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Ageing of Petroleum- and Biobased Polymers, from Nuclear Power Plants to Packaging Materials

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Fibre and Polymer Technology,
Stockholm, Sweden

Department of Fibre and Polymer Technology “Soft matter research”

Ca. 130 people

A major part: PhD students



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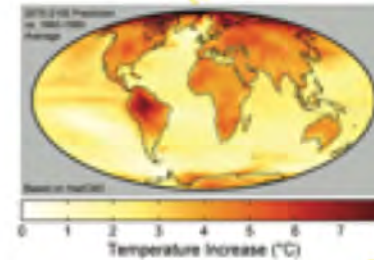




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Energy hunger

Global warming



Food



Water



Source limitations

Polymeric Materials



Health





Long-term properties

Life-time prediction, Accelerated ageing

oxidation, hydrolysis, depolymerization, DLO, migration, swelling, physical ageing, vitrification

- Plastic pipes/tubes (gas, oil, fuel, water)
 - Cables and seals (air, water) - Nuclear power plants
 - Quick connectors (fuel)
 - Polymer films
 - Cables – electric transmission
-

Nuclear Power Plants

47 % EPDM
39 % carbon black
5 % CaCO_3
6-7 % paraffine oil
1 % S
.....

30 % EPDM
6 % CaCO_3
35 % $\text{Al}(\text{OH})_3$
6-7 % stearine/waxes
2 % S
.....

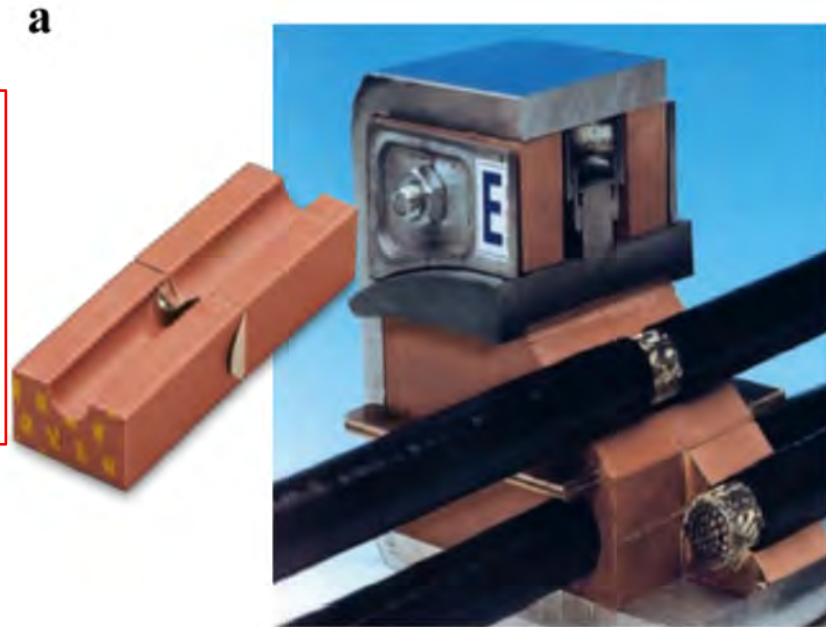
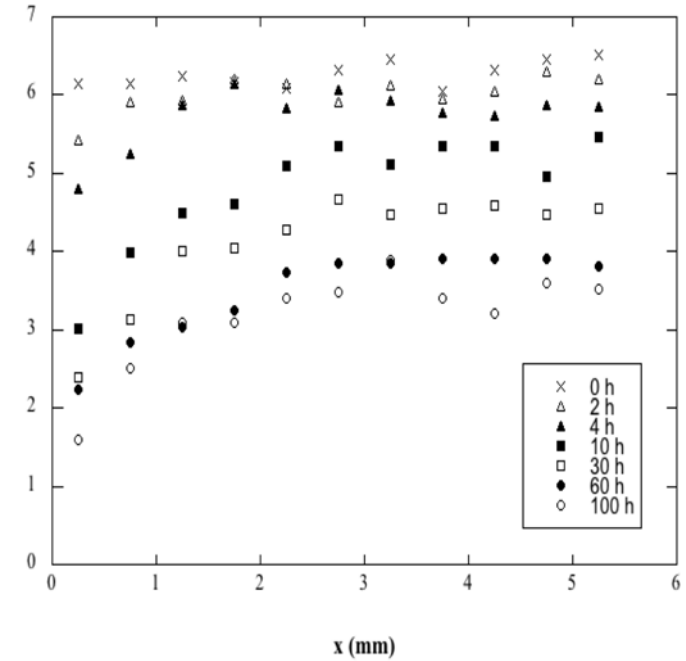
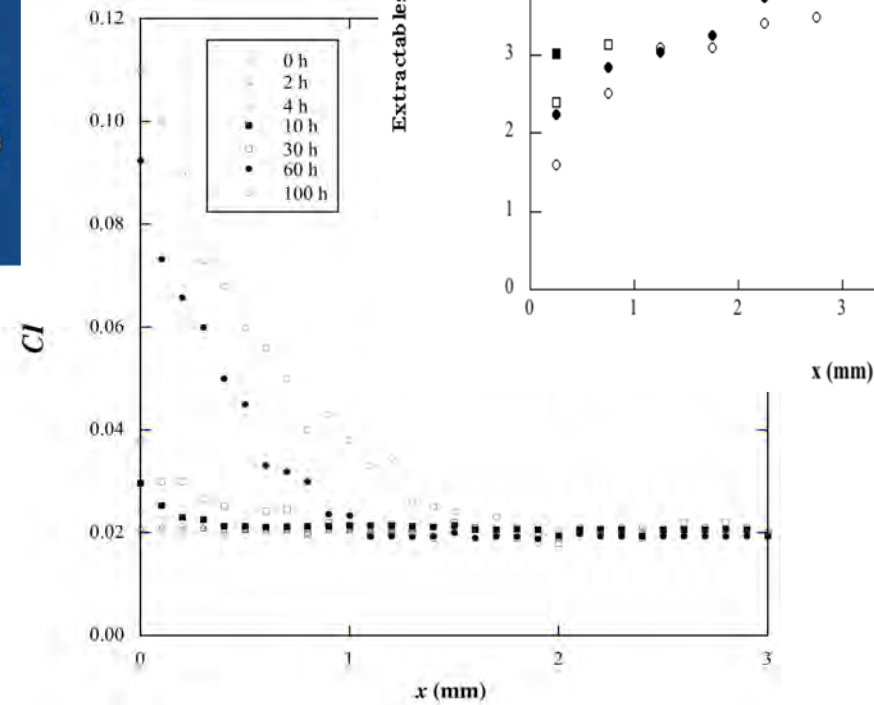
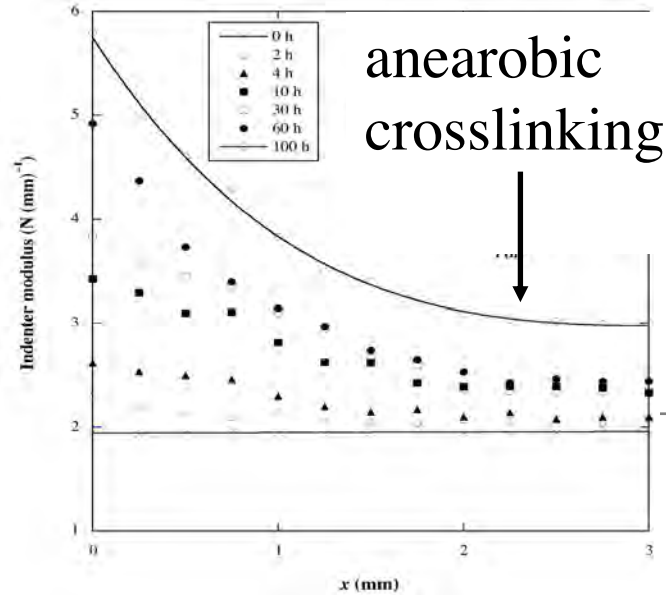
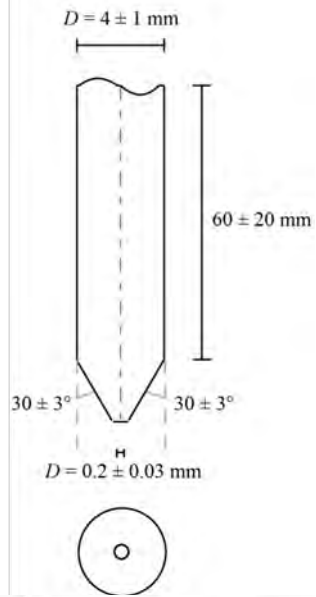


Fig. 1 a) A cross-section of a cable transit system. Lycron seal blocks (pink) can be seen packed in the frame structure. b) Carbon black-containing EPDM seal installed in a transportation valve (knife-port valve).

Profiling of thermally aged EPDM seals using portable NMR, indenter measurements and IR spectroscopy facilitating separation of different deterioration mechanisms

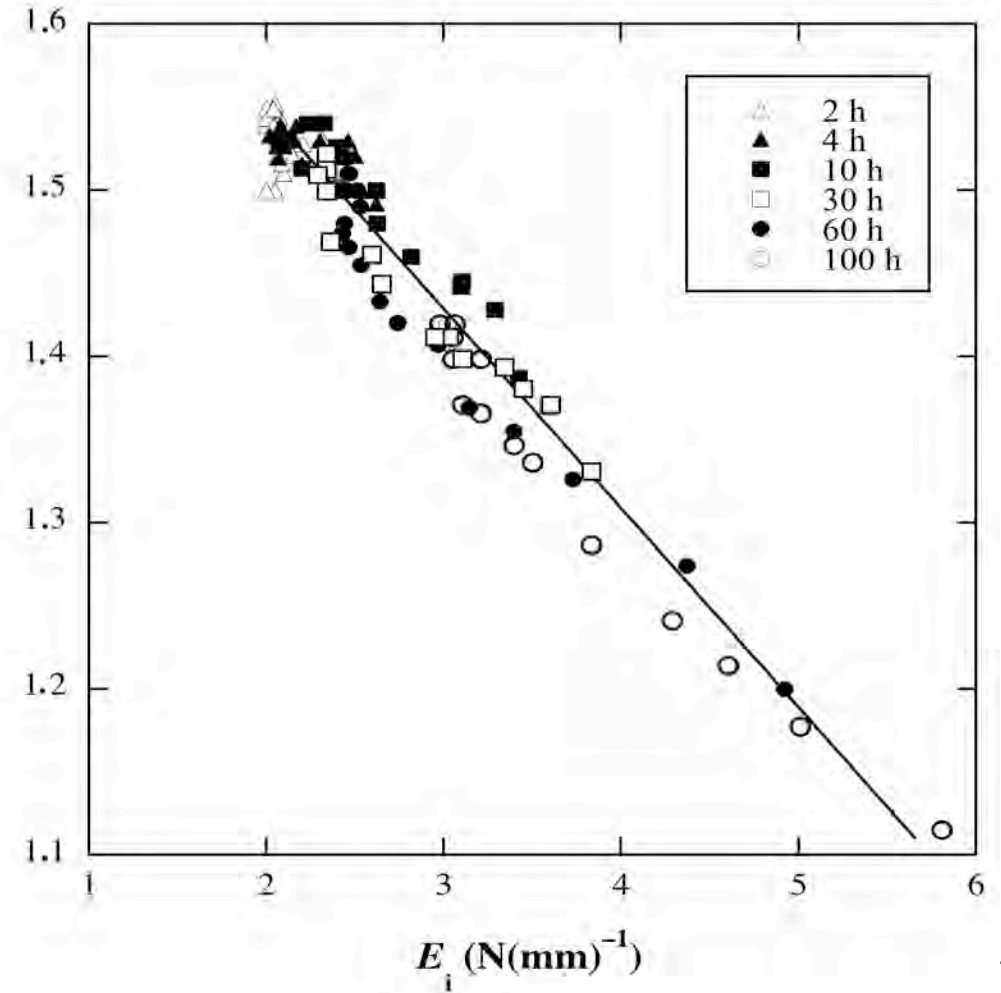
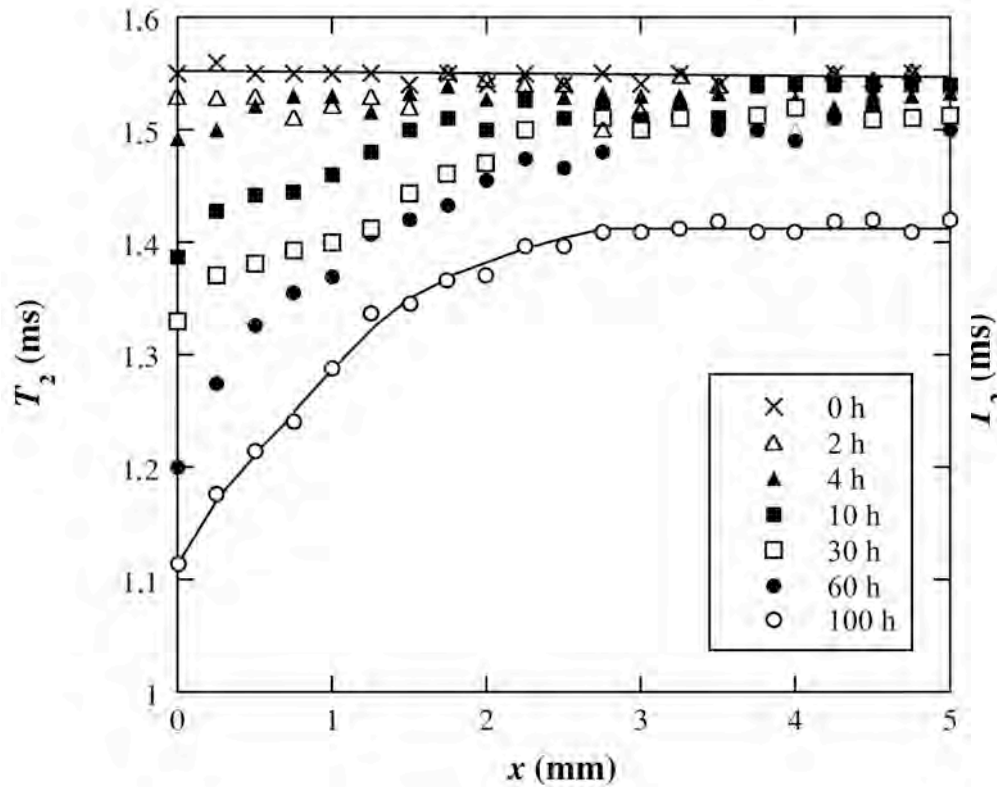
Oxidation, anearobic crosslinking and loss of oil extender (170 C)





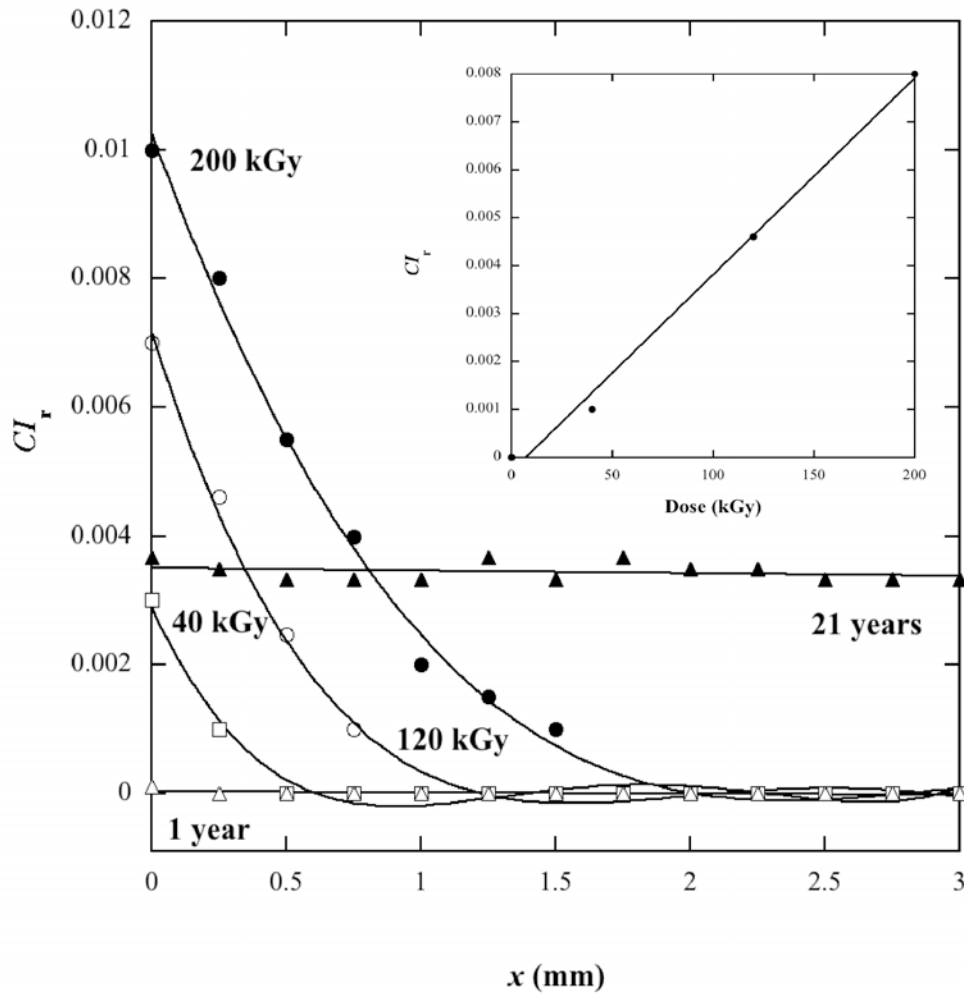
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NMR mouse=Non-invasive No specimen preparation



Radiochemical ageing of highly filled EPDM seals as revealed by accelerated ageing and ageing in-service for 21 years

DLO effects and accelerated ageing
Gamma radiation

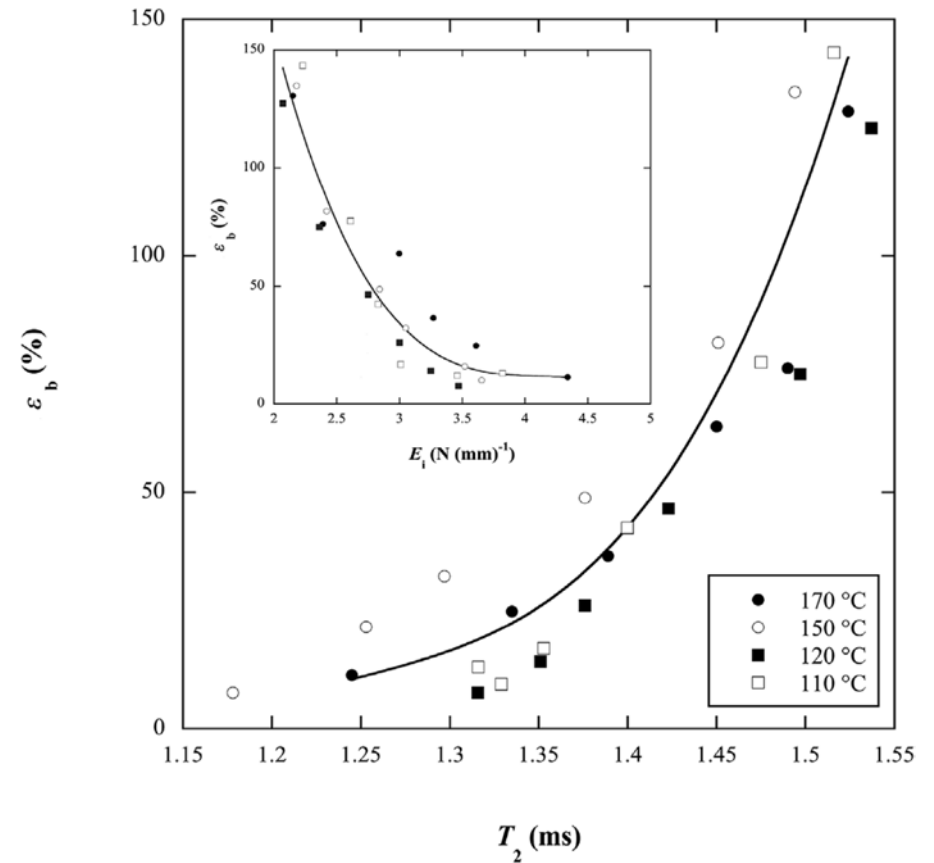
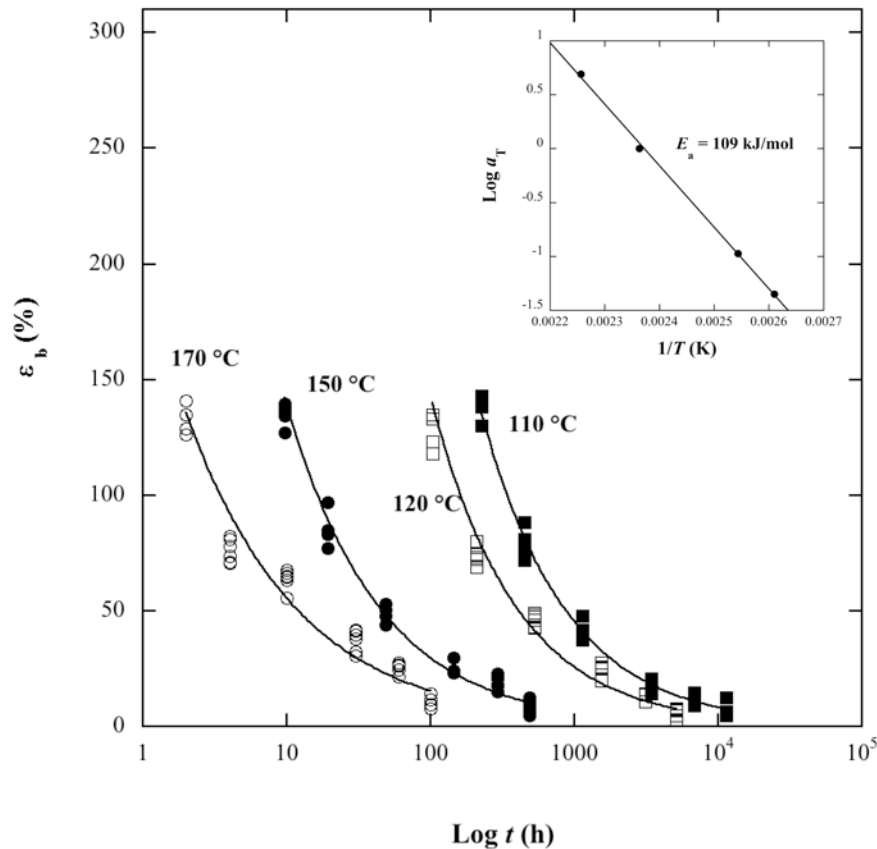


23 C, $p_{O_2}=1$ kPa using ^{60}Co
gamma-ray source that yielded a
dose rate of 0.31 kGy/h



Service conditions
23 C, $p_{O_2}=1$ kPa
0.15 kGy/year.

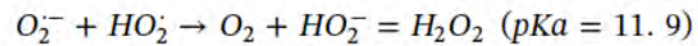
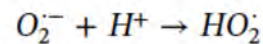
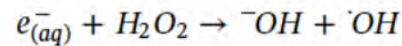
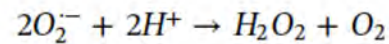
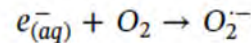
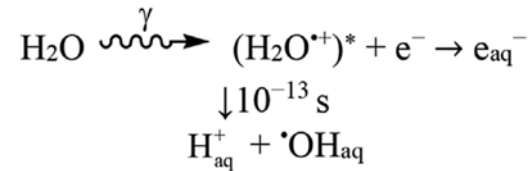
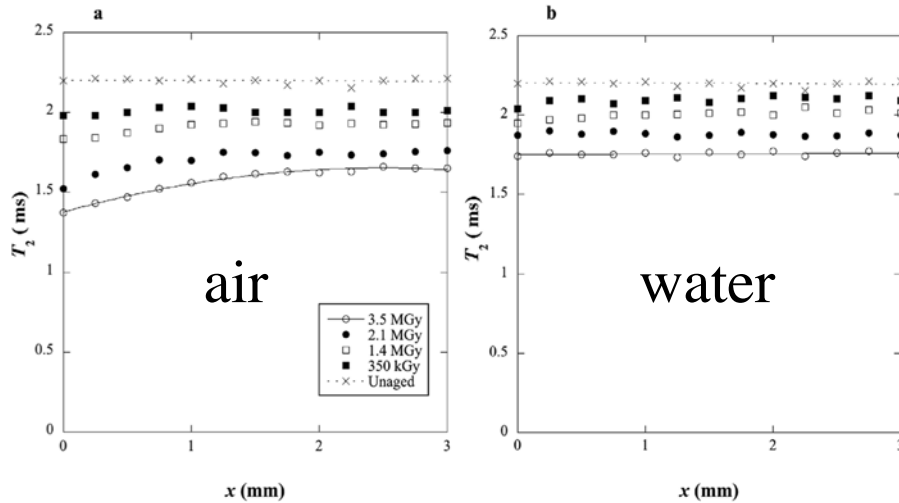
Deterioration of highly filled EPDM rubber by thermal ageing in air: kinetics and non-destructive monitoring



$\epsilon_b = 50$ %, 3000 years at 23 C

Effect of gamma radiation on carbon-black-filled EPDM seals in water and air

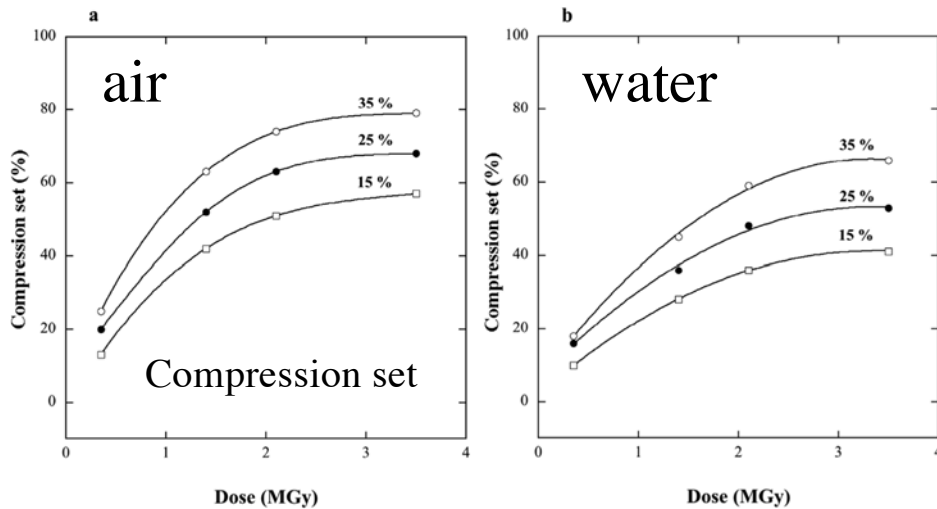
oxidative crosslinking
(but also anaerobic crosslinking)



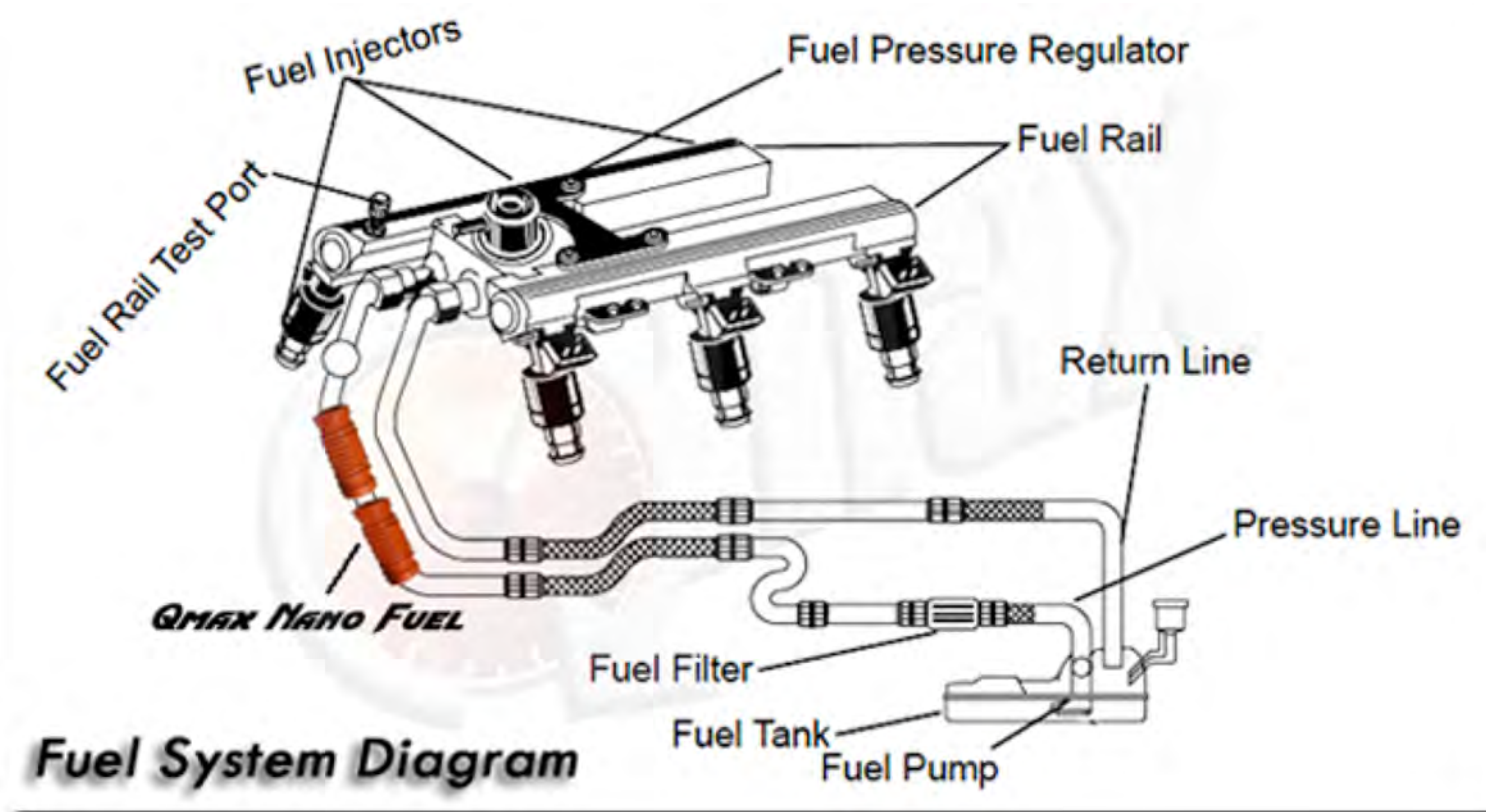
oxygen dissolved in water is consumed during irradiation, less oxygen available for oxidation



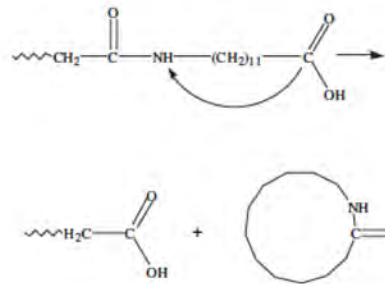
short exposure (40 h) to 350 kGy once per year



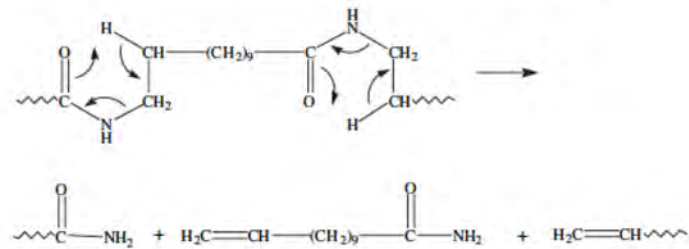
Automotives



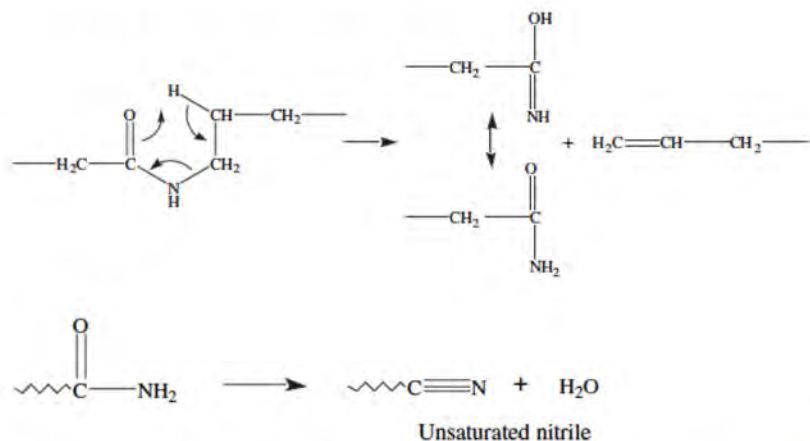
1.1 Intramolecular exchange



1.2 Cis-elimination with alkylamide bond splitting



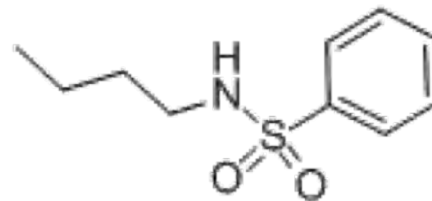
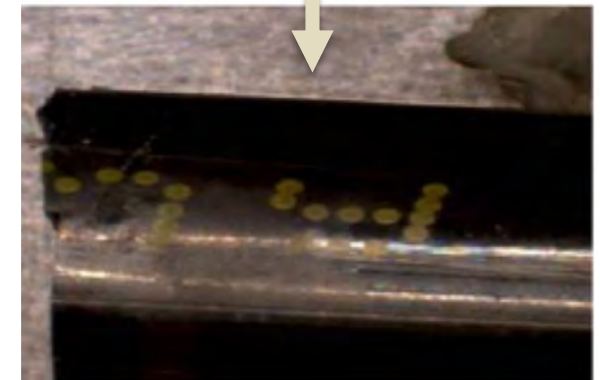
1.3 Cis-elimination and dehydration



Polyamide-12

Petrol/ethanol

Molar mass reduction
Plasticiser loss



Molar mass data of inner surface regions of pipes aged at 110 °C

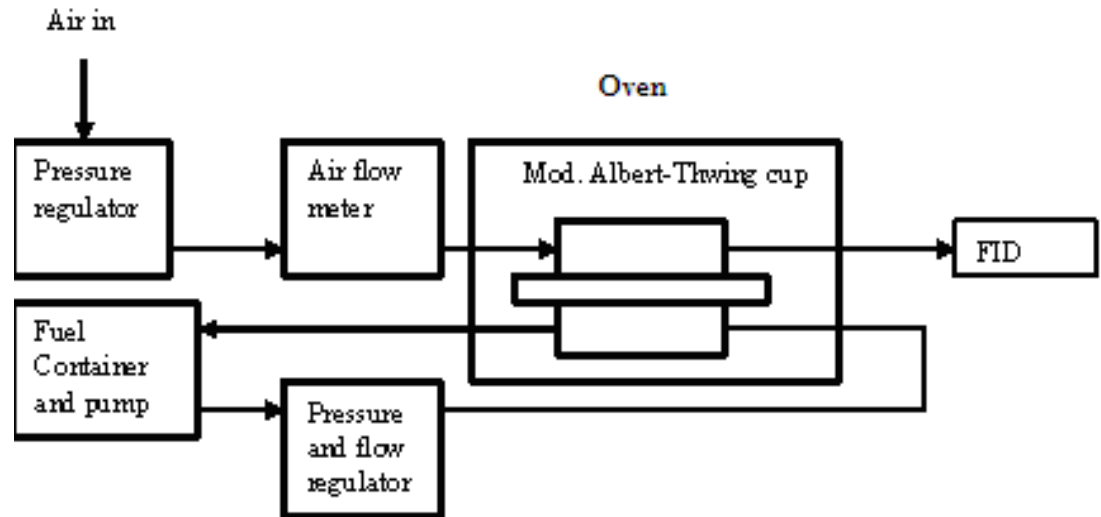
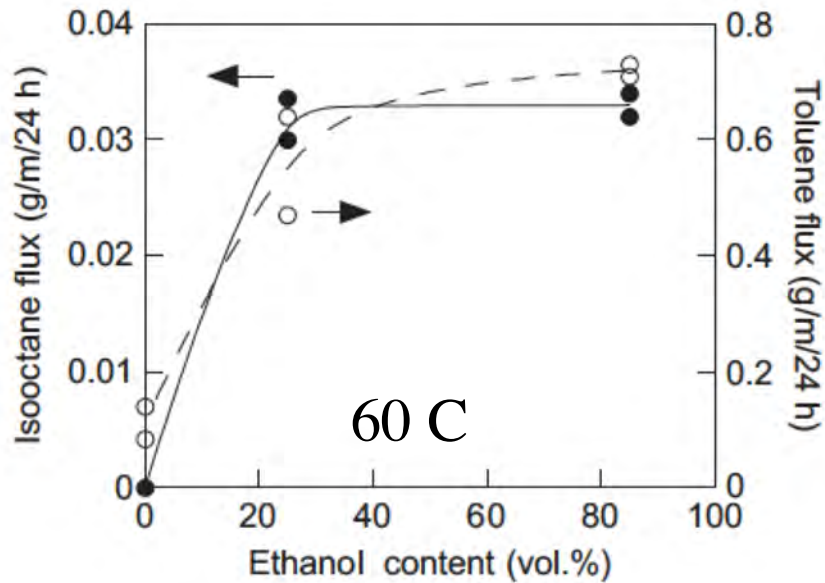
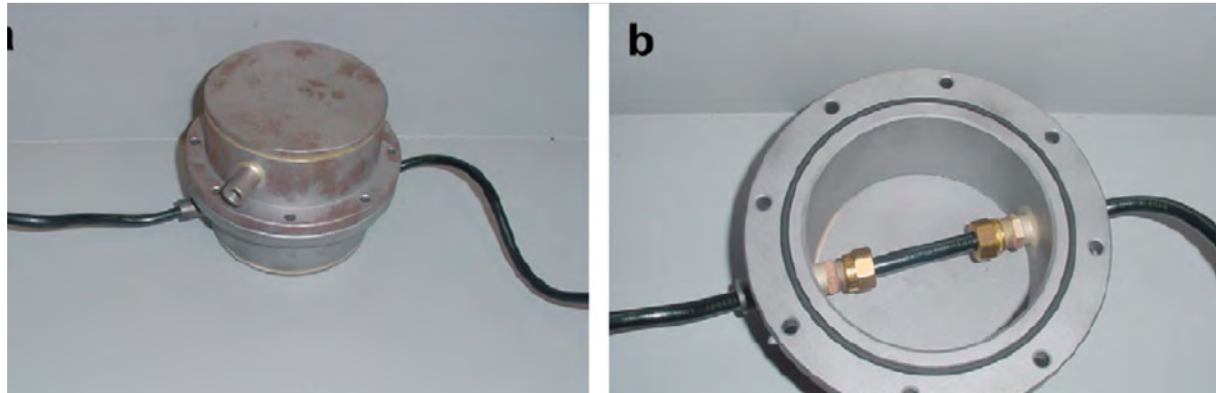
Fuel	Ageing time (h)	\bar{M}_w (kg/mol)	\bar{M}_w/\bar{M}_n
Unaged	0	144	2
E0	1200	65	1.8
E0	1800	72	3.3
E0	2400	62	2.5
E10	1200	39	3.5
E10	2400	72	2.2
E30	1200	76	2
E30	1800	61	2.1
E30	2400	45	2.9

Scheme 1. The three mechanisms of thermal degradation in inert and oxidative environments of PA12 [9–12].

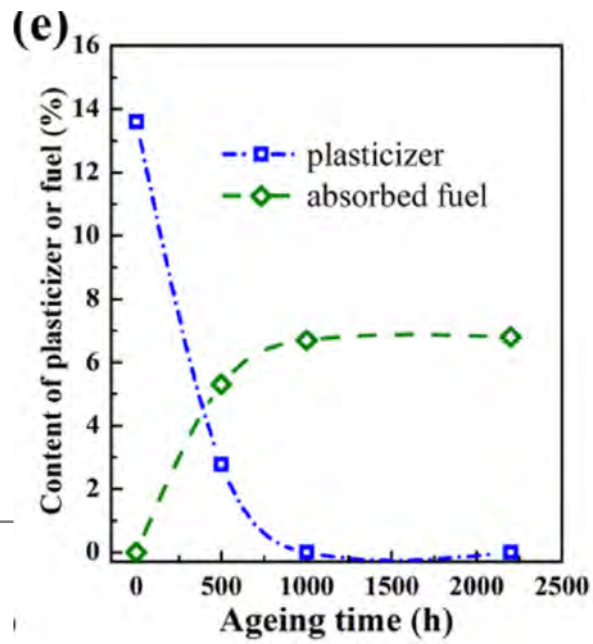
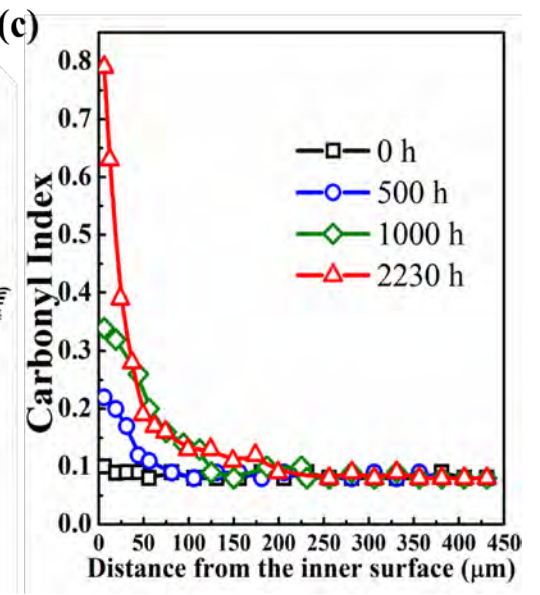
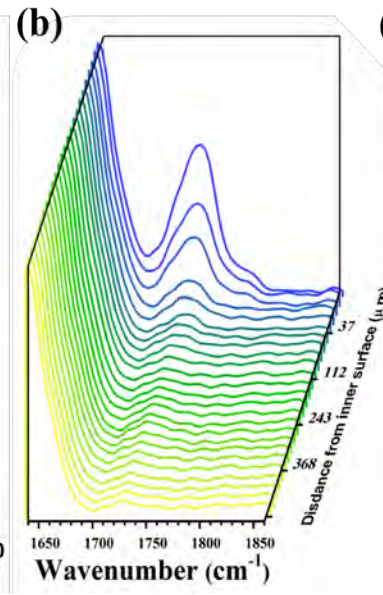
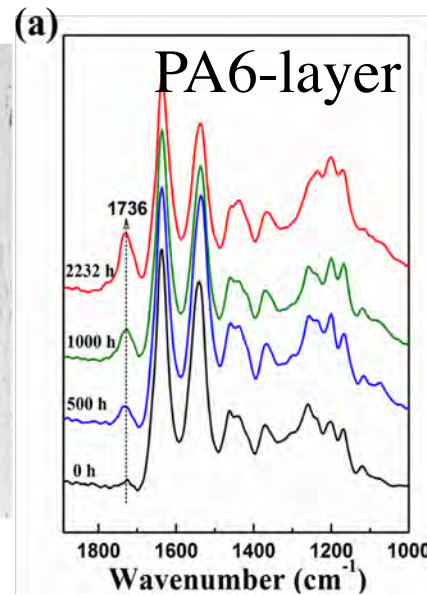
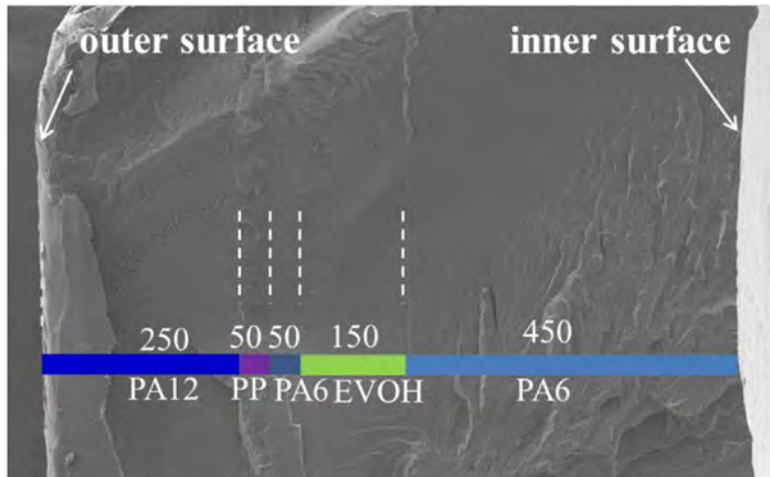
K. Kallio and M. S. Hedenqvist, *Polym. Degr. Stab.* **93** (2008) 1846-1854.

Fuel permeation through pipes

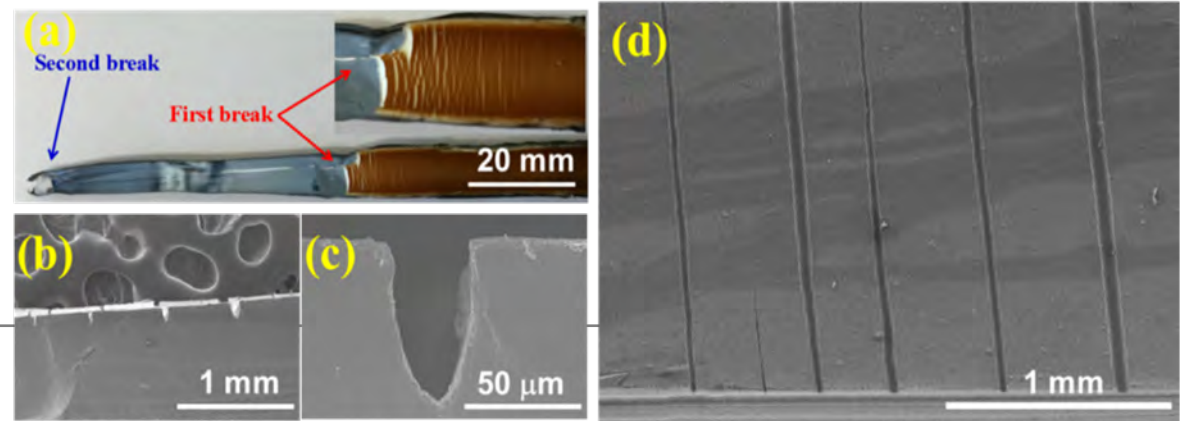
Fuel C
50 vol% Isooctane
50 vol% Toluene



Long-term performance of polyamide-based multilayer (bio)diesel fuel lines aged under “in-vehicle” conditions

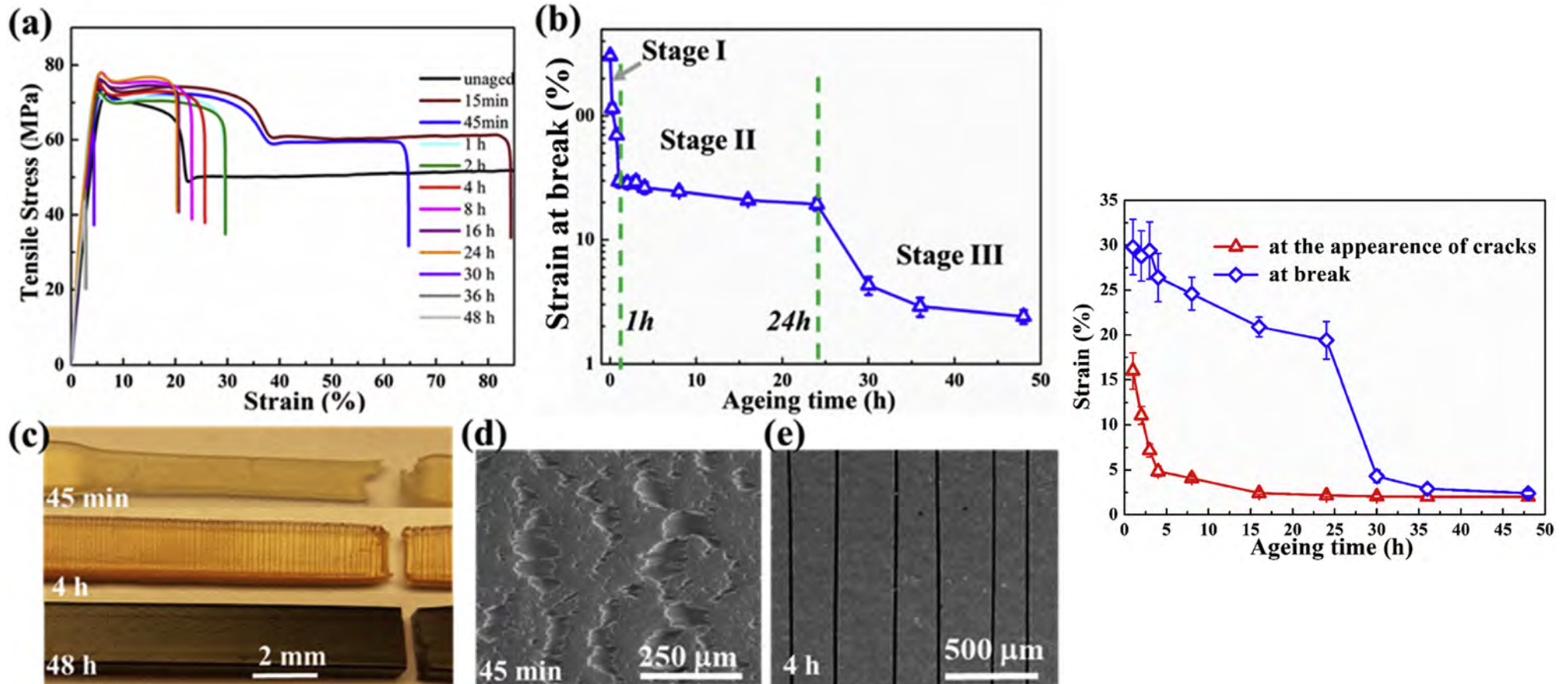


Alternatively petroleum-diesel (B0) and B0 with 20 % biodiesel (B20)

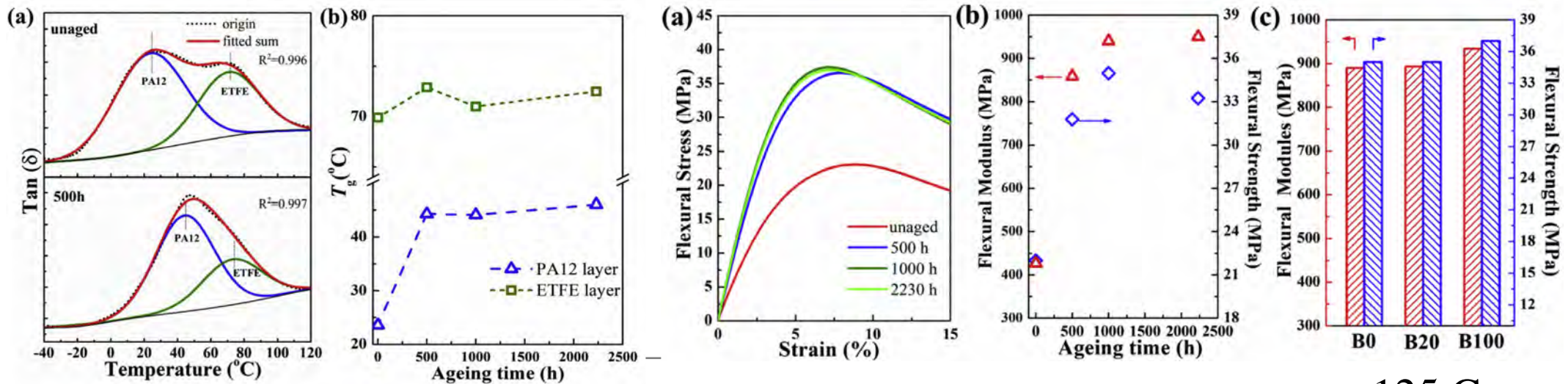
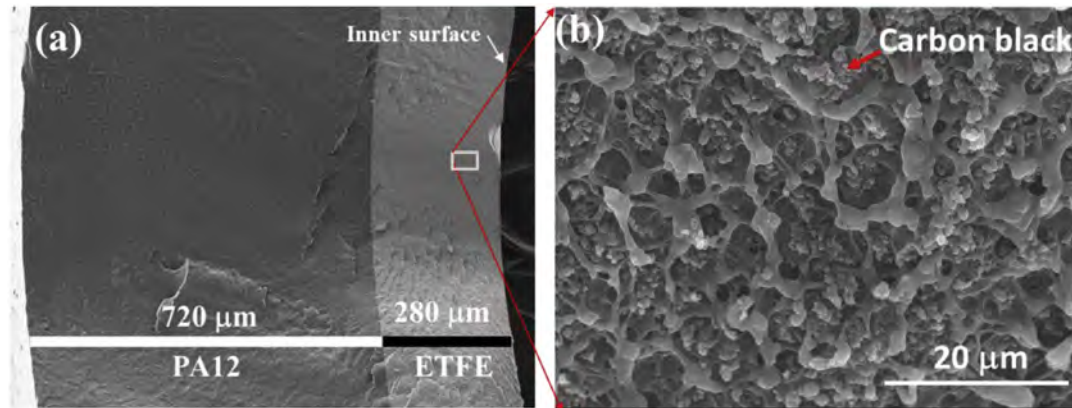


PA6 180 C Dry air

Diffusion-limited Oxidation of Polyamide: Three Stages of Fracture Behavior



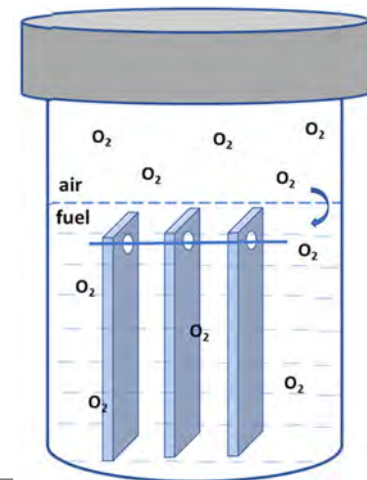
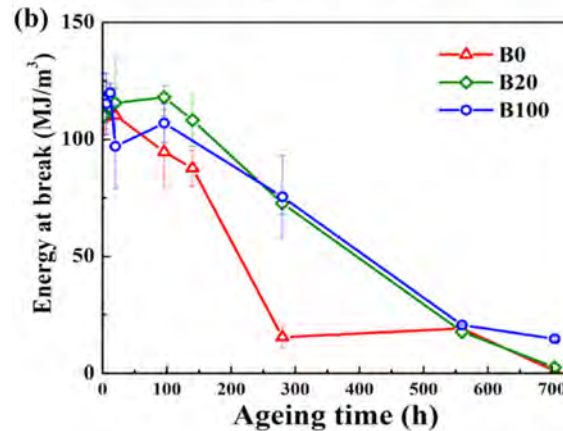
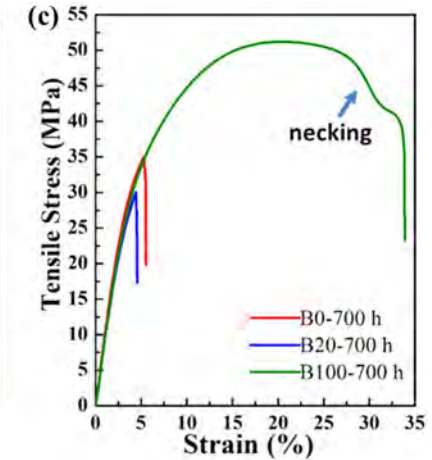
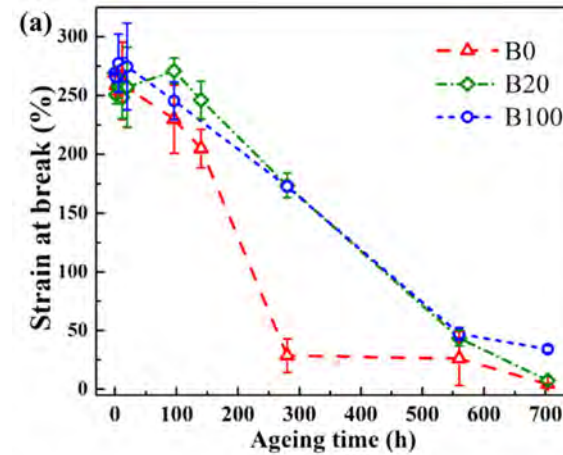
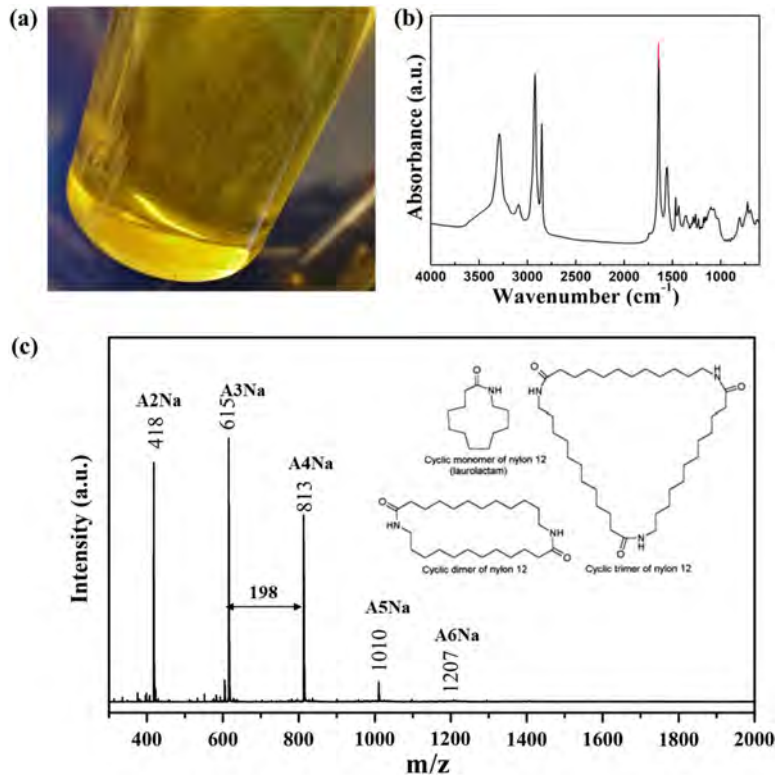
Long-term performance of a polyamide-12-based fuel line with a thin ETFE inner layer exposed to bio- and petroleum diesel



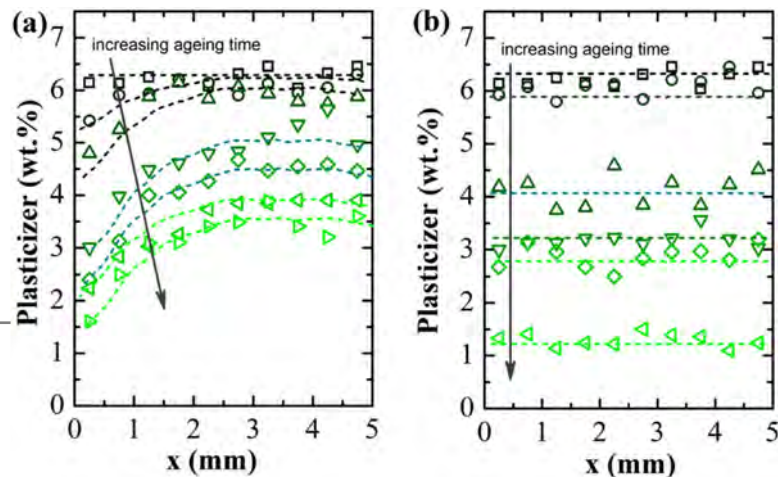
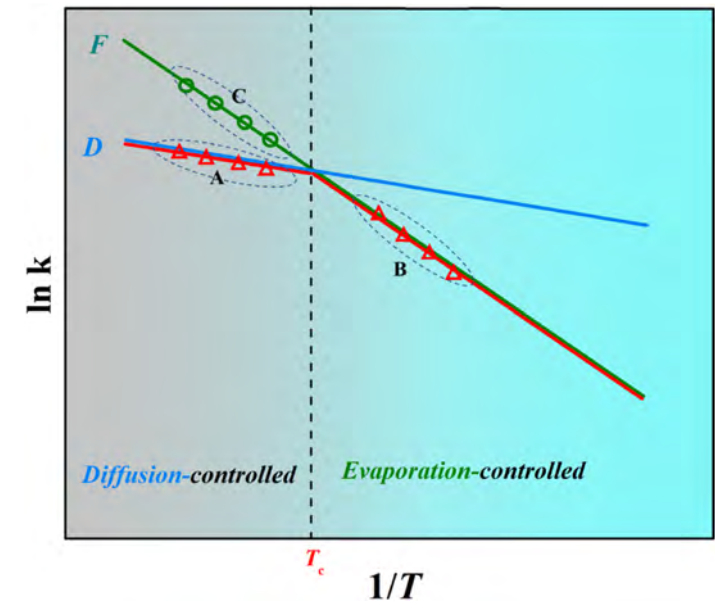
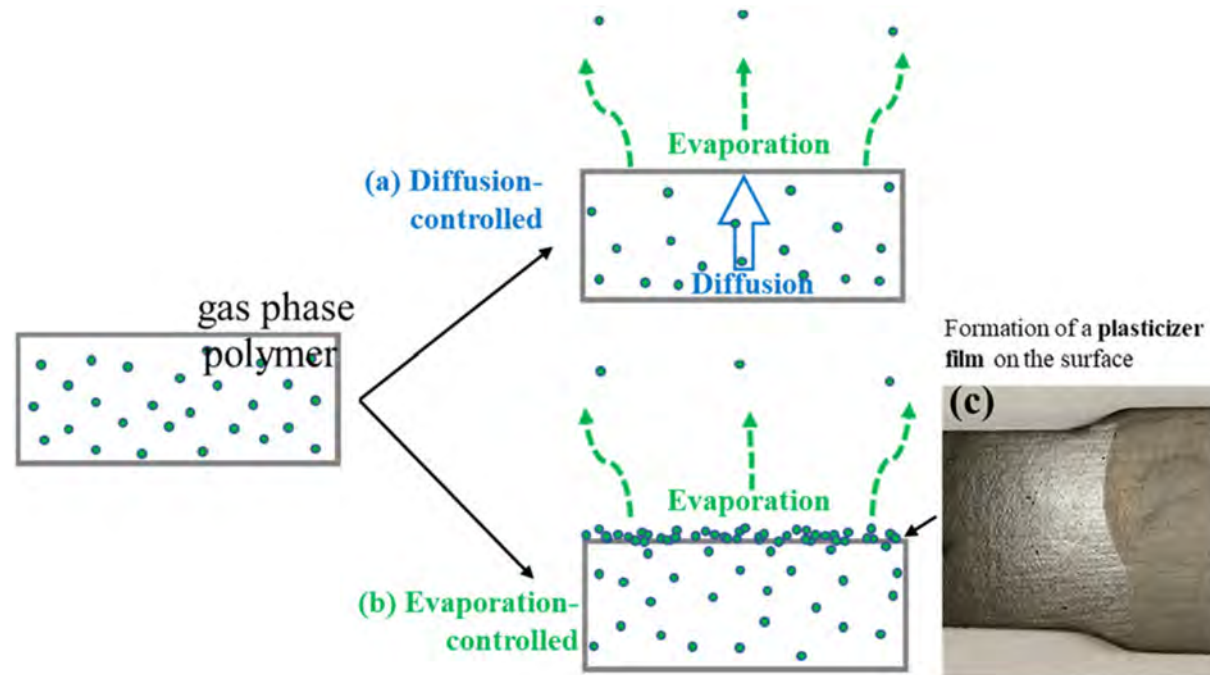
125 C

Polyamide 12 exposed to (bio)diesel at high temperature: Ageing properties and polymer/fuel interactions

125 C



Plasticiser loss from plastic or rubber products through diffusion and evaporation



Prediction over T_g
Complex, safety factor
Case: PA12 125 C to 60 C

Rubbers in fuel/engine parts of vehicles

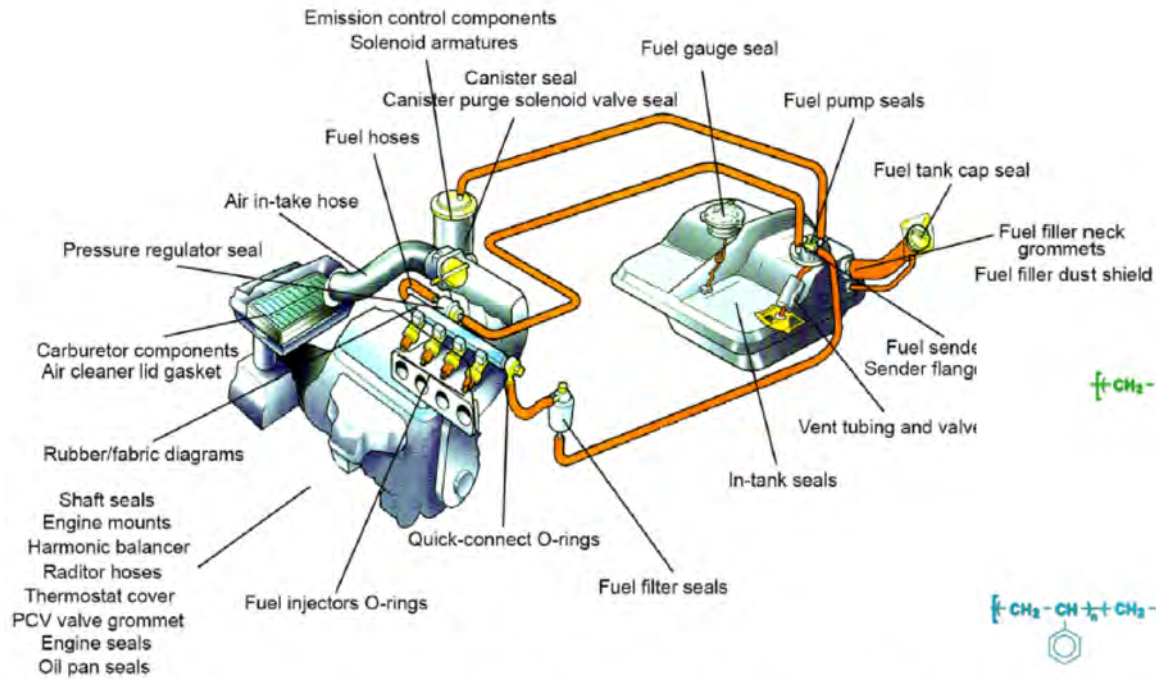


Fig. 1. The location of some of the rubber parts in a conventional fuel system

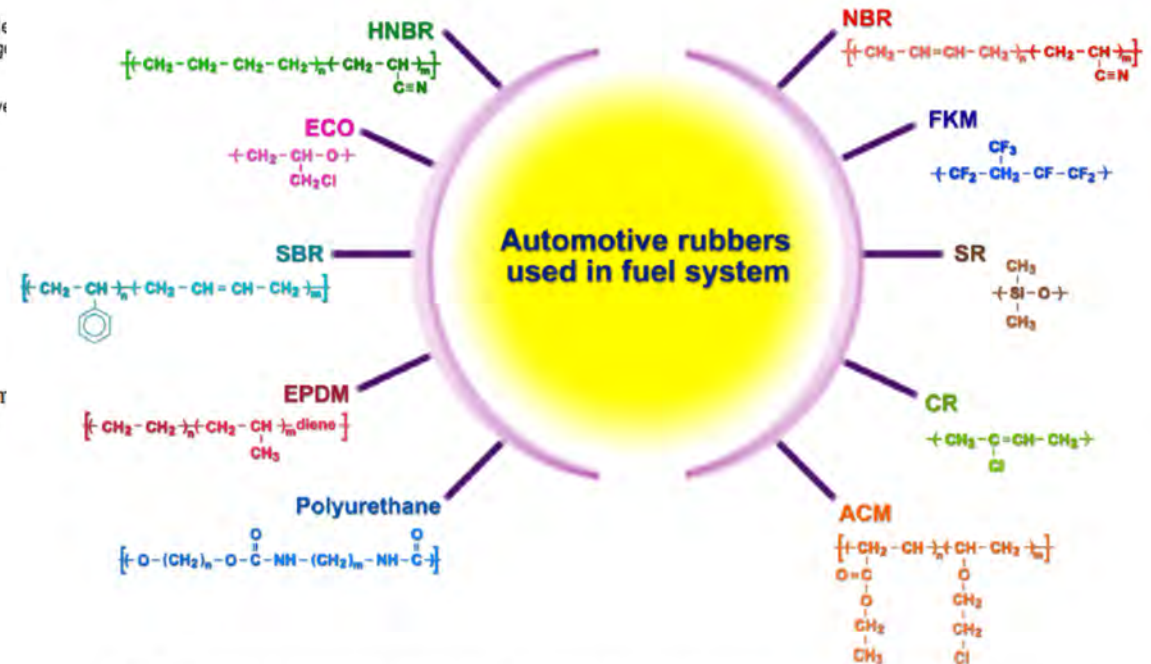
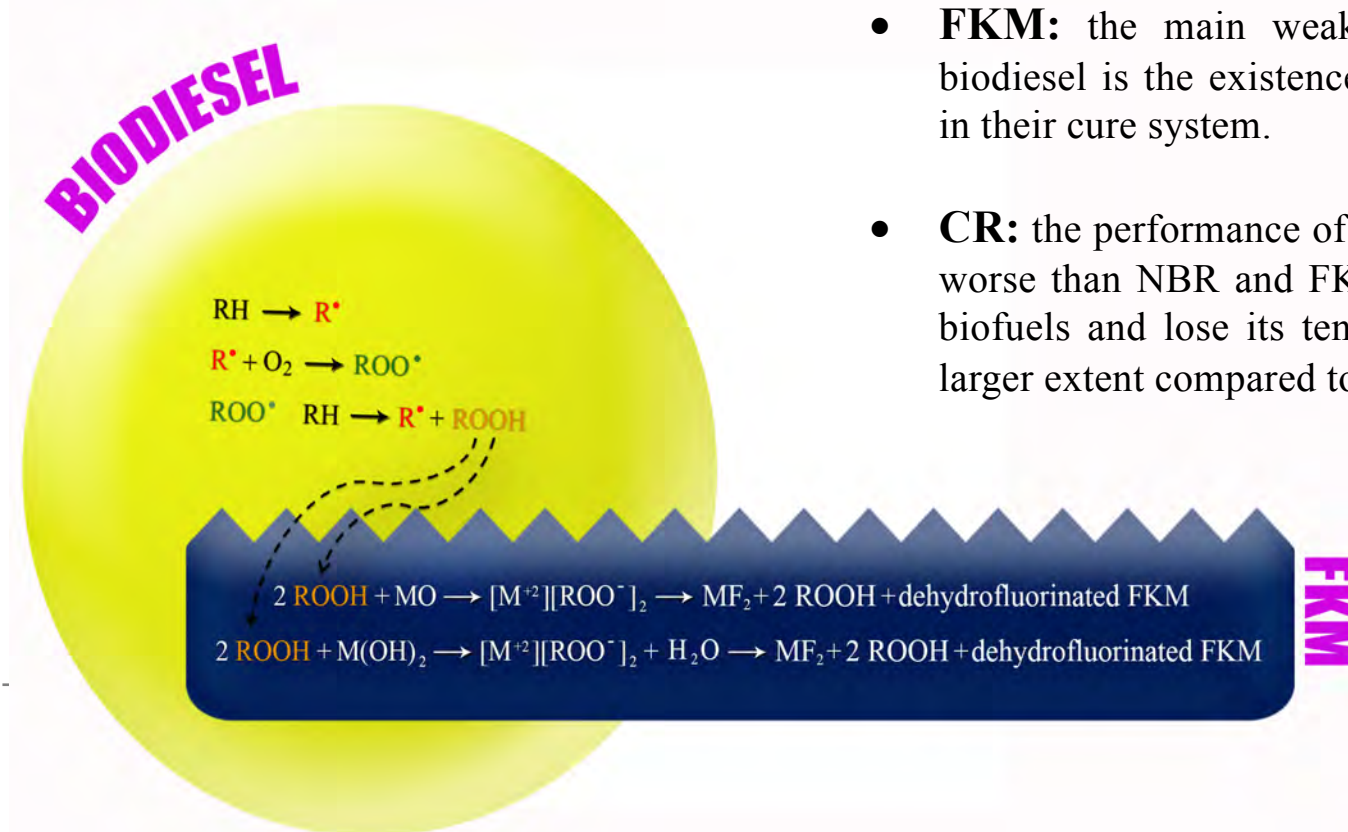


Fig. 2. Chemical structures of the rubbers most frequently used in automobile fuel systems.

“Deterioration of **Automotive Rubbers in Biofuels**: A Review”, S. Akhlaghi, M. S. Hedenqvist, M. T. Conde Braña, M. Bellander and U. W. Gedde, *Renew. Sustain. Energy Rev.* **43** (2015) 1238-1248.

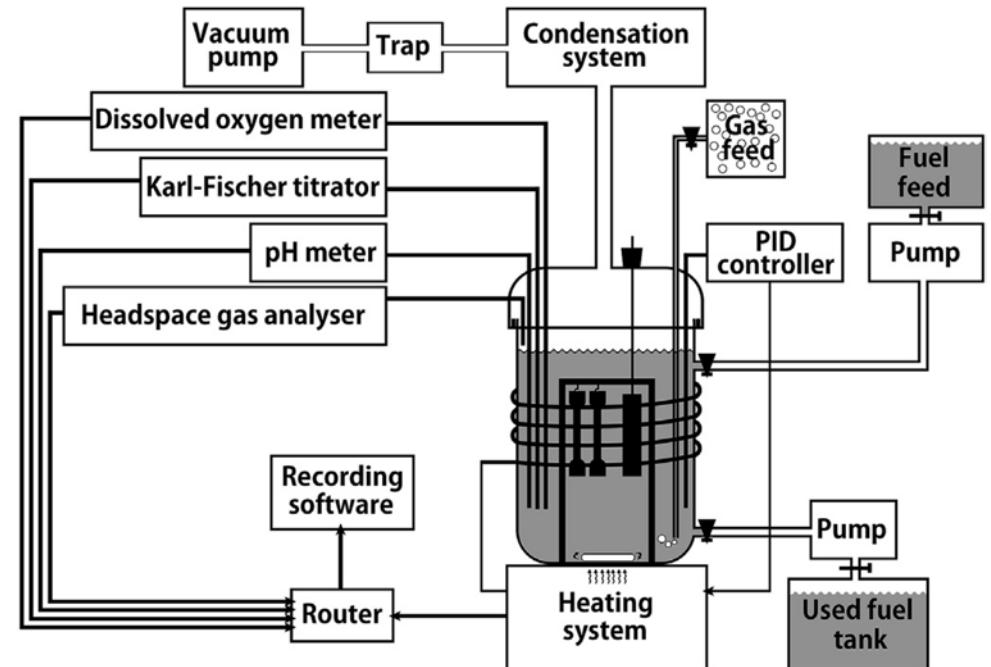
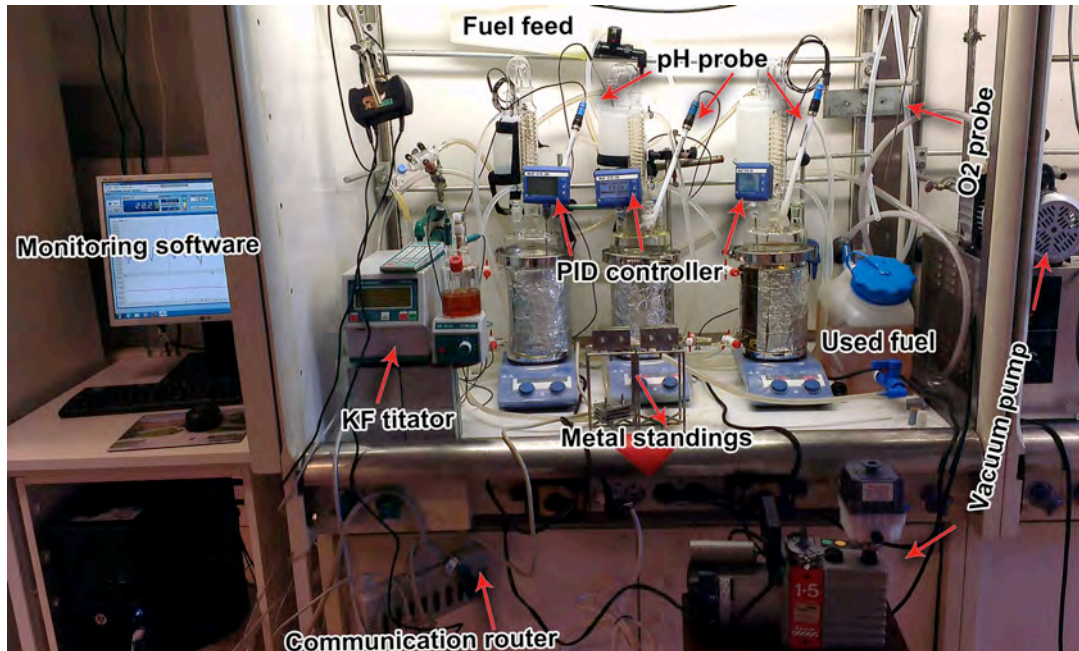
Rubbers in fuel/engine parts of vehicles

- **NBR:** the physical and mechanical properties of NBR decrease after exposure to almost all the commercially available biofuels. NBR resistance to biofuels is improved by increasing ACN% of the rubber compound as well as using sulfur cure system instead of peroxide-based crosslinking system.
- **FKM:** the main weakness of FKM rubbers towards biodiesel is the existence of metal oxides and hydroxides in their cure system.
- **CR:** the performance of CR in biodiesel and bioethanol is worse than NBR and FKM. CR swells much more in the biofuels and lose its tensile properties and hardness to a larger extent compared to FKM and NBR.



Plastic/rubber immersed in fuel

fuel: water/O₂ content, acidity

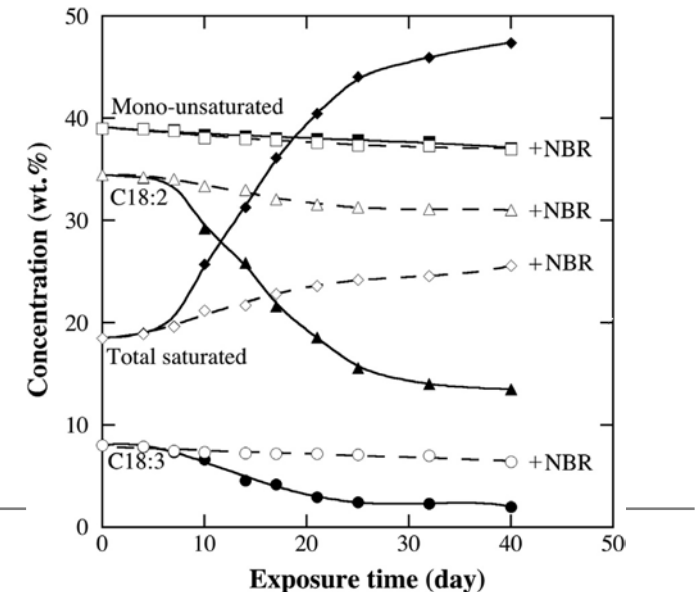
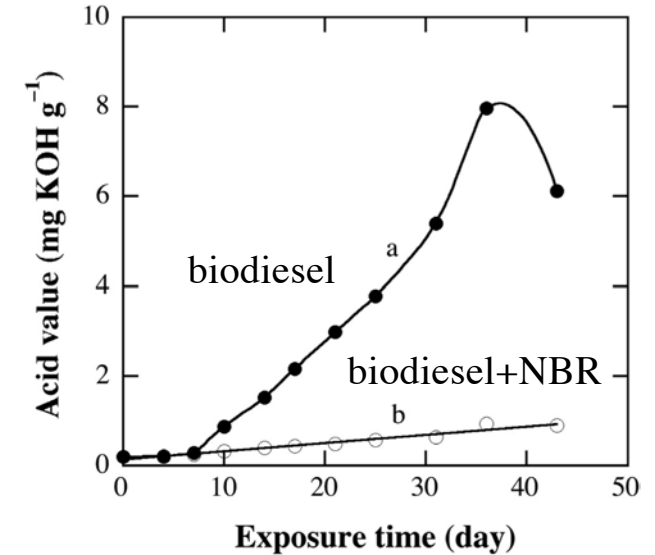
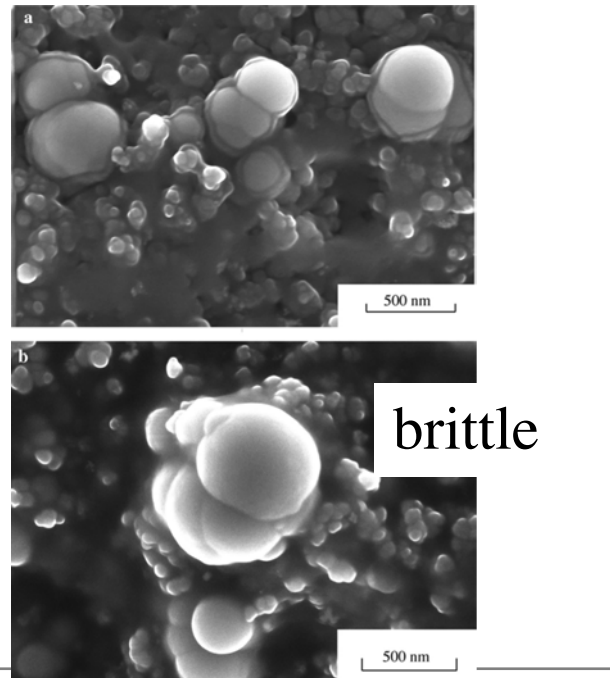
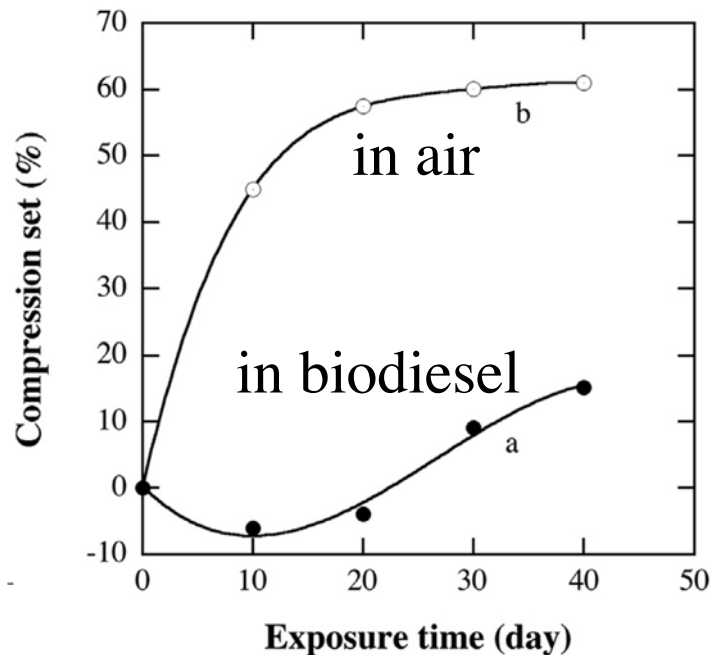


Nitrogen/oxygen gas purge into the fuel
 Creating different p_{O_2} , removal of headspace if necessary

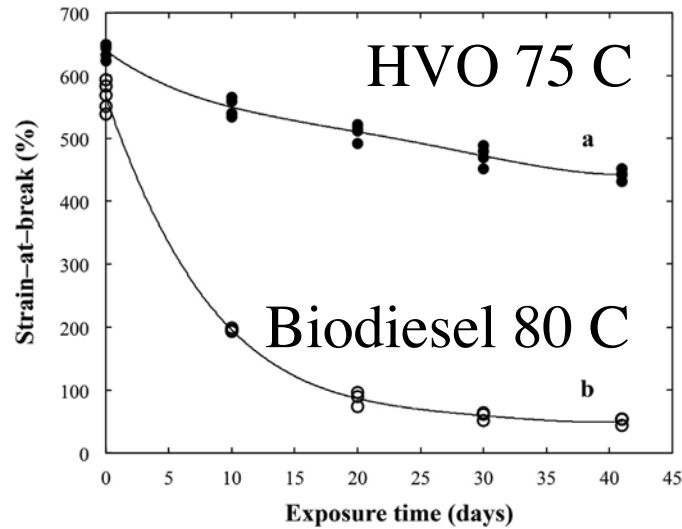
Deterioration of NBR rubber in rapeseed biodiesel

- migration of stabilizer/plasticiser from the rubber to biodiesel
- diffusion of dissolved oxygen from biodiesel into NBR
- absorption of oxidation precursors of biodiesel by the rubber
- internal cavitation was caused by the attack of biodiesel on the acrylonitrile units of NBR
- biodiesel-induced swelling of rubber

90 C

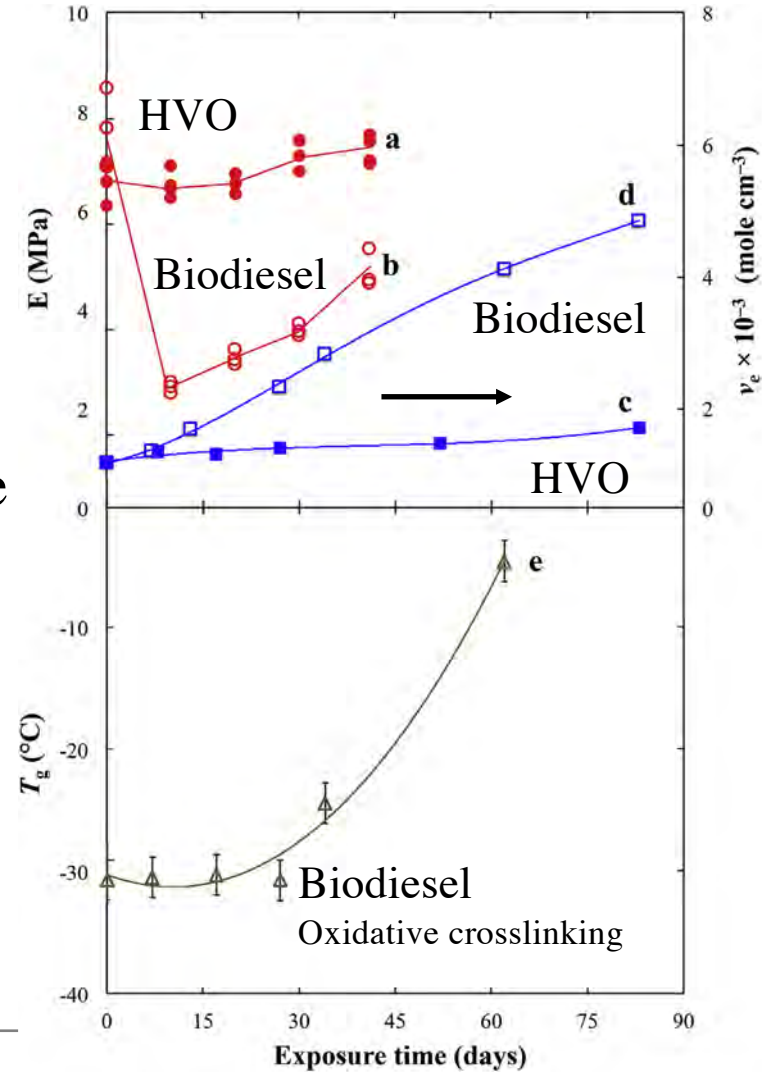
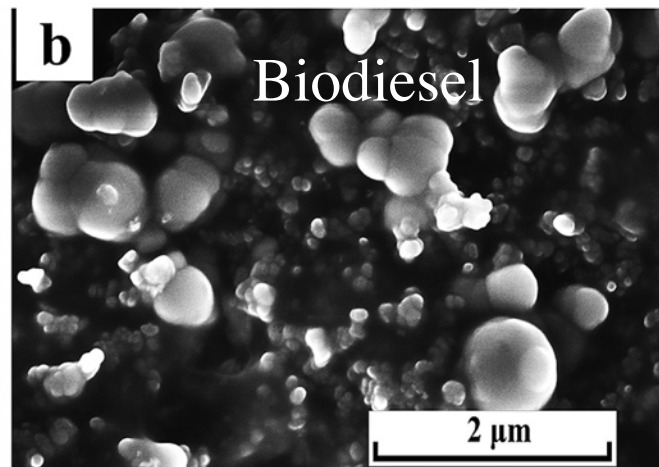
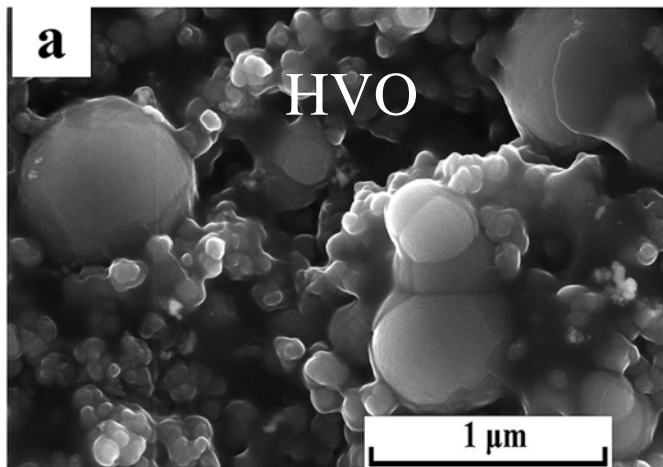


Degradation of carbon black-filled-NBR in biodiesel and HVO



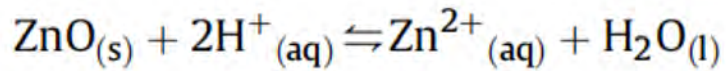
Loss of plasticiser

Cavitation in the
filler-rubber interphase
(biodiesel)



Effects of ageing conditions on degradation of NBR rubber filled with heat-treated ZnO star-shaped particles in rapeseed biodiesel

Effects of biodiesel (80 C, acidic)

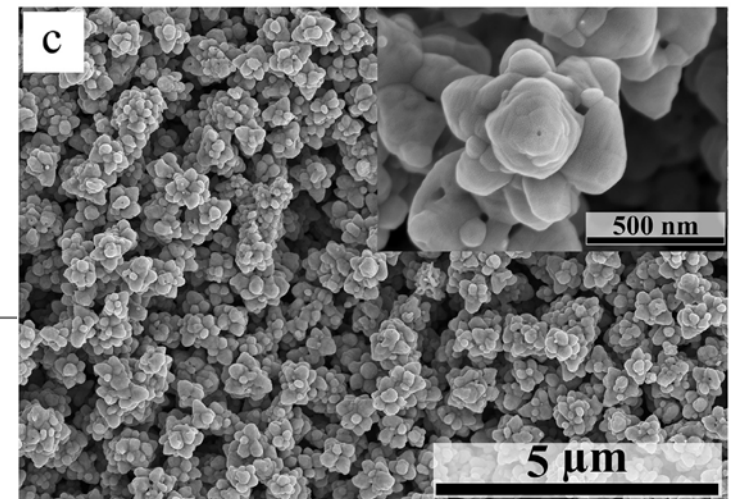
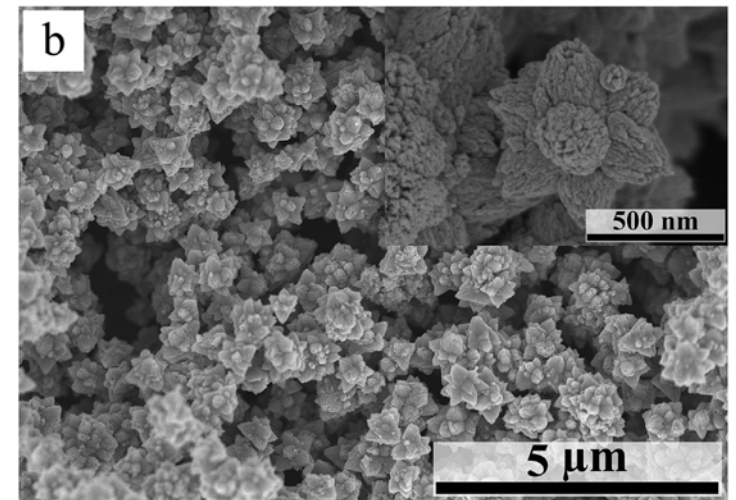
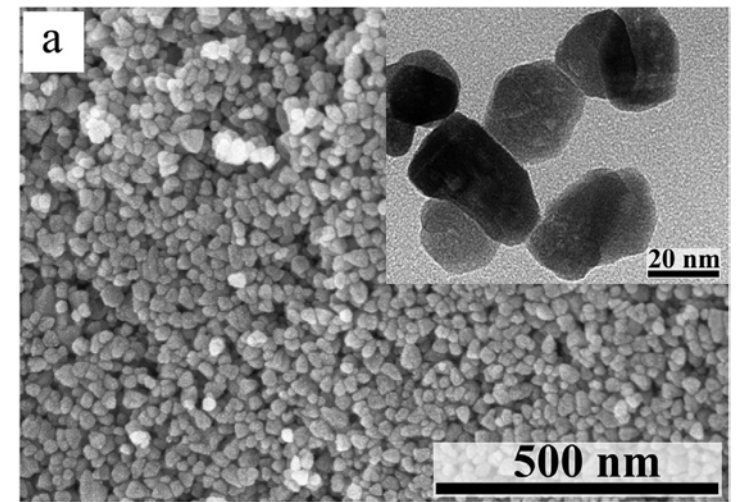
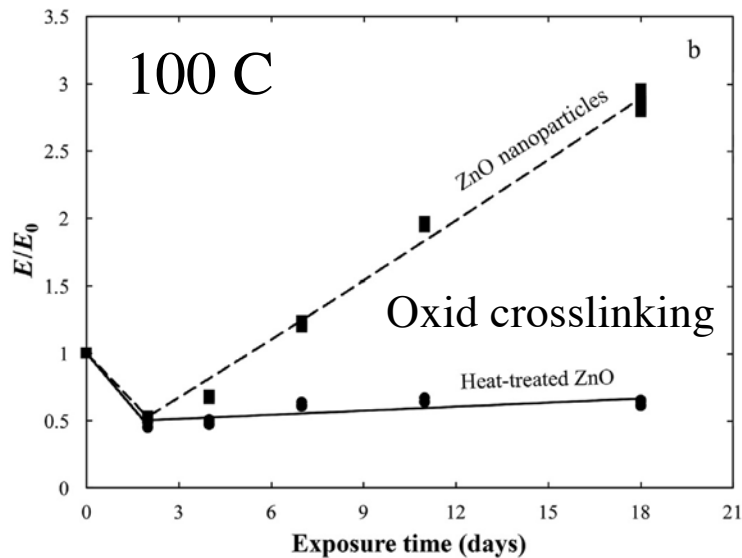


Zn²⁺ attacks the nitrile group, less hydrophilic and takes up more fuel

Nanoparticles

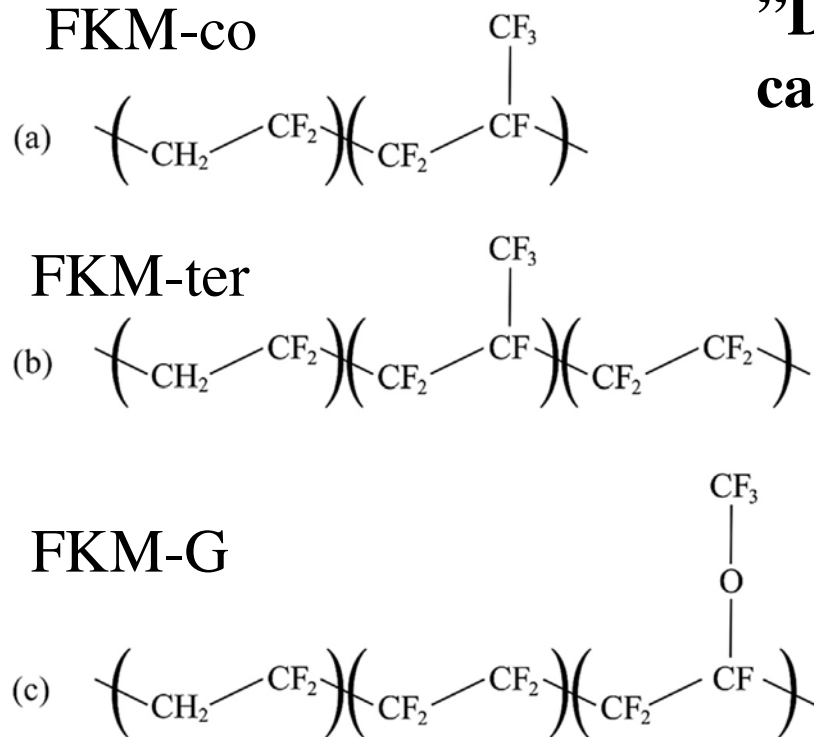
Star-shaped
Better dispersed

Heat-treated
Porous-free less reactive



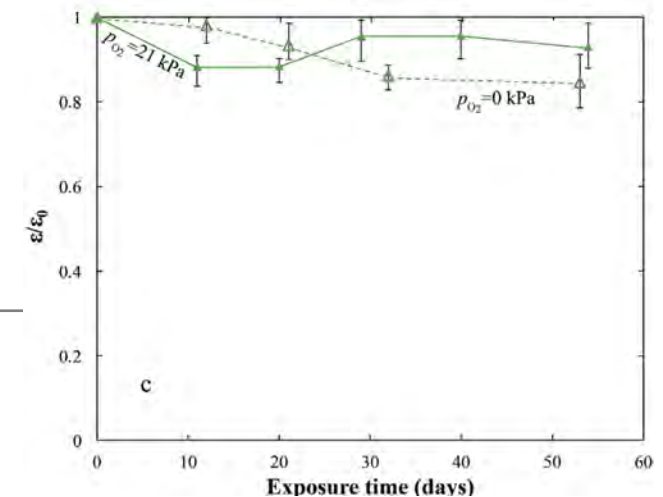
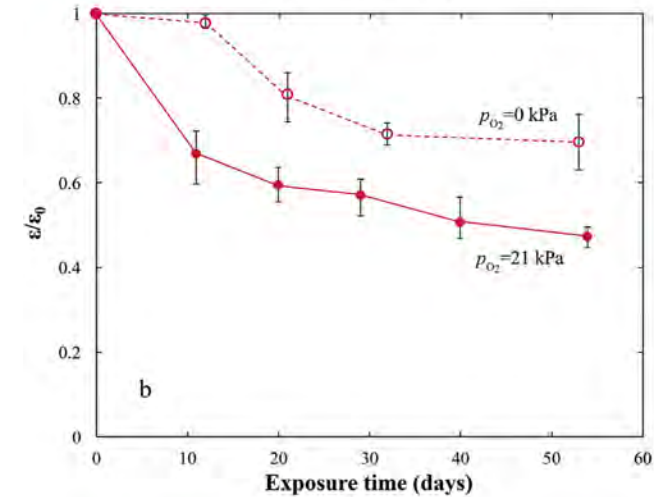
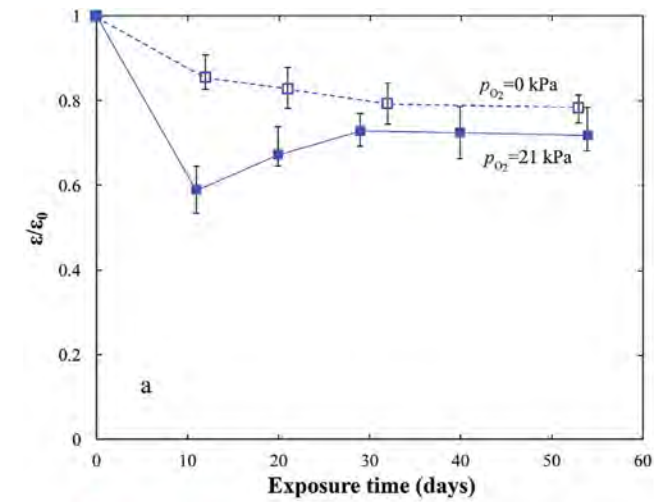
Degradation of fluoroelastomers in rapeseed biodiesel

”Dehydrofluorination causing chain cleavage”



extensive dehydrofluorination driven by metal ions and rupture of the bound rubber-carbon black network

least amount of unsaturations (where biodiesel attack) and metal oxide/hydroxide particles



Protein plastics/elastomers

Gluten polymers



A stiff "coin" (no plasticizer)

"Polystyrene / epoxy"



Soft/flexible film (with plasticizer)

"Soft PVC/LDPE"



Rubber (more plasticizer)
(Meriplast®, by Tereos-Syral)

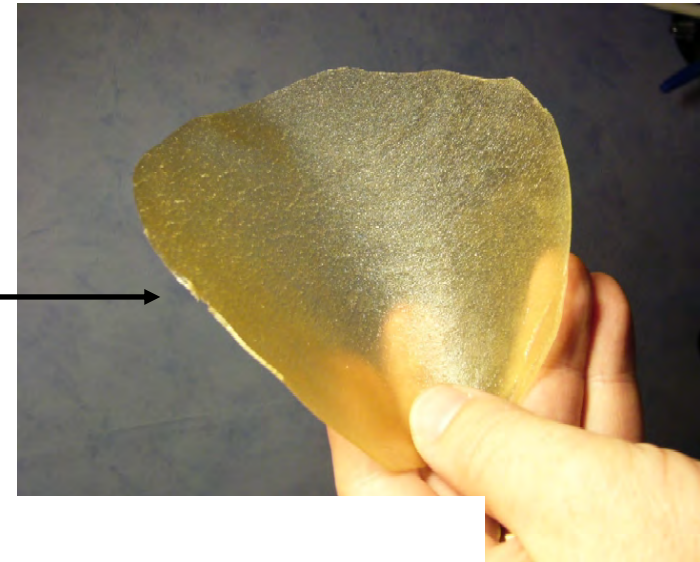
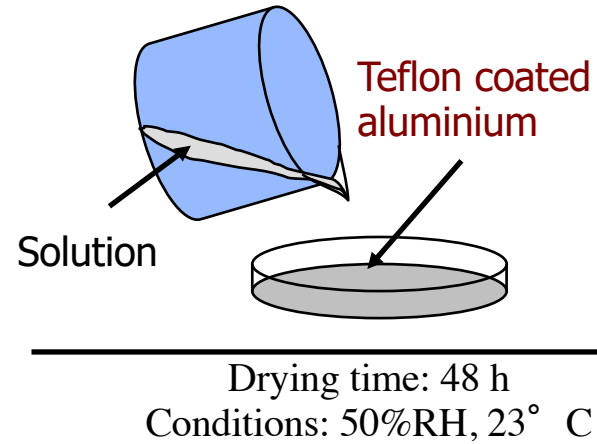


Semi-rigid (with plasticizer)

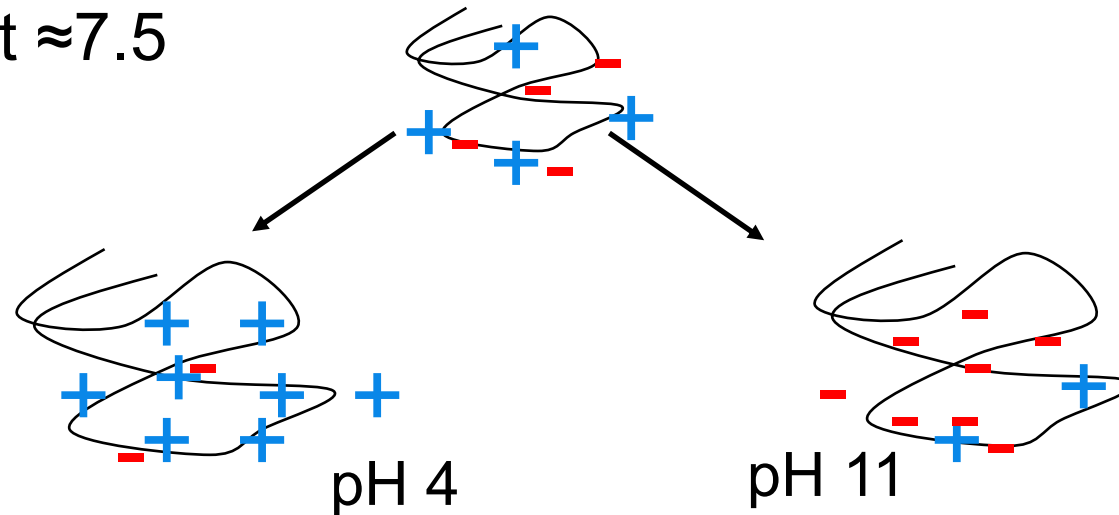
"PP or toughened PS"

Casting

- Gluten
- Glycerol (25 wt%)
- Ethanol
- Water
- pH adjustment
- Heating up to 75 ° C (2.5 ° C/min)



Isoelectric point ≈ 7.5

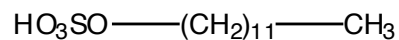




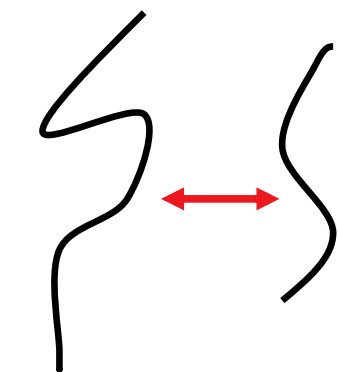
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Ext. 1

SDS

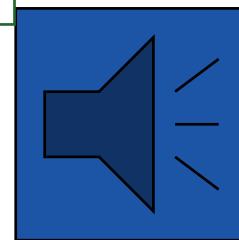


• Na

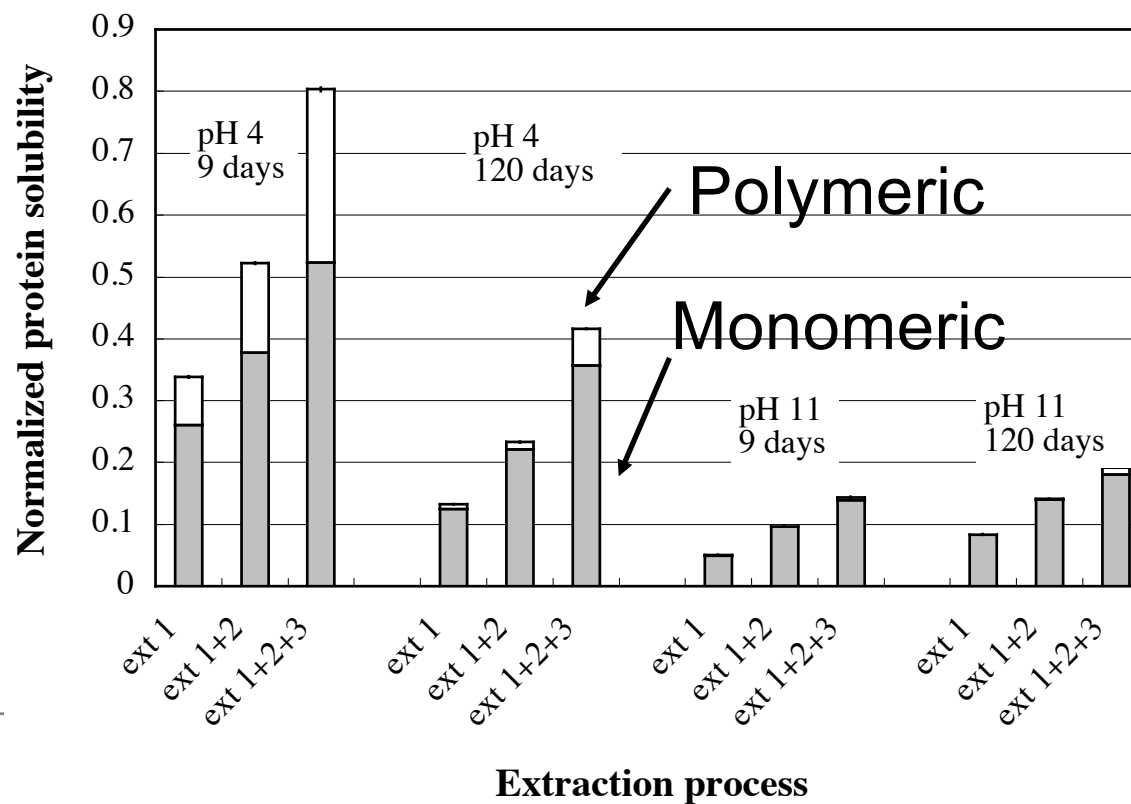
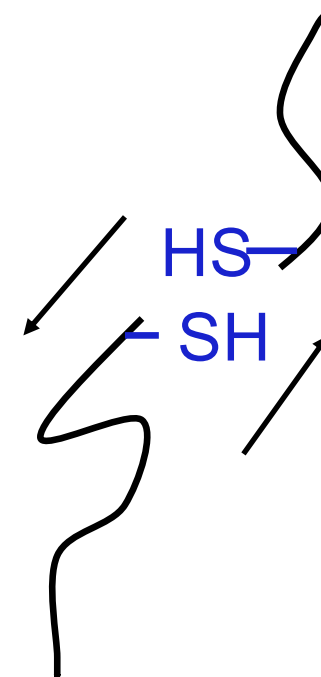


secondary bonds

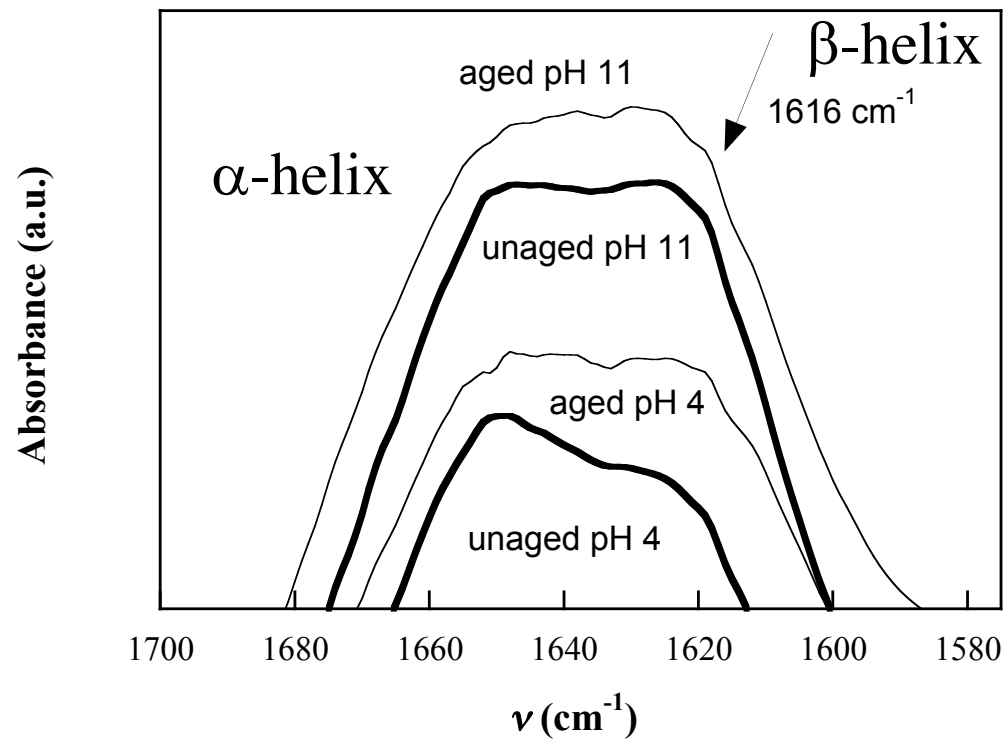
Ext. 2/3



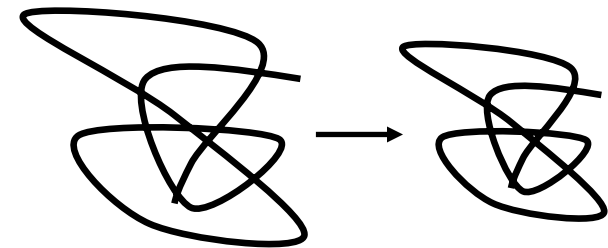
sonication



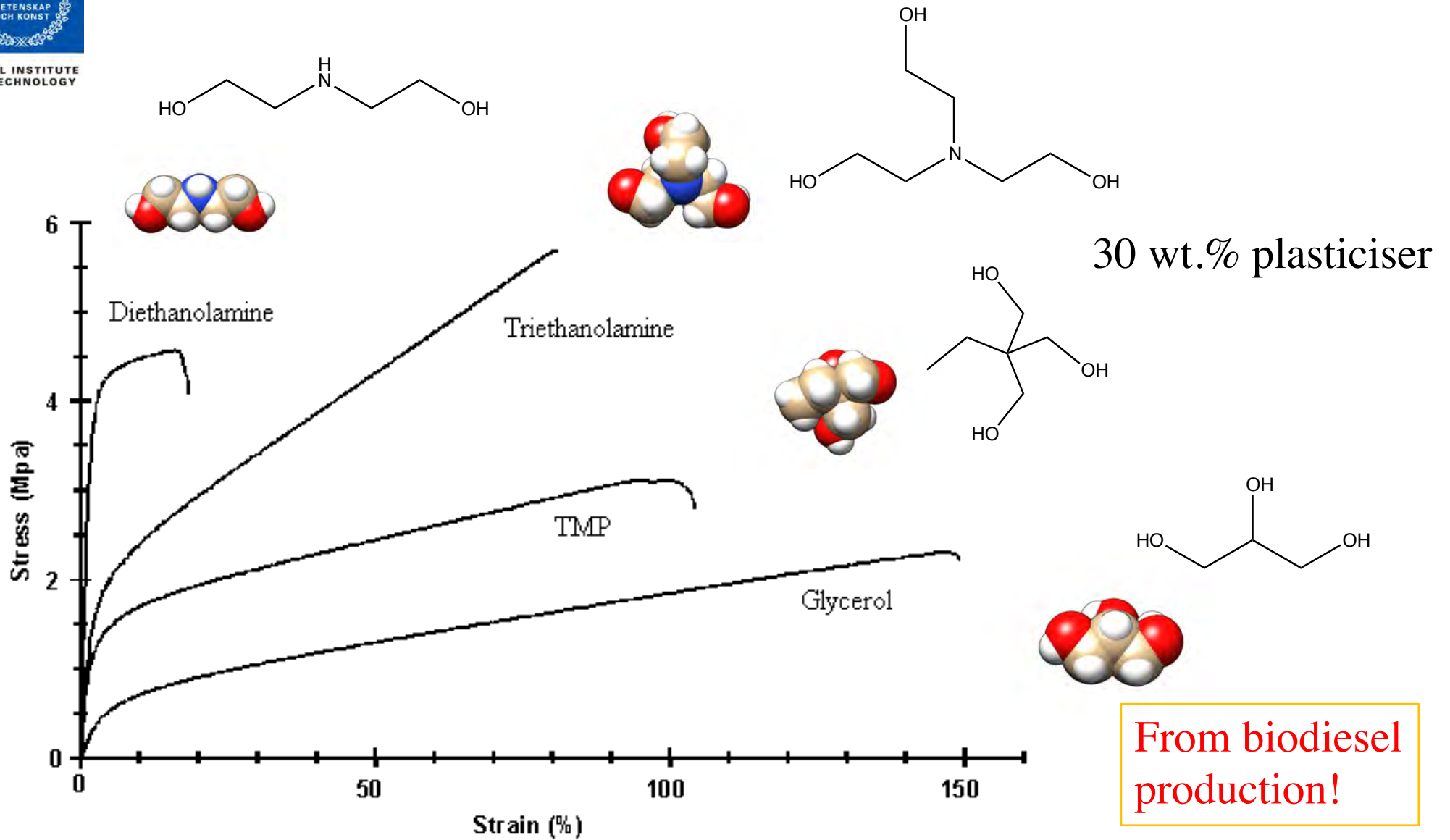
The amide I region



Aggregated
structure

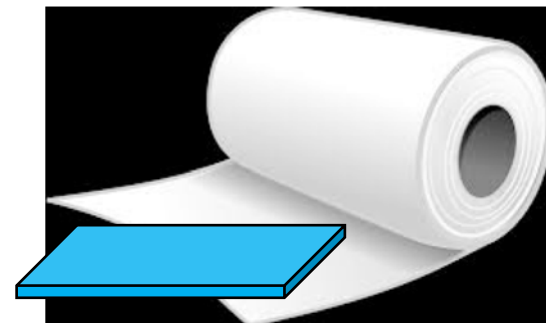
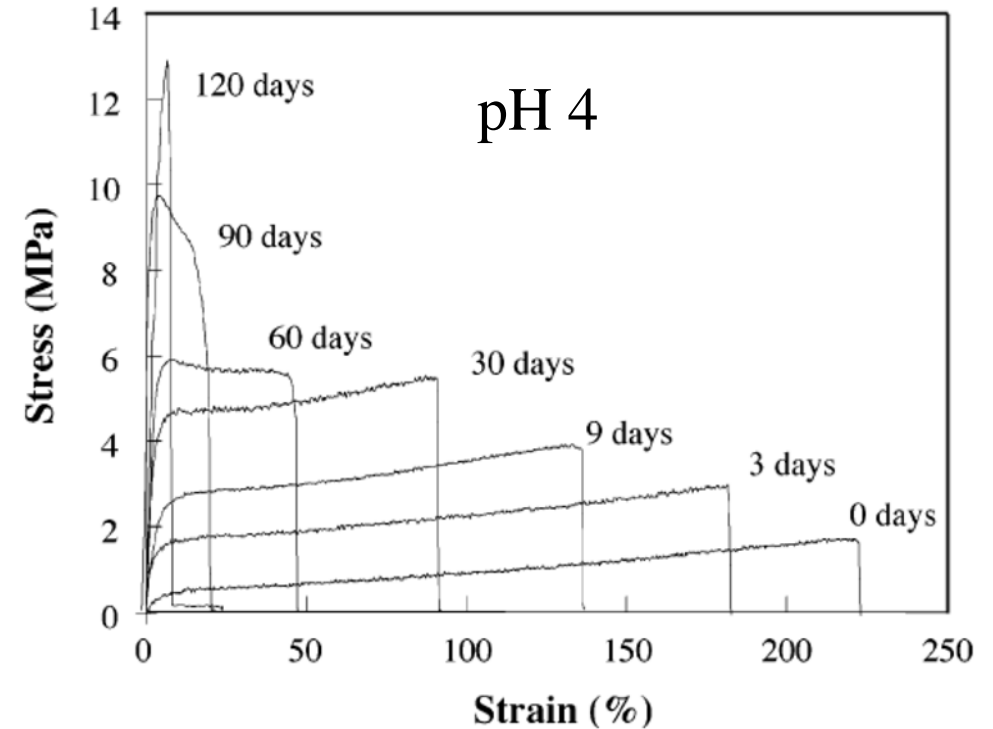
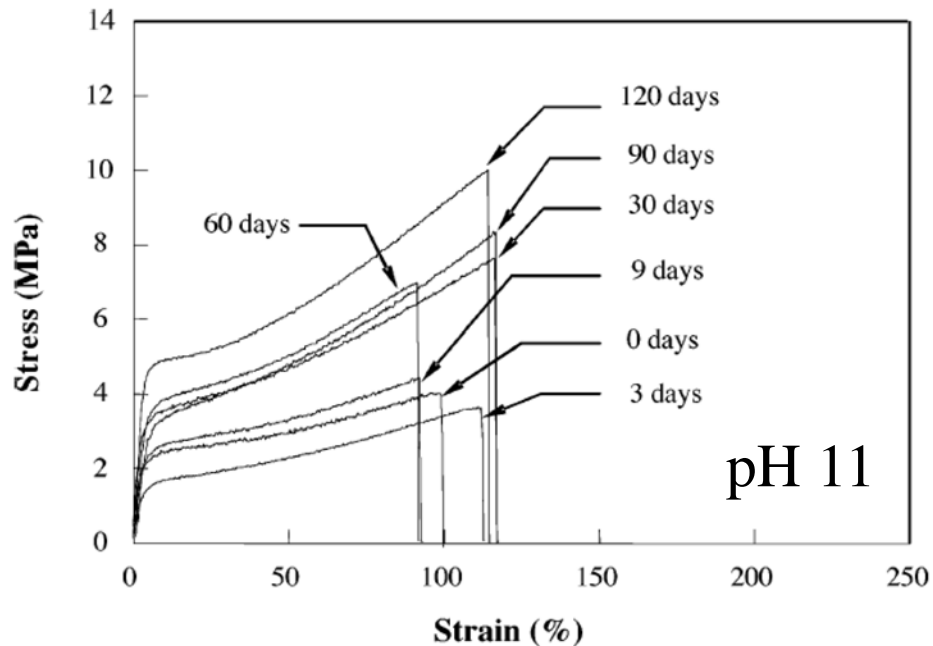


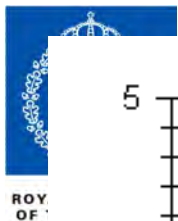
Tunable properties (gluten and plasticiser)



Glycerol migration, bleeding

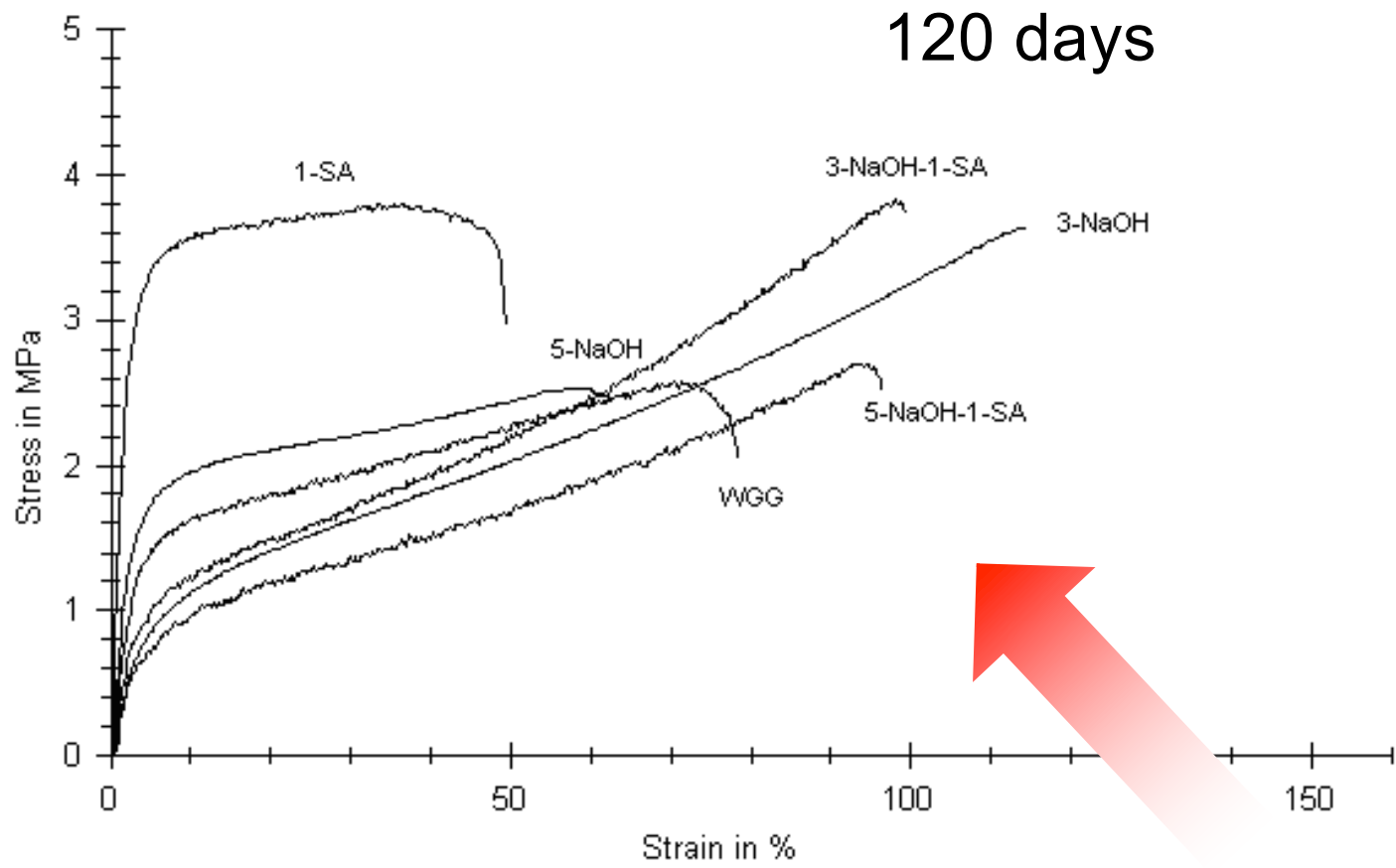
Gluten and glycerol



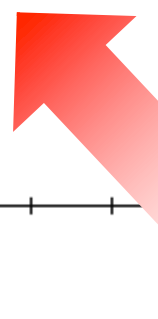
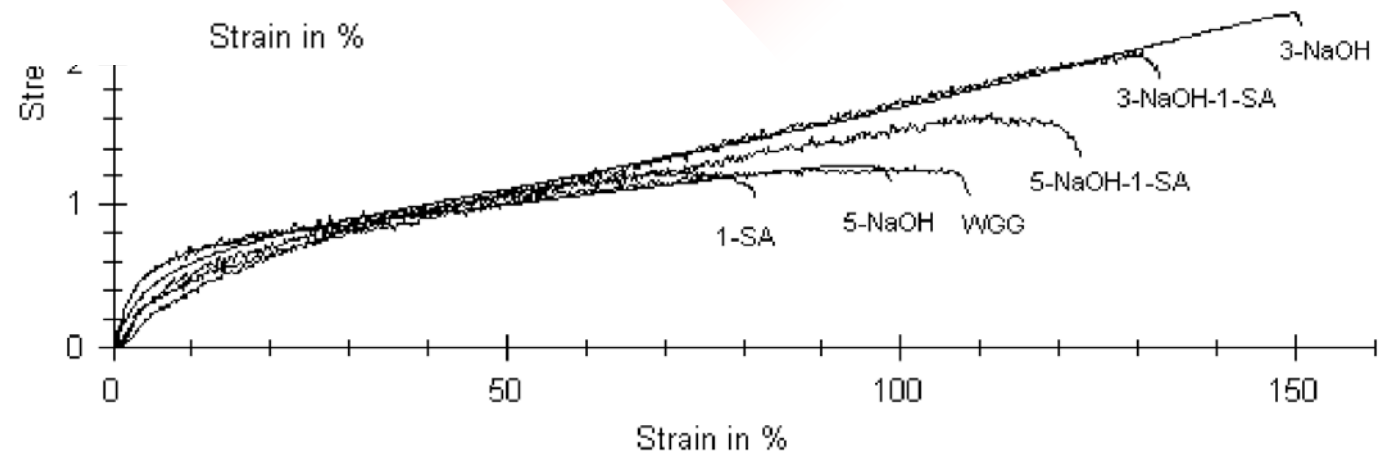


Mechanics

120 days



1 day





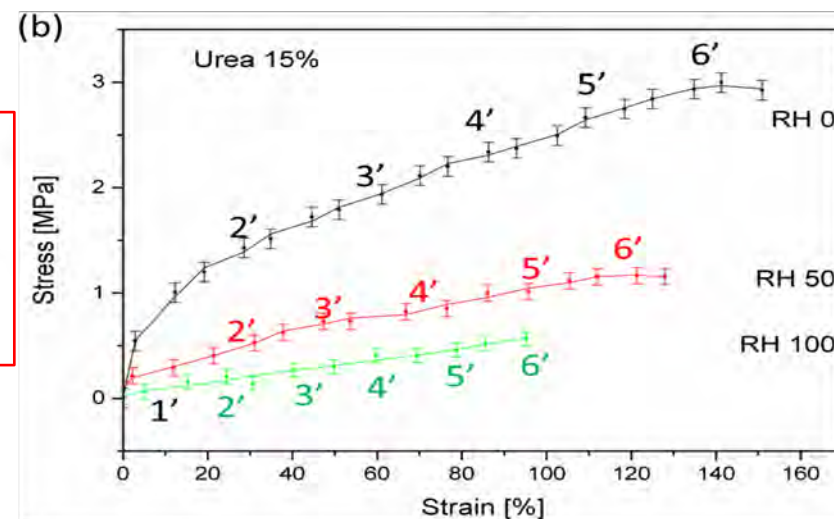
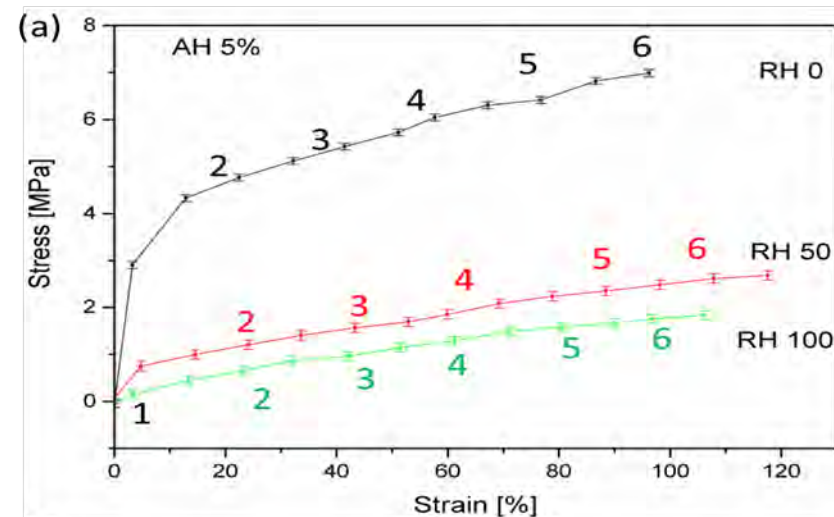
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Effects of moisture

Moisture content in gluten at different RH

Relative humidity [%]	Moisture content [%]					
	AH3	AH5	AH10	U10	U15	U20
0	0	0	0	0	0	0
50	9.5	9.3	9.4	10.4	10.8	11.0
100	51.6	51.0	51.4	55.6	57.5	58.9

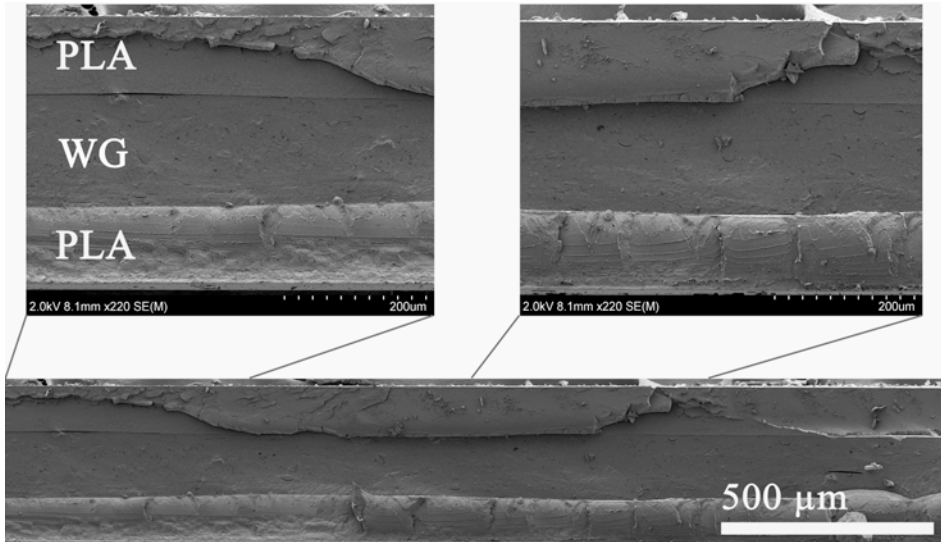
sample	OP (cm ³ ·mm/m ² ·day·atm)		WVTR (g·mm/m ² ·day)
	at 23 °C, 0% RH	at 23 °C, 50% RH	at 38 °C, 90% RH
WG-110-30	0.117/0.329 ^a	7.771/8.156	OR ^b



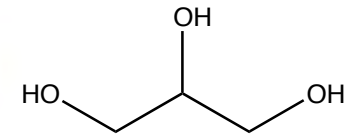
S.-W. Cho et al. *J. Agric. Food Chem.* **58** (2010) 7344-7350.

S. Yu et al. *ACS Sustain. Chem. Eng.* 2016.

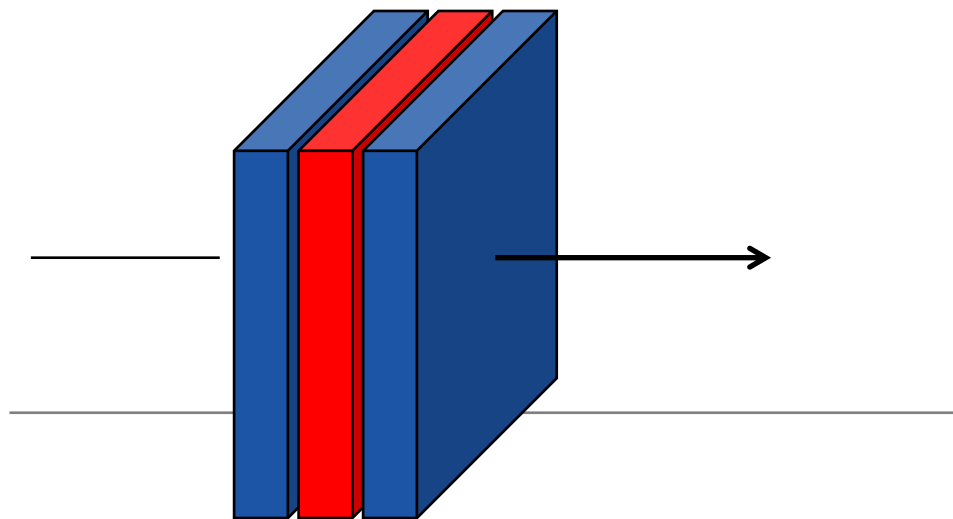
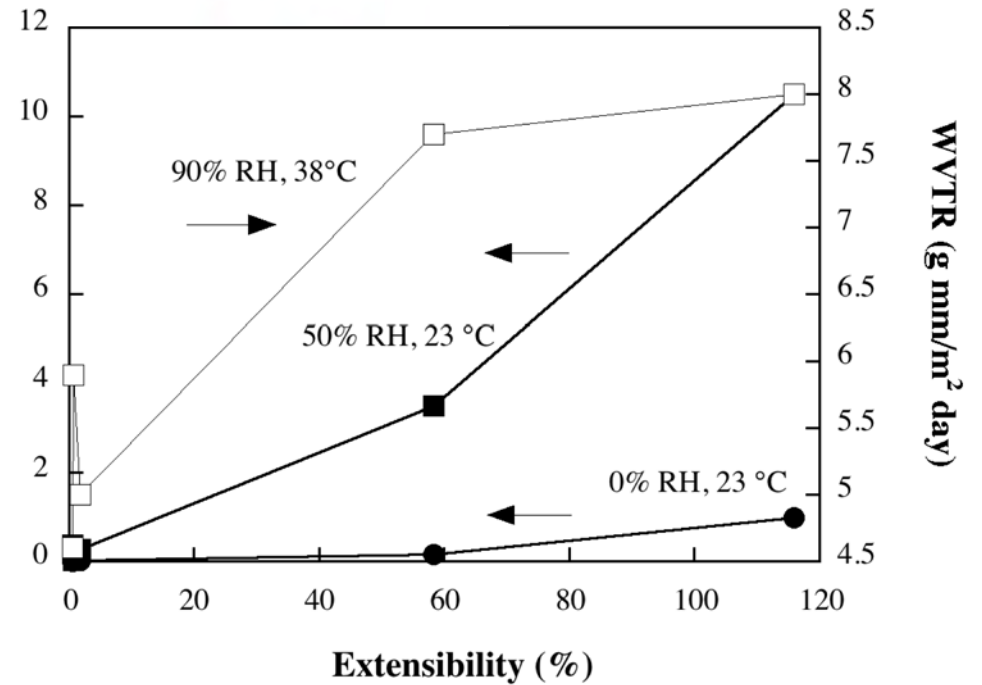
High barrier solutions



Glycerol in wheat gluten (WG)



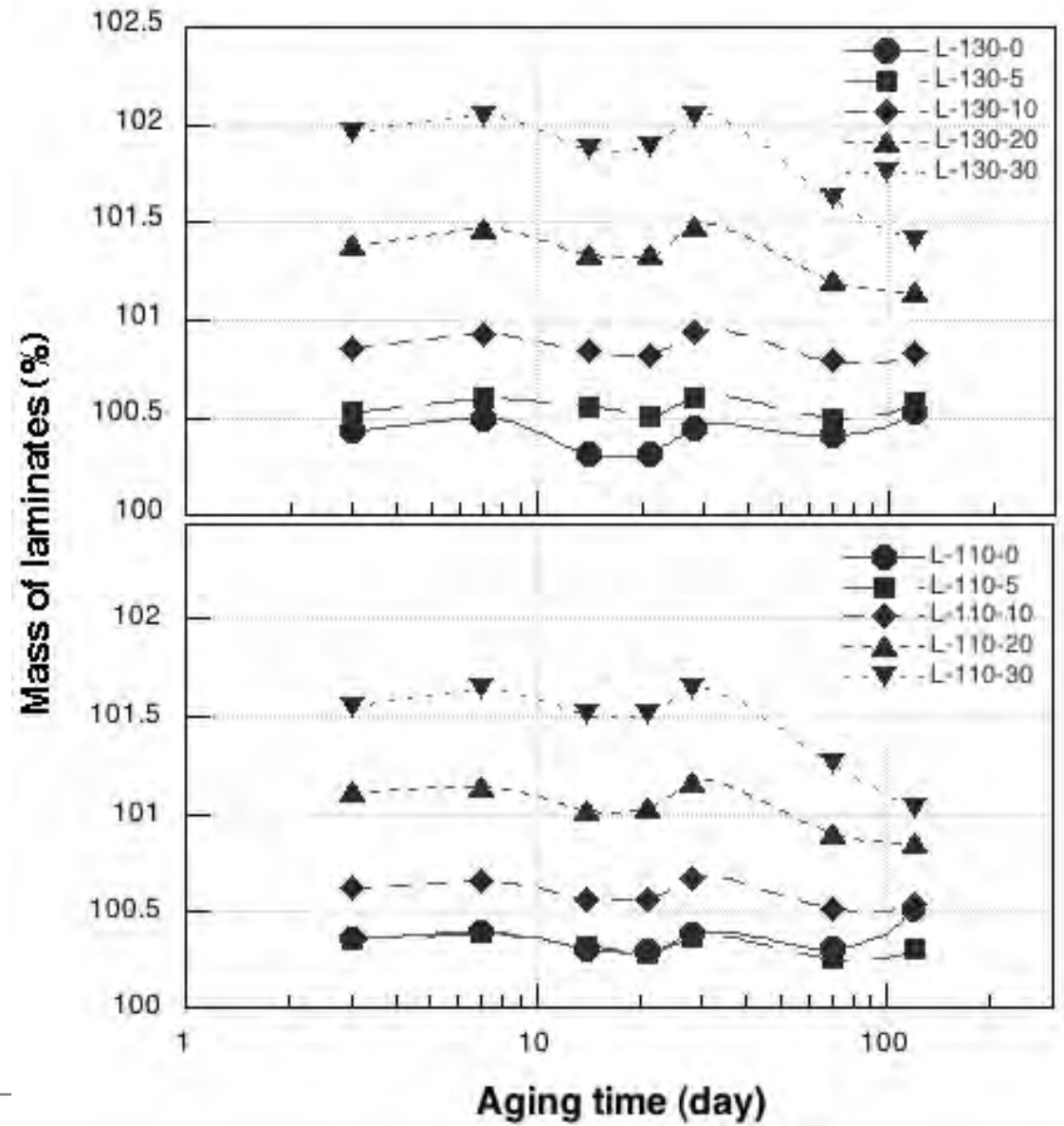
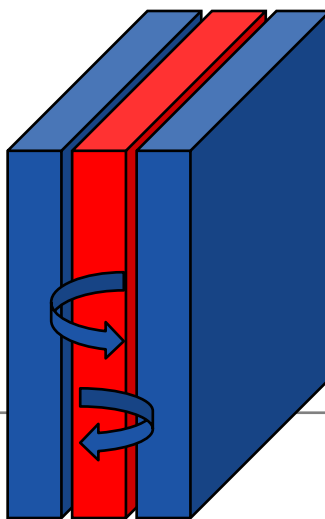
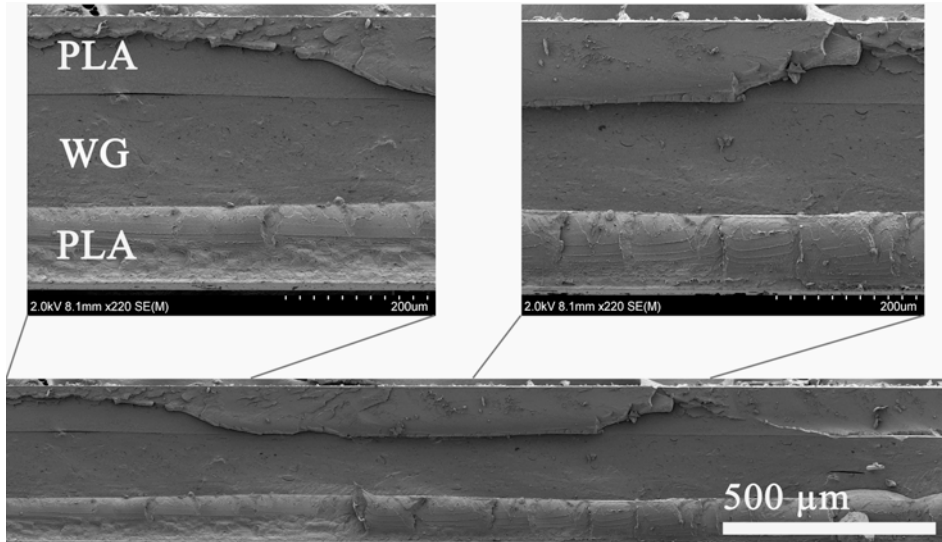
Oxygen permeability ($\text{cm}^3 \text{mm}/\text{m}^2 \text{day atm}$)



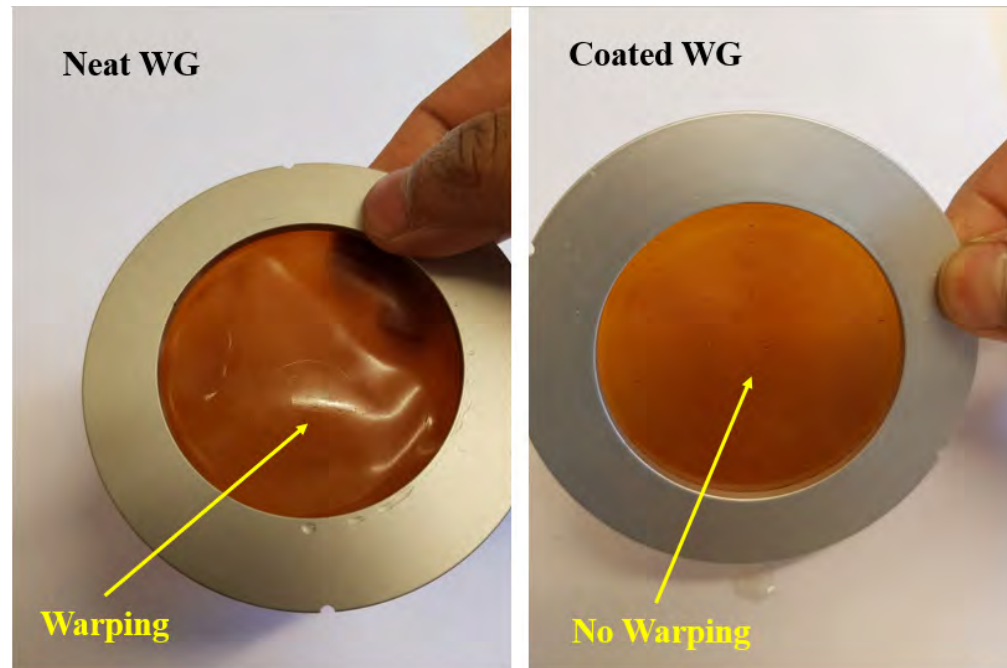


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No migration



PET-coated wheat gluten



100 %/50 % RH
profile



WVTR (PET)
 $11.2 \pm 0.6 \text{ g/m}^2/\text{day}$

Biodegradation of hemp fibre-reinforced wheat gluten



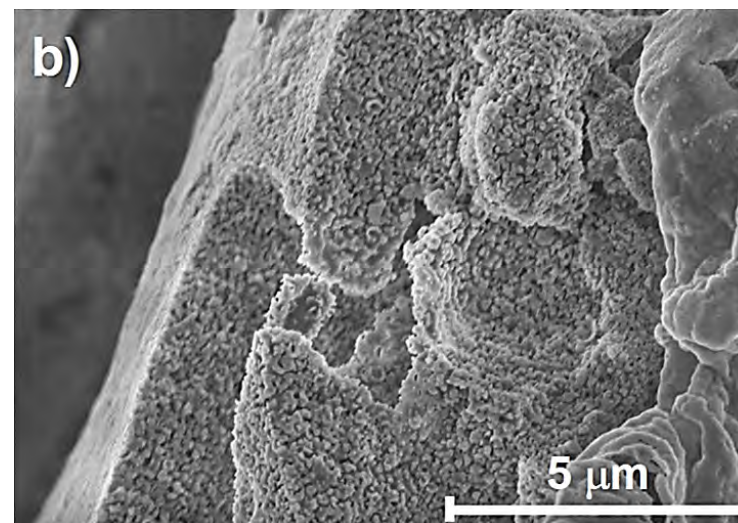
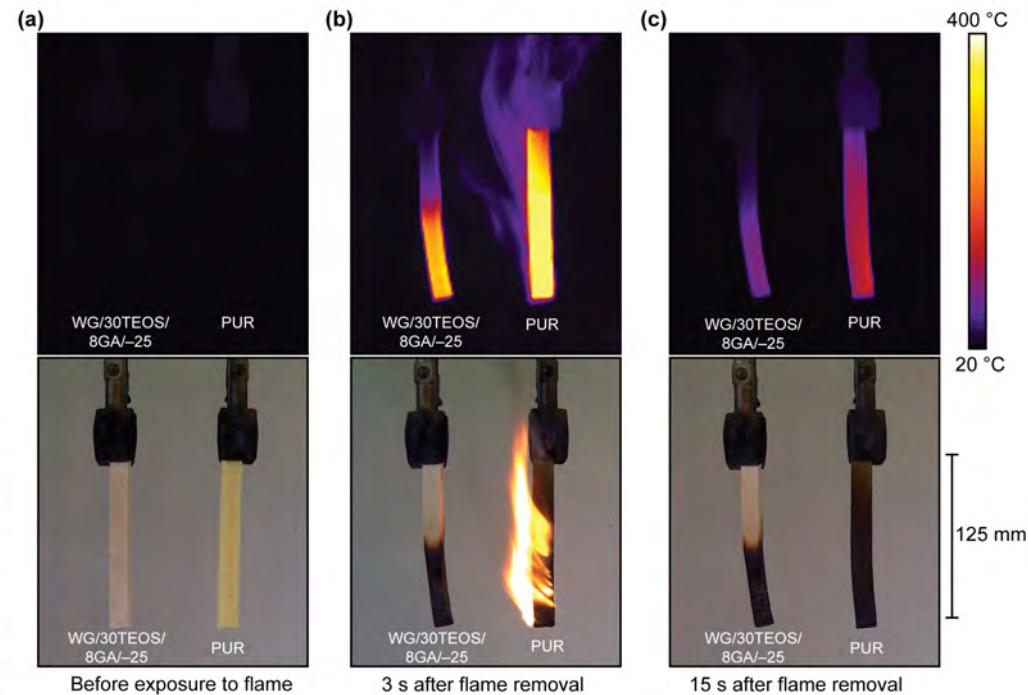
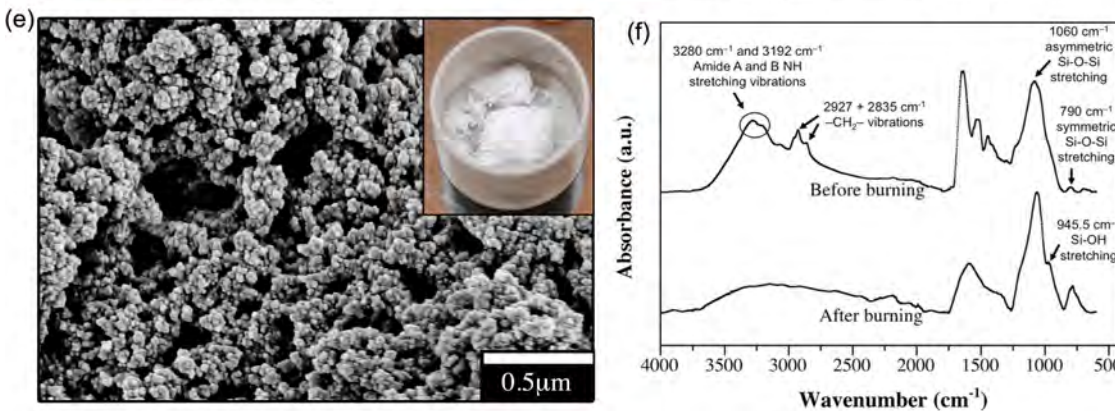
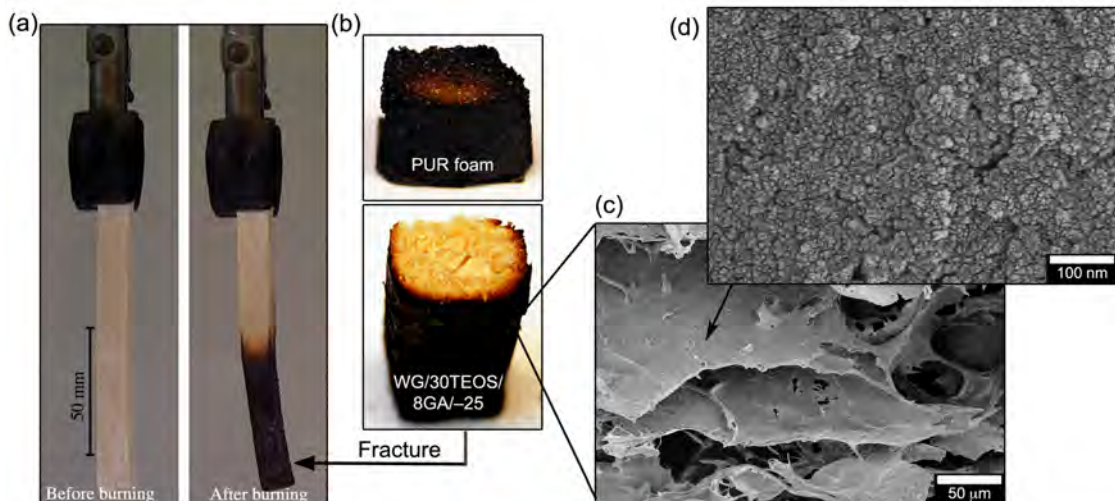
Biodegradation of the composite after 45 (left) and 180 days (right). Soil for the experiment was obtained from an organically grown field situated near the Swedish University of Agricultural Sciences, Alnarp (N55.661303, E13.077222).

fire properties

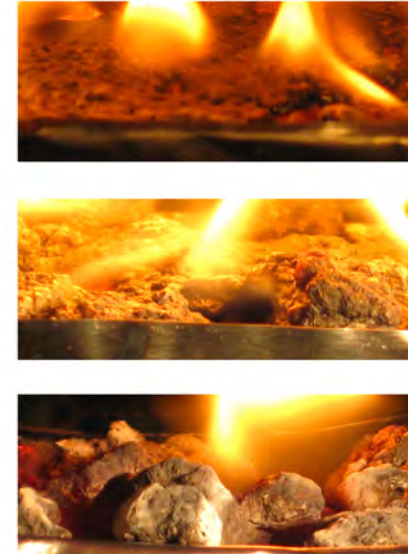
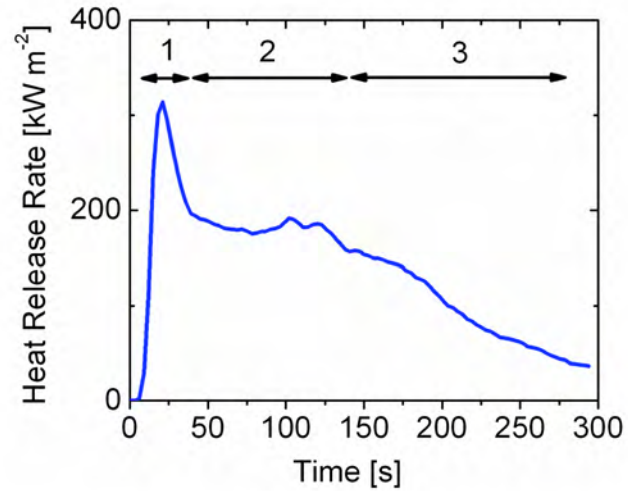
Hybrid films and foams

In-situ polymerized silica

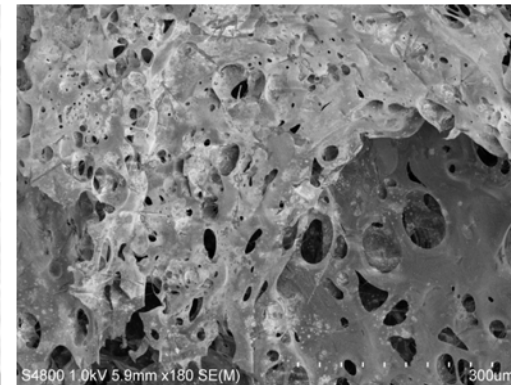
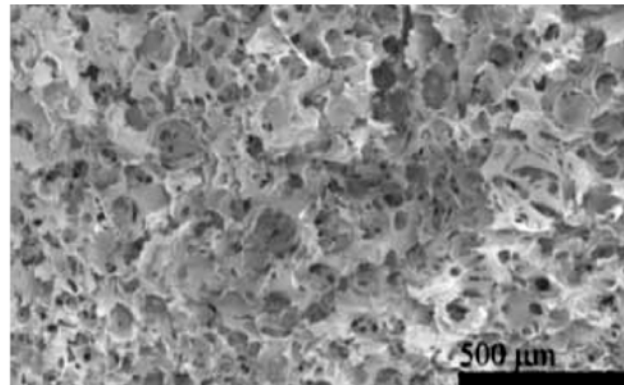
Gluten



fire properties

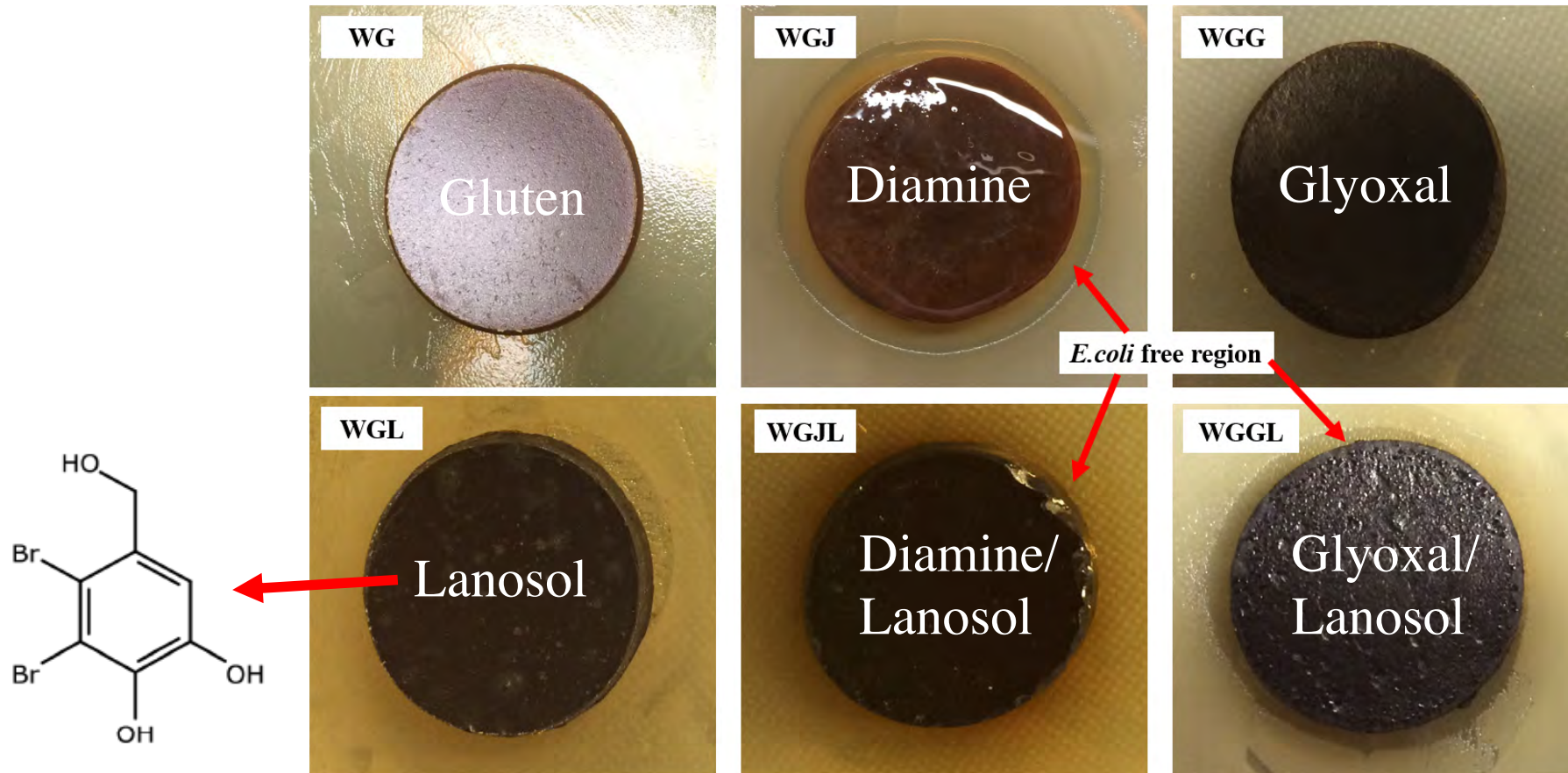


before

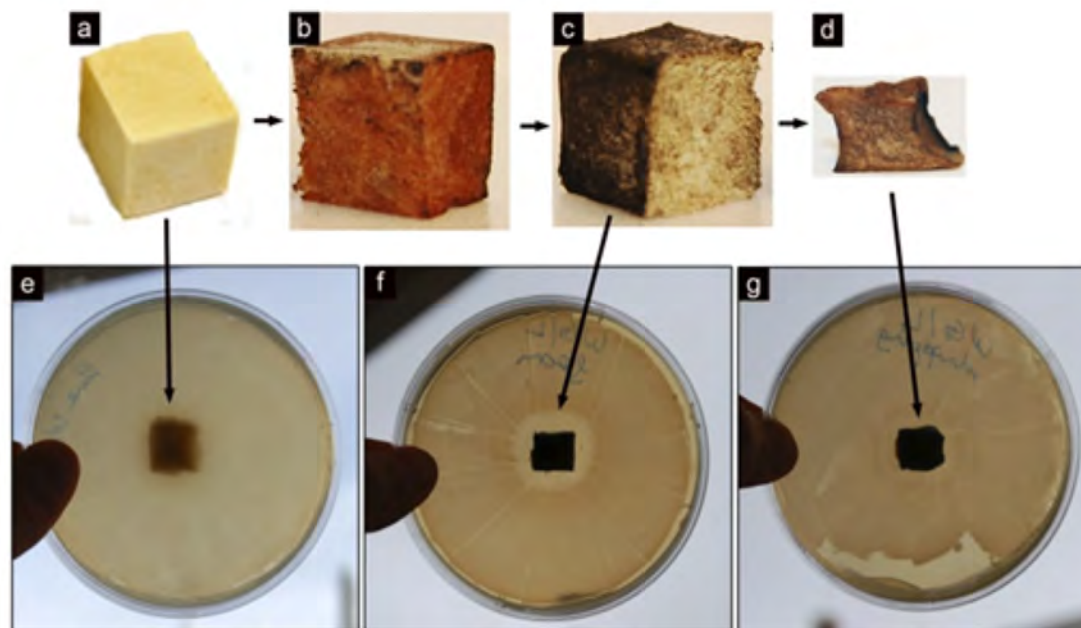
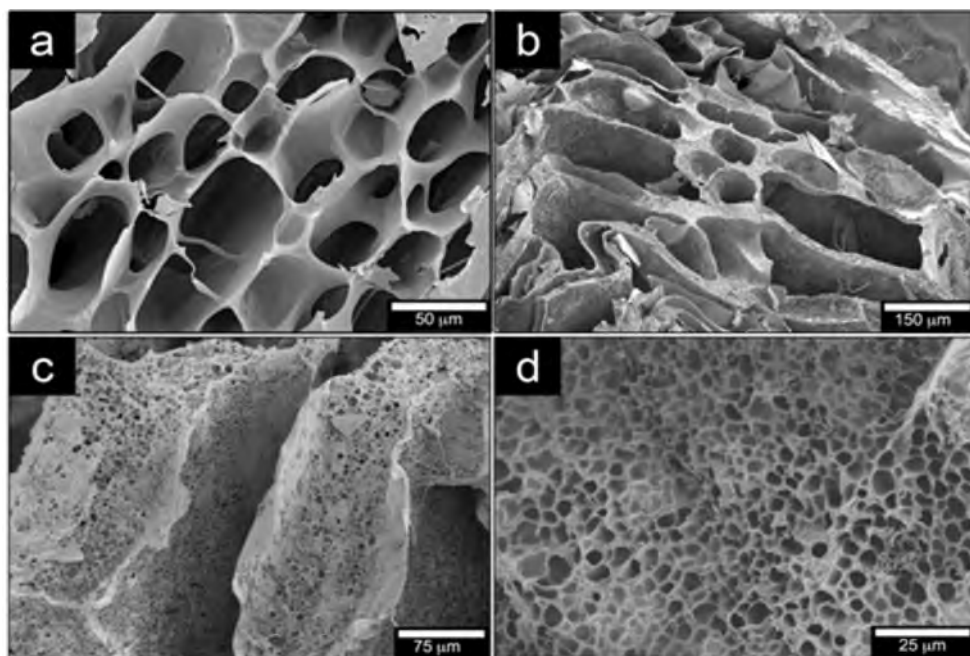


after

Microbe resistance using a diamine, glyoxal and lanosol



Bimodal pore size and antimicrobial properties





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Challenges; accelerated testing
Challenges; biobased materials

Thank you!
