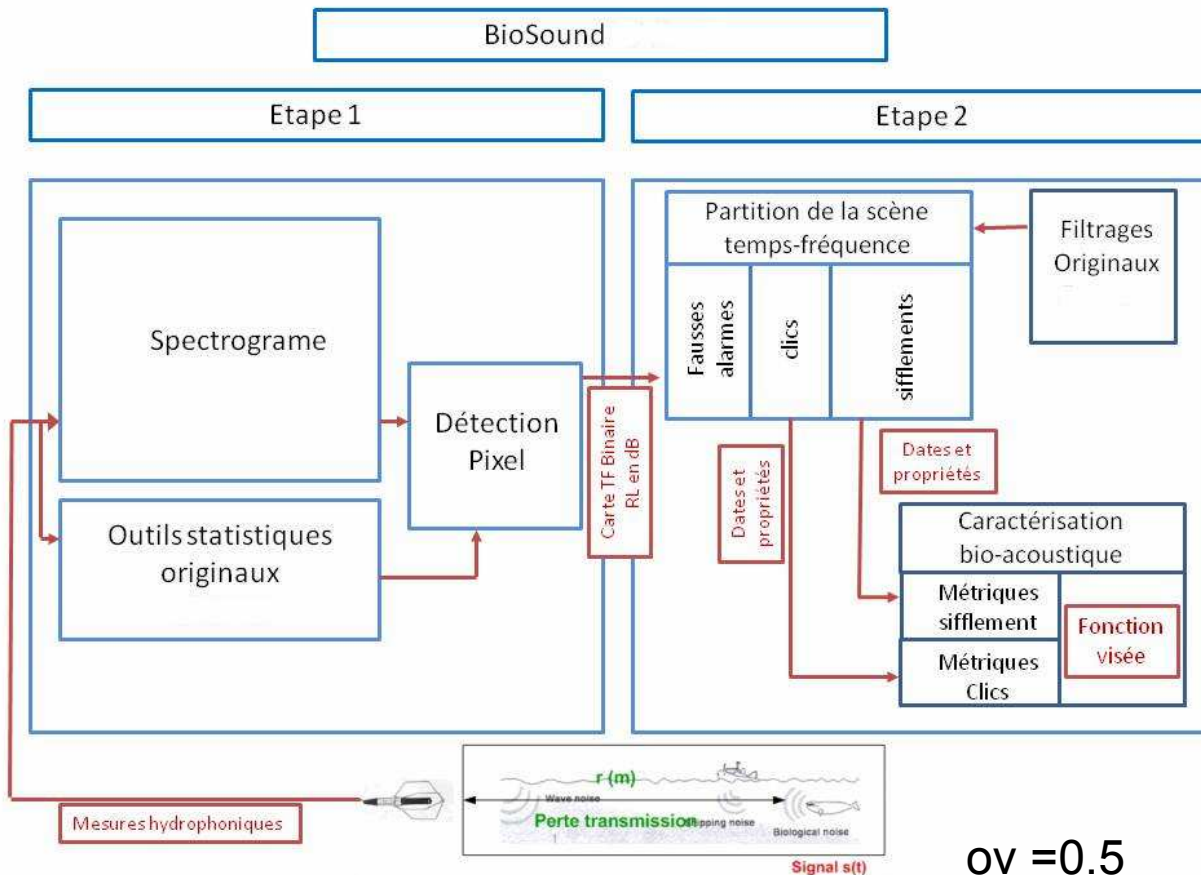


rayon moyen= 350-500m
surface d'écoute = 0.5-1km²



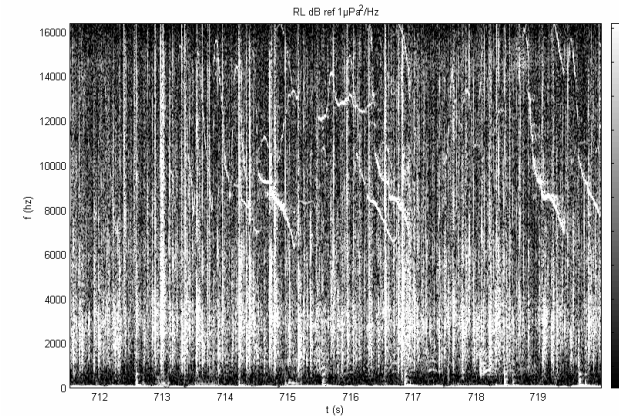
Algorithms – Frequency modulations

whistle detections (WR)

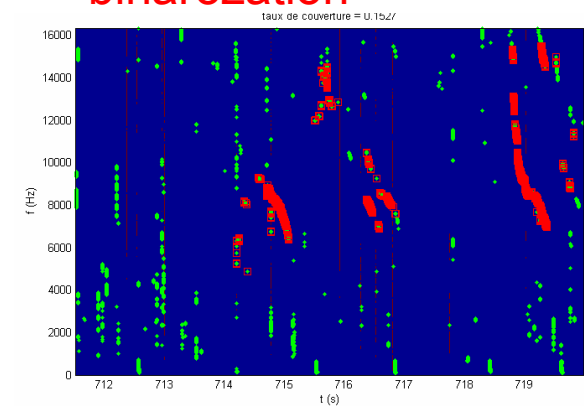


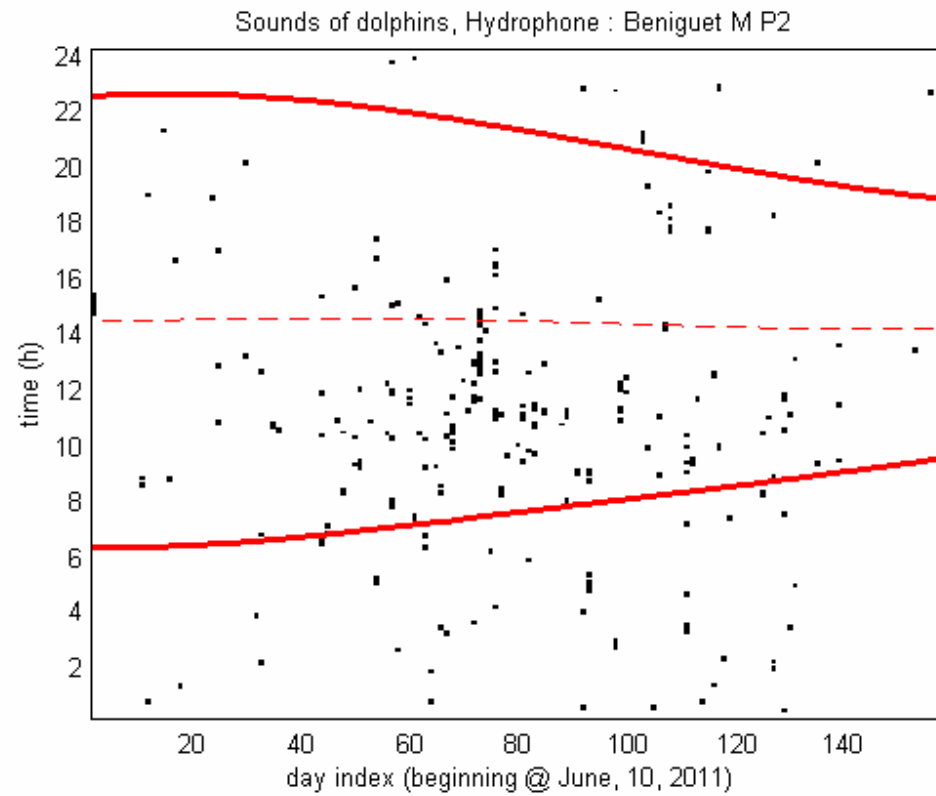
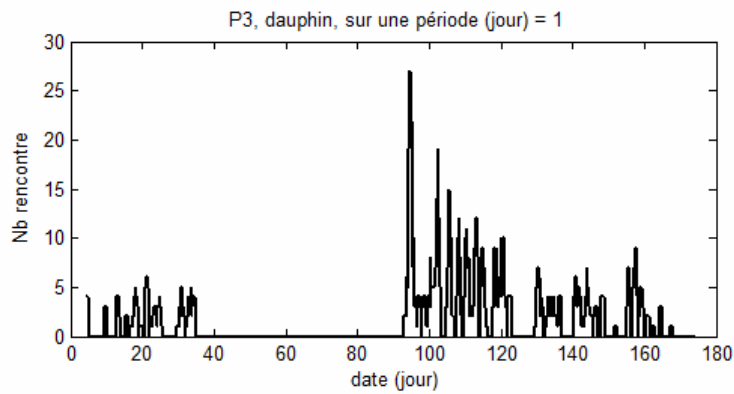
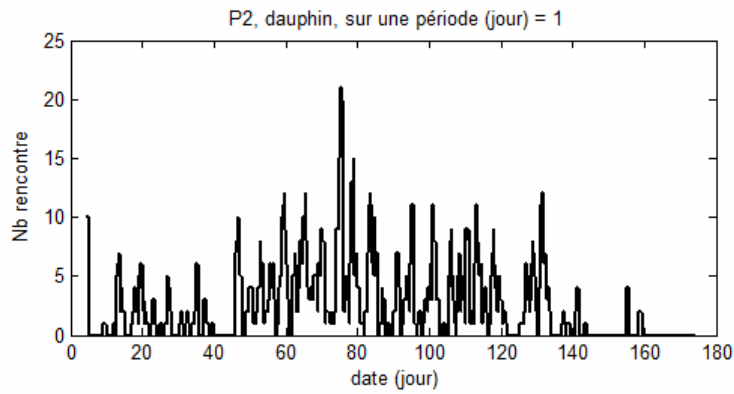
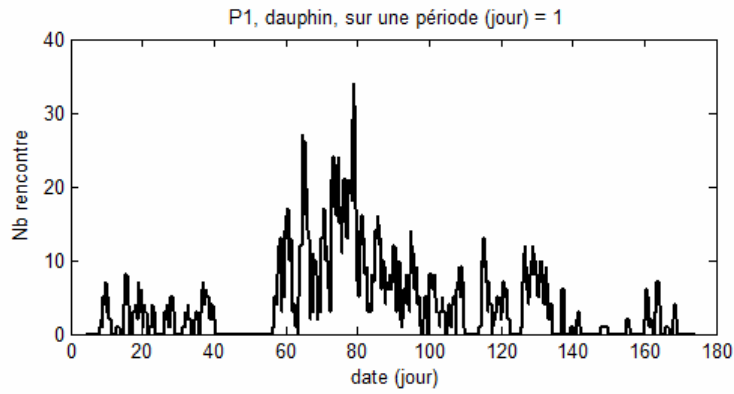
Spectrogram-based detector

$ov = 0.5$
 $L = 1024$
 $w_L = \text{kaiser } 180 \text{ dB}$



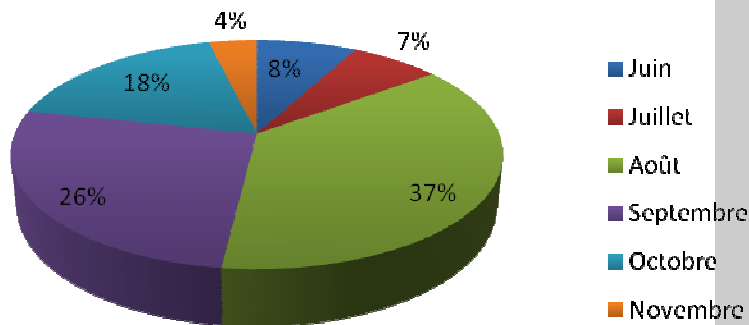
binarization



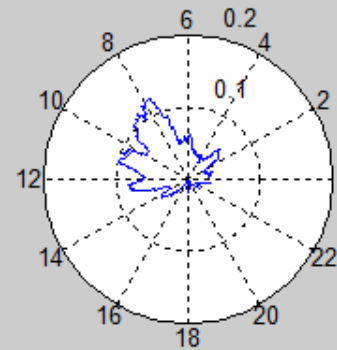


Acoustic presence – time series of whistle detections

6 months

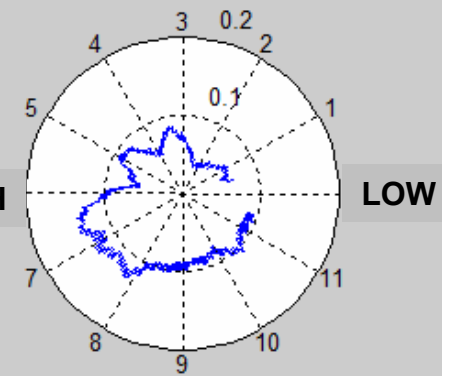


P1, dauphin, proportion de détection, durée = 1h, nombre total de détections = 695



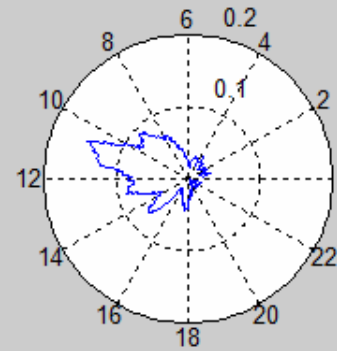
24h

P1 - rythme 12h25

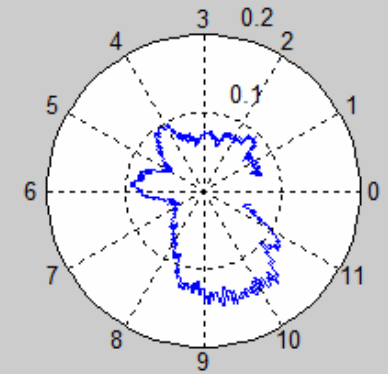


TIDES

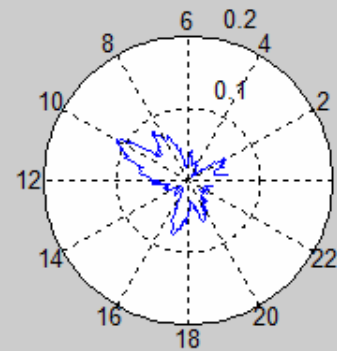
P2, dauphin, proportion de détection, durée = 1h, nombre total de détections = 438



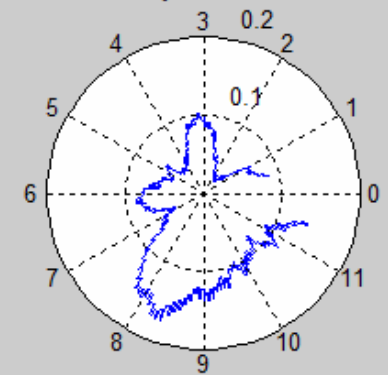
P2 - rythme 12h25



P3, dauphin, proportion de détection, durée = 1h, nombre total de détections = 290

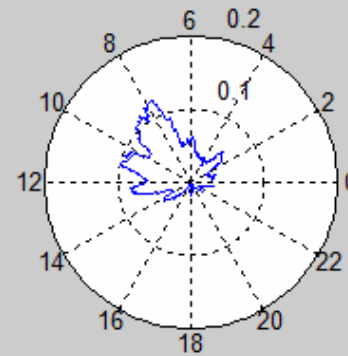


P3 - rythme 12h25

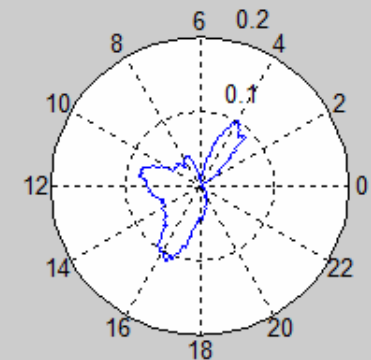


Comparison/com bination of dolphin vs. boat detections (close)

P1, dauphin, proportion de détection, durée
nombre total de détections = 695

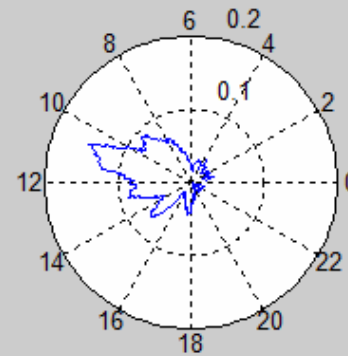


P1, bateau, proportion de détection, durée = 1h,
nombre total de détections = 1217

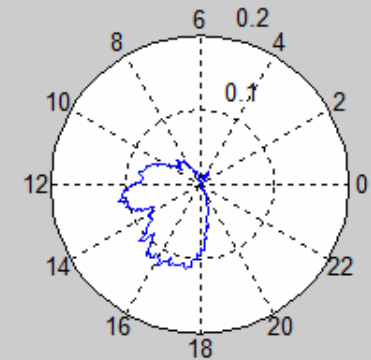


24h

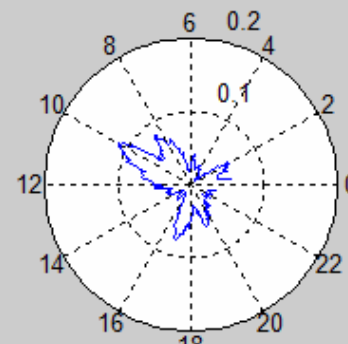
P2, dauphin, proportion de détection, durée
nombre total de détections = 438



P2, bateau, proportion de détection, durée = 1h,
nombre total de détections = 977



P3, dauphin, proportion de détection, durée
nombre total de détections = 290



P3, bateau, proportion de détection, durée = 1h,
nombre total de détections = 200

